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TRANSPORTATION LABORATORY
RESEARCH REPORT

# Earthwork Reinforcement Techniques

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16. ABSTRACT

This report represents the basic theory, design, construction, instrumentation and field data for the reinforced earth fill constructed on California State Highway 39, Los Angeles County. Design equations for designing the reinforcing strip and the skin plate were developed. The calculated stresses based on the design equations agree reasonably well with the field data. Theoretical analysis by the finite element method based on composite elastic properties of the soil and the steel reinforcement was conducted. The distribution patterns of the analyzed steel stresses generally agree with the measured data but with some discrepancies in magnitude. Also presented are corrosion studies and cost comparisons between the reinforced earth wall and three other types of retaining wall. Presented in the Appendix are the derivation of equations for designing the skin plate; the analysis of the composite material properties of reinforced earth; the User's Manual and list of the finite element computer programs.

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Mr. R. J. Datel
State Highway Engineer

Dear Sir:

I have reviewed and now submit for your information this final research project report titled:

"EARTHWORK REINFORCEMENT TECHNIQUES"

Study made by . . . . . Foundation Section

Under the supervision of . . . . . Raymond A. Forsyth

Principal Investigator . . . . . Raymond A. Forsyth

Co-Investigators . . . . . D. L. Durr and Jerry Chang

Research Conducted and Reported by . . . . . Jerry Chang

Very truly yours,

JOHN L. BEATON
Chief Engineer, Transportation Laboratory

Attachment

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Personnel who were involved in data analysis for this project are:

F. J. Sage, Bert Van Voris, Ellsworth L. Chan, and David R. Castanon

The contents of this report reflect the views of the Transportation Laboratory which is responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of the State of California or the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

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# I. INTRODUCTION

Reinforced earth is a soil mass composed of soil and reinforcing elements (Figure 1). The reinforcing elements provide tensile strength to the soil mass.

The concept of strengthening soil by adding reinforcing elements is not new. Some animals and birds have used straw and branches mixed with soil to build their habitations. Straw has also been used since biblical time to strengthen adobe bricks (1). Alternating layers of earth and logs were used by the Gauls to build fortifications (2). In China, mattresses made of wood branches have been placed in soil to form dikes and revetments along the Yellow River for more than a thousand years. Bundles of brushwood called faggots were used in stabilizing the bank of the Mississippi River in the 1880's (3). In England, faggots were used extensively for erosion control of levees and repairing landslides (4,5). In Taiwan, China, bamboo or steel wire mesh has been used for a long time to enclose stone or gravel in a cylindrical form called wire-stone sausage for building spur dikes and revetments (6). The California Division of Highways utilized redwood logs as reinforcing elements to build highway embankments in the 1930's (7) by laying 20-foot long wood logs in rows and covered with earth to form the embankment section. The concept of using wooden beams as reinforcement for constructing vertical retaining walls was patented in 1930 (8). The strengthening of the downstream slope of earth dams by layers of metal reinforcements along with metal grids or concrete panels for facing elements was proposed early in 1904 (9). Using this concept, several dams were constructed in Mexico in the 1930's and 1940's (10). Similar types of construction have been used in Africa (11), Australia (12, 13, 14) and New Guinea (15).

The California Division of Highways used wire mesh in the 1940's to stabilize embankment slopes against erosion and to prevent slumping (16). Wire mesh fence of 5 feet in width were laid horizontally in the outer edge of the embankment at 10 to 15 foot intervals.

In the 1960's a French engineer, Henri Vidal, developed a disciplined approach based upon a rational design procedure for the use of reinforced earth for application to important engineering structures (17, 18, 19).

Most recently, Harrison and Gerrard (20) used the concept of composite elastic properties of reinforced media proposed by Westergaard (21) to develop mathematical expressions of the elastic constants of reinforced earth. Model testing has been conducted by Yamanouchi (22, 23) to study the improvement of bearing capacity of soft ground by layers of resinous net.

Lee et. al., (24,25) conducted laboratory model tests to study the failure mode of a small-scale reinforced earth wall model and the stresses developed in the reinforcements and soil due to static and horizontal sinusoidal seismic loading.

In July 1970, a research work plan entitled "Earthwork Reinforcement Techniques" was initiated by the Transportation Laboratory, California Department of Transportation, to develop a design method based on established principles of soil mechanics. A field performance study was proposed to study the engineering behavior of a prototype reinforced earth fill on Califonia State Highway 39 near Crystal Lake, Los Angeles County. A comprehensive instrumentation was then installed in the embankment and the reinforced earth fill. Observation of field data was conducted during construction and extended for one year after completion of construction. Laboratory tests were performed to investigate the pulling resistance for different type of reinforcements. Design equations were developed for designing the reinforcement and the skin plate enclosed at the front face of reinforced earth fill. Finite element analyses were conducted to predict the field behavior.

A movie film was also developed to present the basic theory, design method, field data, construction cost, and all aspects of soil investigation, construction, instrumentation and reading instruments.

## II. CONCLUSIONS

The study substantiates the following conclusions.

### A. Field Behavior

1. The settlement of the reinforced earth embankment is primarily attributable to the densification and the associated slight horizontal movements of the deep foundation slide debris. These large foundation settlements and the associated horizontal movement are probably the main cause of continuing change in stresses of the steel and soil after completion of the fill.

   The differential settlements between the center portion and each end of the reinforced earth embankment are the primary causes of the axial tensile stresses in the skin plates. It has been proven that the continuous steel skin elements are very effective in linking the reinforced earth embankment into a monolithic soil mass. This monolithic action helps the redistribution of the horizontal movement along the alignment of the reinforced earth embankment.

2. The measured vertical soil stresses generally agree with the calculated, theoretical vertical earth pressures. The stress ratios, K, between the horizontal and vertical soil stresses were their highest during construction and then decreased after completion of the fill with large variations from point to point.

3. The measured stresses in the steel strips near the wall face were generally smaller than, but approached the calculated theoretical stresses, $\sigma_a$, based on Rankine's active state-of-stress theory. The highest steel stresses developed in the inner middle portion of the reinforced earth section. The steel stresses may increase to the value corresponding to the theoretical "at rest" earth pressure.

4. The strains measured in the steel strips and soil generally agreed with each other. The converted steel stresses, however, were generally smaller than the horizontal soil stresses. This phenomenon is probably attributable to the soil arching action.

5. The structural behavior of the skin plates was as expected in the design assumptions in deformed shape

and stress values. The vertical deformation of the skin plate, which is a measurement of settlement within each skin element, is proportional to the overburden height.

6. Field pulling test results indicate that the load-deformation curves resembled the stress-strain curves obtained from laboratory triaxial compression tests on dense sands. When the strips were pulled loose, the yielding, peak, and residual load points are all clearly defined. The frictional forces developed on the steel strips were proportional to the overburden load for each overburden height. The field measured skin friction angle agreed well with the laboratory test results under equal overburden height.

B. Design Methods

1. Equation 4 presented in this paper for the design of reinforcing strips has been verified. The use of the active earth pressure coefficient, $K_a$, for calculating the steel stress is applicable for the end portion of the reinforcements. For the middle portion of the reinforcement, the coefficient of "at rest" earth pressure, $K_o$, should be used in the design.

2. The relationships between overburden height, strip length, and the factor of safety against slippage shown in Figure 21-g can be used for determining the minimum length of reinforcement, providing the requirement for stability is met.

3. Design Equation 7, developed in this paper for design of the steel skin plate, accurately predicted the stresses developed in the skin plate. Use of the vertical deformation, $\delta_v$, of the skin plate for one of the major design functions has proven to be a satisfactory approach. The assumption of a semi-circular shape simplified the calculation of the stresses in the skin plate and accurately predicted the measured stresses.

C. Theoretical Analysis

The theoretically analyzed results of soil stresses and horizontal movement by the finite element method in general compare favorably with the measured values. The distribution patterns of calculated steel stresses generally agree with the measured data but magnitude are different. The calculated stresses in the skin plate are

all smaller than the measured values. The difference is probably because the finite element program calculated the hoop tension only without consideration of bending. The field data indicates that the predominant stresses developed in the skin plate are due to bending.

The discrepancies between the calculated and measured results are thought to be attributable to the following factors:

1. Two dimensional analysis - The finite element mesh model assumes a two-dimensional structure. The prototype embankment, however, is a three-dimensional structure. The alignment of the reinforced earth fill follows three chords of a horizontal arc, and the embankment was placed in cone shape canyon.

2. Time function - The measured data shows significant changes in steel stress with time because of the continued settlement of the embankment foundation. The finite element program does not include time function of foundation settlement in the analysis.

3. Construction increments - The number of construction increments assumed in the analysis may have a significant effect on the stresses computed in the reinforcing strips. For moderately large increments, the top layer of strips initially have compressive stresses (much like the compression steel in concrete beams). As subsequent layers are added the initial compression is overcome by the expected tensile forces. The actual construction process is almost continuous.

4. Edge effect - The skin plate is curved in shape. The soil may not be in continuous contact with the skin plate. A void may exist between the skin plate and the compacted soil mass at some points. This "edge effect" was not accounted for in the composite element representation of soil-strip behavior.

D. Cost

Even though this demonstration project of the reinforced earth embankment was the first of its kind in the United States and was located in a relatively remote mountainous area with very limited work space, it was found that the reinforced earth embankment was still more economical than all three other types of retaining walls (metal crib wall, reinforced concrete crib wall, and reinforced concrete retaining wall).

## III. RECOMMENDATION

The basic concept of reinforced earth design using conventional soil mechanics theory for determining the stress developed in the reinforcement has been verified from the research project. The field data indicates, however, a wide range of variation, depending on boundry geometry and foundation conditions of the site. Additional research is necessary to further define the factors which influence behavior of soil-reinforcement interaction. In addition, one of the major unknowns is the possible effect of an earthquake on the stability of reinforced earth fill. Following are the specific recommendations for further studies.

### A. Continual Field Studies

The Transportation District 2 of the California Department of Transportation is constructing a reinforced earth fill on Interstate Highway 5, near Dunsmuir, Siskiyou County. Another one near Lakehead, Shasta County will be constructed in 1975. Both of these will be constructed on relative rigid foundations using steel strips for reinforcement and concrete panels for facing. These sites offer the ideal location for theoretical analyses by the finite element method. It is proposed to install instrumentation on these projects to further study reinforced earth field behavior. A research work plan was submitted to the Federal Highway Administration for approval on January 31, 1974.

### B. Improving the Finite Element Analysis Computer Program

It is proposed to improve the finite element analysis computer program by taking into consideration the following:

1. Accounting for possible movement of reinforcement relative to the soil

2. Consideration of including elasto-plastic behavior of soil and reinforcement

3. Consideration of the "edge effects" on using skin plate and concrete facing

4. Improving procedure for handling the overburden dependent and time dependent effects on the elastic properties of the composite material.

## C. Earthquake Resistance Studies

The objective of the earthquake resistance studies are necessary to develop a method for evaluating the dynamic response, and the stability of reinforced earth fill under earthquake loading. This study will involve two phases.

### 1. Theoretical Analysis by the Finite Element Method

In cooperation with University of California at Davis a computer program similar to the QUAD4 program (26) will be developed by considering the following factors.

a. The stress-strain behavior of the steel-soil composite material

b. The damping behavior of the steel-soil composite material

c. The Poisson's ratio of the steel-soil composite material

### 2. Field Dynamic Test on Prototype Structure

Instruments for measuring dynamic response of stress and strains under seismic loading will be installed in the field prototype structure. A steady-state-vibration and a controlled dynamic blasting to produce earthquake-like seismic excitation will be conducted in the field. The dynamic response will be measured by the installed instrumentation. The field test data will then be compared with the analytical results by the finite element method.

## IV. DISCUSSION

### A. Basic Theory

The basic mechanism of a reinforced earth embankment can be explained by Rankine's State-of-Stress theory. Assuming that an element of cohesionless soil mass in a fill is acted on by vertical and lateral stresses, the element of soil mass will be compressed (Figure 2). If the lateral stresses are smaller than the vertical stresses, lateral expansion and vertical compression will occur (Figure 3). When the lateral strain reaches a critical value, the element of soil mass will fail by shearing along a failure plane. A triaxial compression test indicates the same mechanism as described above. The state-of-stress at an imminent failure condition can be described by a Mohr diagram (Figure 4) in which Point A represents the state-of-stress shown by Figure 2 where $\sigma_1$ equals $\sigma_3$. In order to to hold the soil element without failure the lateral stress ($\sigma_3$) must be increased. By Providing reinforcement in a soil element (Figure 5), the skin friction of the reinforcement will supply additional lateral strain. This additional lateral resistance acts as an imaginary plate fixed at each end of the soil element to prevent failure. The state-of-stress at a stable condition is shown by Figure 6.

The state-of-stress developed in a reinforced earth embankment may vary from an "at rest" state in the inner portion of the embankment to the "active" state near the outer face of the embankment. However, the maximum frictional force required to prevent the soil mass from failure can be assumed to be equal to the active earth pressure as shown in Figure 4. The frictional force developed along the surface of the reinforcement is then resisted by its tensile strength.

Referring to Figures 1 and 7, the frictional forces along the surfaces of the reinforcing strips will create a soil arching action in the vertical plane which, in effect, causes the soil particles to link together to form a series of vertical counterfort walls or reinforcing wedges which provide internal stability of the soil mass in a reinforced earth fill.

The determination of the maximum allowable vertical and horizontal spacing of the reinforcements is still uncertain. However, it can be assumed that the reinforcements must be closely spaced so that an arch action within the soil mass can be developed between reinforcements. This arch action, which causes the soil particles to link together

without separation, may depend upon the size of soil particles, the skin friction between the soil and reinforcements, the internal frictional angle of the soil, and the stress developed within the soil mass. Because it is difficult to determine the influence of these unknown factors, the only rational way to select the maximum reinforcement spacing is through large-scale model tests and field performance studies. However, experience has shown that rather small size reinforcements at relatively close spacing (5-foot horizontally and 1-foot vertically) are satisfactory.

B. Design of Reinforcement

Based on the theory and principle discussed in the previous paragraph, the basic equations for designing the reinforcement are presented as follows:

Referring to Figures 4 and 7, following are the notations to be used in developing the basic design equations:

$p$ = active earth pressure in pounds per square foot
$f_s$ = steel tensile stress, in psi
$K_a$ = Rankine active earth pressure coefficient
$b$ = steel strip width, in inches
$t$ = steel strip thickness, in inches
$\gamma$ = soil density, in pounds per cubic foot
$H$ = overburden height, in feet
$d$ = horizontal steel strip spacing, in feet
$\Delta h$ = vertical steel strip spacing, in feet
$T$ = tensile force in steel strip, in pounds
$F$ = frictional resistance, in pounds
$L$ = length of steel strip, in feet
$\delta$ = friction angle between steel and soil

It is believed that the wall face may rotate slightly outward after compaction. A Rankine's active earth pressure may develop on the inner face of the skin plate, as

$$p = \sigma_3 = K_a \gamma H \tag{1}$$

The total earth pressure acting on the inner face of the skin plate will tend to either pull out or break the steel strips. The pull force, T, developed in each steel strip will be then

$$T = K_a \gamma H d \Delta h, \tag{2}$$

and $$T = f_s b t, \tag{3}$$

or $$f_s = \frac{K_a \gamma H d \Delta h}{bt} \quad (4)$$

The friction force developed on each face of the reinforcing plate will be then

$$F = \frac{\gamma H b L \tan \delta}{12} \quad (5)$$

Therefore, the factor of safety against slippage can be expressed as

$$F.S. = \frac{2F}{T} = \frac{2 \gamma H b L \tan \delta}{12 K_a \gamma H d \Delta h} = \frac{b L \tan \delta}{6 K_a d \Delta h} \quad (6)$$

Equations 4 and 6 are the basic equations developed by the Transportation Laboratory for evaluating the reinforcement design provided by the Reinforced Earth Company.

C. Design of Skin Plates

The skin plate which provides restraint for the soil between individual rows of reinforcing strips must be rigid enough to resist anticipated impact or shocks and flexible enough to tolerate a certain degree of deformation to conform with the settlement of the soil mass upon loading. The standard shape of the skin plate used by the Reinforced Earth Company consists of semi-elliptical element of 10 to 13 inches high with a thickness of about 1/8" (3mm).

For simplicity in stress analysis, a semicircular section of skin plate with the assumed soil pressure and deformation configuration is shown in Figure 8. The vertical load, P, which represents the resulting force transferred from a uniform vertical pressure acting along an effective length of reinforcing strip will cause a vertical deformation, $\delta v$, on the skin plate. This vertical deformation is assumed to have the same magnitude as the settlement of the soil mass caused by a uniform vertical soil pressure acting on the top and bottom row of reinforcement. Using strain energy principles (27), the equations for computing the vertical load, P, and end moment, $M_a$, are developed (see Appendix A) as follows:

For hinged end conditions at A and B (Figure 8),

$$P = \frac{4EI\delta_v}{R^3\pi} - \frac{4K_a\gamma HR}{3\pi} - \frac{\gamma HR}{24\pi}(3\pi - 32); \quad (7)$$

and for fixed end conditions at A and B (Figure 8),

$$P = \frac{\delta_v EI}{\pi R^3}\left(4 - \frac{32}{8-\pi^2}\right) + \gamma HR\left(\frac{4-4K_a}{3\pi} - \frac{1}{8}\right)$$

$$- \frac{8\gamma HR}{8-\pi^2}\left(\frac{4-4K_a}{3\pi} - \frac{(1+\pi - \pi K_a)}{8} + \frac{1}{9}\right); \quad (8)$$

and

$$M_a = \frac{8\delta_v EI}{R^2(8-\pi^2)} + \frac{2\pi\gamma HR^2}{(8-\pi^2)}\left(\frac{4-4K_a}{3\pi} - \frac{(1+\pi - \pi K_a)}{8} + \frac{1}{9}\right). \quad (9)$$

In Equations 7 and 8, magnitude of P depends upon the restraint conditions at the ends A and B and the value of vertical settlement, $\delta_v$. In Equation 9, the value of $M_a$ also depends upon the value of $\delta_v$ which can be measured or estimated for settlements of embankment based on field observed data or previous experience.

Once the load, P, and the end moment, $M_a$, are known, the calculation of the stresses in the skin plate becomes a statically determinate problem. These stresses can be readily computed. Equations 7 and 9 can be verified by measuring strain and thus, stresses at selected points on the skin plate and the vertical deformations, $\delta_v$, in field performance studies on prototype structure or laboratory scale model tests.

D. Stability

The overall stability of a reinforced earth embankment under all expected loading conditions was analyzed by considering the reinforced earth mass as a solid block or a gravity type of concrete retaining wall. Sliding instability and earth pressure developed within the backfill behind the reinforced earth mass, and the potential sliding or bearing failure of the foundation was investigated in the same manner as is ordinarily done for design of embankments and retaining walls.

As a rule of thumb suggested by the Reinforced Earth Company, for stability considerations, the ratio of depth to clear height of a reinforced earth embankment is suggested to be at least 0.8. It is also suggested that the footing of the reinforced earth embankment be embedded in an excavated or backfilled berm to one-fifth of the clear height of the reinforced earth embankment; the width of the berm should be at least 5 feet and the outer slope of the berm should be not steeper than 1.5 feet horizontal on 1 foot vertical (Figure 9).

## E. Corrosion

The durability of the steel reinforcement and skin plate is one of the major concerns in the design of reinforced earth structures. According to Herbert Uhlig (28), the major factors that govern corrosivity of a given soil are porosity (aeration), electrical conductivity, content of dissolved salts including depolarizers or inhibitors, moisture content, and acidity or alkalinity. In general, life expectancy of steel strips is governed by the rate of metal loss due to corrosion. Havilard, Bellair and Morrell (29) reported the results of ten studies concerning the durability of galvanized steel culverts. It was found that the rate of metal loss for uncoated steel culvert varies from 0.0001 to 0.0056 inch per year.

The California Transportation Laboratory developed a method for estimating relative soil corrosivity by combining the relative influences of the hydrogen-ion concentration (pH) and the minimum resistivity of the soil (30). Figure 10 is a chart developed for estimating underground corrosion rate of steel pipe. This chart shows the relationship between corrosion rate, minimum soil resistivity (ohm/cm$^3$) and pH values for acid soils and alkaline soils. A thorough investigation of soil samples and corrosive environment for a given construction site is recommended. Laboratory and field soil tests should be conducted to determine various factors which affect corrosion.

Figure 10 can be used for estimating the rate of metal loss, and to establish the required thickness (corrosion allowance) of steel reinforcement for the design life. In excessively corrosive soils, cathodic protection (31) may be employed to prevent reinforcement deterioration.

## F. Demonstration Project

A reinforced earth fill, the first in the United States, was constructed between August 1 and October 18, 1972.

This project is located on Route 39, near Crystal Lake, in the San Gabriel Mountains, Los Angeles County. The reinforced earth fill is constructed on top of a random fill embankment founded over slide debris. At the bottom of the slide debris a toe buttress was built to act as a stabilizing fill embankment. The overall height of the system is approximately 360 feet. The reinforced earth fill has a maximum height of 55 feet and a length of 528 feet. A drainage system consisting of surface and subsurface drain pipes were installed to remove surface water and seepage. The detailed design and stability analysis of the Route 39 embankment was reported in Highway Focus, January, 1972, published by the U.S. Department of Transportation (32). Figure 11 shows a plan view and a sectional view. Photo 1 shows the completed view of the project. Several important features pertaining to the demonstration project are discussed as follows:

1. Soil Testing

Soil material for the embankment and reinforced earth fill consists primarily of decomposed granite obtained from two cources; (1) slide debris at construction site and (2) borrow material from a borrow site located approximately 1.5 miles northwest of the construction site on California State Highway 2. Soil samples were taken from these two sources for laboratory tests. A summary of testing results of the borrow material is shown in Table 1. The coefficient of earth pressure at rest, $K_o$, was computed based on J. Jaky's (33) expression, $K_o = 1-\sin\emptyset$. Laboratory pulling tests to determine the skin friction were conducted using a specially designed small shear box (32). The stress-deformation curve obtained from the laboratory pulling test is shown in Figure 12. Based on the residual shear stress as indicated in Figure 12, the envelope line shown in Figure 13 indicates a skin friction angle of 31 degrees between the galvanized reinforcing steel strip and the decomposed granite borrow material.

Corrosion tests were also conducted for the borrow material. It was found that the borrow material is an alkaline soil with a pH value of 7.7 and an average resistivity of 13,000 ohms per cubic centimeter. The rate of metal loss is less than 1 mil per year based on Figure 10. A life of more than 50 years can be expected for the galvanized steel strip.

2. Skin Plates and Steel Reinforcement

The galvanized reinforcing steel and the skin plate were all purchased from the Reinforced Earth Company and imported from France at $750 per ton. The dimensions of the steel

reinforcing strips are as follows:

| | |
|---|---|
| Thickness: | 0.118 inches (3 mm) |
| Width: | 2.362 inches (60 mm) |
| Length: | 22.79 to 46.0 feet (7 to 14 m) |

A standard tension test was conducted at the structural material laboratory of the Transportation Laboratory. Testing results are as follows:

| | |
|---|---|
| Yielding strength: | Fy = 37,000 pounds per square inch |
| Ultimate strength: | Fu = 50,000 " " " " |
| Young's Modulus: | E = 28.5 x $10^6$ " " " " |
| Poisson's ratio: | = 0.28 |

The skin plates are semi-elliptical in shape, 10 inches high along the major axis, and 3.7 inches deep along the minor axis. The skin plate has a thickness of 0.118 inches (3 mm) and length varying from 6.56 feet (2 meters) to 39.37 feet (12 meters).

3. Construction Operation

The construction of the embankment was started on March 14, 1972 and completed to Elevation 6353, the footing of the reinforced earth fill, on July 31, 1972. Figure 14 shows the daily history of the fill height.

The construction of the reinforced earth was begun August 1, 1972. The fill area was leveled with an approximately 1% downward slope back from the face of the wall. Batter boards (Photo 2) were erected at approximately 10-foot spacing to provide the initial horizontal and vertical control for placing the skin elements which are laid against the batter boards and brought to a precise level. The reinforcing strips were laid perpendicular to the alignment of the skin element on the compacted fill (Photo 3). Each strip was then bolted to the skin element. Wooden wedges were driven between the skin elements to tilt the elements inward towards the fill (Photo 4). As the fill was placed and compacted against the upper edge of the skin plate (Photo 5), the skin element was forced outward to a plumb position. The correct amount of inward cant determined by trial and error to be approximately one-half inch. At each end of the skin element an expansion gap of one inch was provided. Connection plates were placed over the gap at each end of the skin elements to prevent local soil sloughing. Three skin elements were erected prior to placing and compacting the first 10-inch lift of fill.

The purpose of maintaining three skin elements above the last compacted lift of fill throughout the wall construction is to provide a sufficient resistance to the outward force during compaction of the fill and to serve as a safety barrier at the wall face. Compaction control of the fill was maintained using a nuclear gage. The field measured densities are shown in Table 2.

4. Construction Equipment and Labor Work

The construction of the reinforced earth fill requires only ordinary highway construction equipment and the usual labor force. Tables 3 and 4 show, respectively, the equipment and labor work with hourly rates used in construction of the California Highway 39 reinforced earth project.

5. Construction Cost

The construction cost of the reinforced earth fill consists primarily of the following three parts described below:

a. The galvanized steel skin elements and reinforcing strips were imported from the Reinforced Earth Company of France. The price of steel was $750 per ton, delivered from France to the job site, which include patent rights, transportation, packing, custom duty, and required service in design and supervision of construction.

b. The borrow material is a contract item. The bid price was $1.80 per cubic yard, which includes excavation, grading, and transportation of the fill material from the borrow site to the job site.

c. The erection of the skin element, placing and compaction of fill material were paid by force account. The hours of rent for each piece of construction equipment and labor work hours were recorded daily by the Resident Engineer's Staff. The hourly rate was based on the values listed in Tables 3 and 4. Figure 15 shows the daily record of construction quantities. The cost spent each week for rent of the construction equipment and labor service, together with the unit cost are shown in Figure 16. It is seen that at the time when the equipment and labor were mobilized at the highest peak, the unit cost of compacted fill and the total unit cost including equipment, labor, steel and fill material became the minimum at $3.50 and $7.40 per cubic yard of fill, respectively. Average unit

quantities and costs are shown in Table 5. It should be pointed out that this project was the first of its kind in the United States and was located in relatively remote mountain area with very limited working space. Thus, the cost data may not be representative of present-day construction in a more accessible site.

Based on the unit price of $750 per ton for the steel and $5.00 per cubic yard for placing and compaction of the fill material, the unit cost of reinforced earth fill versus height is plotted in Figure 17 and tabulated in Table 6. For comparison purposes, the unit cost for reinforced concrete crib wall, metal crib wall, and Type 1 reinforced concrete retaining wall (spread footing), which are indicated in California Division of Highways' 1973 "Standard Plans" pages 35, 37, 87, respectively, are also plotted in Figure 17 based on current contract bid prices furnished by the Office of Structures of the California Department of Transportation. The structural backfill is estimated to be $8.00 per cubic yard for the crib walls and the reinforced concrete wall. It is seen that the reinforced earth fill is lower in cost than the three types of retaining walls.

## 6. Instrumentation

In order to monitor the behavior of the completed structure, a comprehensive instrumentation program was planned and implemented. These instruments included (1) slope indicators to measure the internal movement of the embankment and the slide debris, (2) settlement platforms (Photo 6) to measure the vertical settlements, (3) extensometers (Photo 7) to measure the soil strains (4) soil pressure cells (Photo 8) to measure soil stresses, (5) strain gages to measure the stresses developed in the reinforcing strips (Photo 9) and skin elements (Photo 2), (6) gage points to measure the deformations of the skin plates and the wall face, (7) monuments to measure the displacements on the wall face, top of fill, and top of the berm. Locations of the instruments are shown in Figures 11 and 18. Photo 10 shows three instrumentation shelters for reading the instruments. Installation details of instruments are shown in Table 7, 8 and 9. The detailed data of slope indicator holes and its installation are shown in Table 10.

## 7. Field Data

All instruments in the reinforced earth fill were read periodically during construction and after completion of construction for approximately one year. The slope

indicators installed in the embankment were read periodically since March 28, 1972. The various field data are discussed separately as follows:

a. Internal Movement of Embankment

The internal movements in the embankment were measured by slope indicators. A total of 10 slope indicators was originally planned for the embankment and the reinforced earth fill. Due to the difficulty of drilling through the talus and the considerable expense involved, only three slope indicators were installed. The locations of the three slope indicators are shown by Figure 11.

Horizontal movements measured by slope indicators SI-1 through SI-3 are shown in Figures 19 through 24. Slope indicator SI-1 initially deflected about 1.5 inches westward during construction and almost recovered to the vertical position at 15 feet deep about one year later. In the southward direction, the top of SI-1, deflected continuously to more than 3 inches but recovered almost to the vertical position at about 15 feet deep. The slope indicator SI-2, deflected continuously westward and northward for 0.9 inch at 10 to 20 feet deep. The slope indicator SI-3 deflected about 3.9 inches westward but only 0.5 inch northward. The pattern of the plotted data shown in Figures 23 and 24 indicate that the slope indicator casing is not locally deflected but the whole section of embankment was moving in the down slope direction. This movement is probably the cause of the cracking of the roadway pavement directly above and behind the reinforced earth fill (Photo 14) between Station 552+95 and Station 553+75 observed in April 1974.

The settlements of the embankment were also measured by slope indicators SI-1, SI-2, and SI-3 and shown in Figures 25 through 27. The maximum settlements are 0.55 foot, 0.73 foot, and 0.95 foot measured by SI-1, SI-2, and SI-3, respectively.

b. Movements of the Reinforced Earth Fill

The horizontal movements of the reinforced earth fill were measured by three series of survey monuments located on the embankment berm (Series "A", Figure 28), on the wall face (Series "B", Figure 29), and on top of the wall (Series "C", Figure 30). Appreciable horizontal movements were observed along the left wing of the reinforced earth fill (wall Station 13+04 to 14+75). The horizontal movements vary from 0.3 foot to 0.45 foot

on the berm (Figure 28), 0.1 foot to 0.55 foot on the wall face (Figure 29), and 0.1 foot to 0.65 foot on top of the wall (Figure 30). The largest horizontal movement occurred between wall Station 13+25 and Station 14+50 where the crack was observed in April 1973 (Photo 14). This horizontal movement is consistent with the movement measured by slope indicator SI-3. These cracks were patched by District 07 Maintenance Department personnel in the summer of 1973. The data shown in Figures 28 through 30 indicate that movement diminished considerably after June 1973. Figures 31 and 32 show the displacements of the wall face. An appreciable rotation of the wall face was observed at Stations 12+75, and 14+00.

c. Settlement of Reinforced Earth Fill

A daily history of settlements and fill heights of the reinforced earth fill are shown in Figure 33. At Station 551+75, approximately at the middle of the wall alignment, the measured settlements were proportional to the increases in fill height and continued to increase at a reduced rate after completion of fill. The settlements at Levels B and C were comparable. Much larger settlements occurred at Level A. The readings on June 20, 1973 indicate an average settlement of 1.3 feet at Levels B and C and 3.5 feet at Level A. The average difference in settlement between Level A and the average of Levels B and C from Section I through Section IV is about 1.2 feet which is believed to be primarily attributable to densification of the slide debris below the embankment.

At Station 550+25, much smaller settlements were observed, due to the lower wall height (36 feet as compared to 53 feet at Station 551+75) and lesser thickness of slide debris in the foundation. The readings on June 20 indicate the average settlements are 0.75, 0.68 and 0.50 feet at Levels A, B, C respectively, from Section I through IV. The average difference in settlement is only 0.07 foot between Levels B and C. The rate of settlement after completion of fill at Station 550+25 was much smaller than that at Station 551+75.

d. Soil Stresses in the Reinforced Earth Fill

Figures 34 and 35 show the soil stresses measured at Station 550+25 and Station 551+75, respectively.

The ratio, K, between the horizontal stress and vertical stress is also plotted on these two figures. The $\gamma H$ lines represent the theoretical vertical soil stresses in pounds per sq. in. computed from the unit weight, $\gamma$, 143 pounds per cubic foot and the depth of fill, H, over each instrument level. The K values varied irregularly during and immediately after construction. The values of the vertical and horizontal stresses were close in magnitude in the beginning which is believed to be due to the equal influence of the compaction operation. As the fill height increased over the instrumentation level, the influence of the compaction operation diminished. After completion of the fill, the K values still varied slightly in the range of 0.11 to 0.41 at Station 550+25. The calculated Rankine's coefficient of active earth pressure, $K_a$, is 0.22 and the coefficient of earth at rest, $K_o$, is 0.36, based on an internal friction angle of 40° obtained from laboratory triaxial compression tests on the borrow material (Table I).

At Station 551+75, the K values range from 0.20 to 0.90. The K values at this station are much greater than $K_a$ and $K_o$ except at Section I, Level C where some bulging has been observed on the skin plates.

e. Stresses in Steel Strips

The daily history of stresses in the steel strips is shown in Figure 36. The steel stresses are computed from products of the average values of strains recorded on tops and bottoms of the strips and the modulus of elasticity ($28.5 \times 10^6$ psi) obtained from laboratory tests of the steel strip. For comparison, the steel stresses for the active earth pressure case and "at rest" case were computed and are shown on Figure 36 using Equation 4 based on data as shown.

At Station 550+25, on Level A tensile steel stresses were observed at one foot from the wall face. After completion of the fill, the stresses near the wall face decreased with time and eventually became compressive on Level A. This phenomenon was probably due to the restraint provided by the berm. At 15 and 25 feet from the wall face, the tensile steel stresses increased with time and finally reached $\sigma_a$, the calculated active earth pressure. At Level B, the tensile steel stresses at 15 feet from the wall face decreased with time to values much lower than $\sigma_a$, while the stresses

at 25 feet from wall face increased with time and approached the calculated earth pressure at rest, $\sigma_o$. At Level C, the magnitude of tensile steel stresses at 15 and 25 feet from wall face decreased with time, and approached $\sigma_a$. The steel stress at one foot from wall face decreased to below $\sigma_a$ but approached $\sigma_a$ at a later time.

At Station 551+75, all strips on Level A were in compression with the maximum stresses developed near the wall face. This phenomenon is undoubtedly due to the restraint provided by the berm, since Level A is about 10 feet below the top of the berm. At Level B, all strips were stressed in tension with the magnitude much less than $\sigma_a$ near the wall face and at 30 feet from the wall face, while the strip at 15 feet from the wall face was stressed to approach $\sigma_a$. At Level C, all steel stresses increased with time. The reading on June 20, 1973 shows that the stress approached $\sigma_a$ near the wall face, and becomes greater than $\sigma_a$ at 15 and 30 feet away from the wall face.

f. Strain in Steel and Soil

Daily history of horizontal strains in the steel strips and soil are compared in Figure 37. The strains in the steel strip were measured by strain gages glued one each on bottom and top face of the strip at each planned location. The strains in the soil were measured by an extensometer and read out electronically. The strains measured in both the steel strip and soil were reasonably consistent with each other and approach the same magnitude with increasing time after completion of the fill, except for those measured at Section II, Level C, at Station 551+75.

The constant discrepancy in strains measured by strain gages C-15 and 16 on the steel strip and by Extensometer 78 for the soil on Level C, Section II, at Station 551+75, may indicate that slippage of the steel strips occurred since bulging out of the skin plate occurred at this level. This may explain the high steel stresses, with magnitudes greater than $\sigma_o$, (Figure 36, Gages C-15, 16, 17 and 18) and the horizontal soil stress approaching $\sigma_a$ (Figure 35, PC 135).

g. Horizontal Soil Stresses and Converted Steel Stresses

The daily histories of horizontal soil stress and converted steel stress are compared in Figure 38. The

converted steel stresses, representing the equivalent soil stress, are computed using Equation 4 with measured steel strain data and the elastic modulus of steel equal to $28.5 \times 10^6$ psi. All the converted steel stresses are smaller than the comparable soil stresses. This difference is probably due to the soil arching action. This would cause the soil near the steel strip to be strained less than that at the center of the interval between two steel strips.

h. Axial Force in Dummy Strips

Addition instrumented steel strips were installed in the fill for pulling tests. Strain gages were installed at each 5 feet spacing for measuring the strains along the steel strips before and during pulling tests. The case histories of the axial forces developed in two of the instrumented dummy strips are shown by dotted lines in Figures 39-a and 39-b for the 23-foot and 46-foot strip, respectively. The maximum stresses are all developed at about 10 feet from the wall face for the 46-foot strip. In the 23-foot strip, it is believed that the maximum stresses developed between 10 and 15 feet from the wall face. Figure 39-c shows the relationship between overburden loads and the maximum axial force observed at gage Point 10 for the 46-foot strip and the extrapolated maximum axial force between gage Points 10 and 15 for the 23-foot strip. The axial forces developed during construction are all lower than the calculated tensile force, $T_a$, from Equation 4, based on the Rankine's active earth pressure case. However, after the fill was completed the axial force continued to increase and the maximum axial force reached $T_a$, in the 23-foot strip. In the 46-foot strip the maximum axial force finally reached $T_o$, the calculated tensile force from Equation 4 based on the "at rest" earth pressure case. The continuous increase in tensile force after completion of the fill was probably due to the continuing settlement developed in the fill as shown in Figure 33. It has also been observed that the face of the wall has been continuously moving horizontally downslope since completion of the fill (Figures 28 through 32).

The solid line shown in Figures 39-a and 39-b are the axial forces observed during field pulling tests to be discussed later.

i. Stress in Skin Element

Figure 40 shows the daily history of stresses in the skin elements. The locations and the identification numbers of the strain gages are shown on the upper right of the

figure. Gages 1, 5 and 9 measure strains on the front face in the axial direction; Gages 3, 7 and 11, measure strains on the inner face in the axial direction; Gages 2, 6 and 10, measure the circumferential strain on the front face; and Gages 4, 8 and 12, measure the circumferential strain on the inner face. The actual deformation of the skin elements closely approximated the deformation assumed in developing Equations 7, 8 and 9 for designing the skin plates. Tensile circumferential stresses developed on the front face and compressive circumferential stresses on the inner face. The axial stresses were in tension except for skin element 8 which is embedded in the embankment berm. The tensile axial stresses are believed to be attributable to the greatest settlement occurring at the middle of the reinforced earth fill. Because the largest settlement occurred at the middle of the fill, all skin plates were being pulled toward the middle where end to end buckling has been observed for many of the skin elements.

j. Field Behavior of Steel Skin Plate

Deformation of the skin elements were measured at 5 separate gage points on the faces of the skin plates with a specially designed vernier-micrometer caliper capable of accurately measuring to one-thousandth of an inch.

The deformation of skin element No. 20 (on Elevation 6368.92, near Station 551+75), which is a typical case, is shown in Figure 41. The relationship between the magnitude of deformation and fill height is also shown. These deformations agree very well with the assumptions made in developing the design Equations 7, 8 and 9. Based on the vertical deformations observed in the field, the stresses in the skin plates were calculated using these equations, for both hinged and fixed end conditions. A comparison of the measured and computed stresses is shown in Figure 41. The calculated Stresses based on hinged end assumption (Equation 7) agree reasonably well with the measured data, while the calculated stresses using Equations 8 and 9 (fixed end condition) are almost three times larger than those measured.

8. Field Pulling Tests

Additional dummy steel strips were installed in the fill at 5 levels for field pulling tests. Three strips, 5, 10, and 15 feet in length, were embedded at each of three levels under overburden heights of 7.5, 12.4 and 18.2 feet. Three

23-foot strips were embedded at a depth of 18 feet and three 46-foot strips were embedded at a depth of 38 feet. One each of the 23-foot and 46-foot strips was instrumented with strain gages on both top and bottom at 5-foot intervals.

Pulling loads were applied using a hydraulic jack acting against wooden blocks for bearing pads (Photo 11). The pulling loads were measured with a load cell. Deformation or extension of the steel strips was measured with two extensometers fastened on each side of the steel strip (Photo 12). A Hewlett-Packard 2010A Data Acquisition System (Photo 13) was used to record electronically the pulling loads and strains of the steel strips.

Load deformation curves obtained from field pulling tests are shown in Figure 42 for the 5-, 10- and 15-foot strips and Figure 43 for the 23- and 46-foot strips. Three pulling loads were selected for analysis and are indicated on the curves. These three loads are (1) yield load representing the proprotional limit of the load-deformation relationship; (2) peak load representing the maximum pulling load observed; (3) the residual load representing the pulling load when deformation increased appreciably without changing in the pulling load.

One of the 23-foot strips was broken at a pulling load of 14,000 pounds. Three of the 46-foot strips were broken at pulling loads of 13,460; 14,200 and 14,450 pounds. The rest of the strips failed by slipping at the residual loads shown in Figures 42 and 43.

The yielding loads represent the elastic properties of the steel. When the strip is long enough and the overburden load is high enough, i.e., when the frictional grip is large enough, the yield load will reach the yield capacity of the steel (about 10,300 pounds). If the frictional grip is not sufficient at the front end of the strip, the soil will start to strain before reaching the yield strength of the steel. Therefore, it appears that the yield load represents the yield capacity of the steel or the maximum possible frictional grip of the compacted soil without the introduction of strain of the soil. The peak load represents the maximum mobile pulling resistance of the composite material of the reinforcement and soil. After the peak load, the strip becomes partially loose and progressively, the whole length of the strip starts sliding when the pulling loads drop to the residual level. If the strips break there will be no peak load or residual load. Figures 44-a, 44-b and 44-c show the relationship between the three types of pulling loads and the overburden height and strip length. The skin-friction angles, $\phi_u$, decrease with increasing overburden height as shown in Figure 44-c. This phenomenon cannot be explained theoretically.

It is interesting to note that under a constant overburden height, the yield, peak and residual loads are all proportional to the overburden loads which are the products of the overburden height, H, the unit weight, $\gamma$, the width of steel strip, b and the length of the steel strip, L. Since $\gamma$, b and H are constant under a constant overburden height, the yield, peak and residual loads are all proportional to the strip length. A field soil unit weight of 143 pounds per cubic foot was used in calculating the overburden loads. When the length of strip is constant, the relationships between the yield load and peak load with the overburden load are nearly linear. This is not the case, however, with respect to the relationship between the residual and overburden load. This phenomenon is probably attributable to the fact that the residual loads are not well defined on the pulling test curves as shown on Figures 42 and 43. Some of the pull tests were not continued long enough to establish the flat portion of the load-deformation curve. Because the peak load represents the maximum mobilized friction grip, the factors of safety were evaluated using the peak loads as failure loads and the designed tensile loads were calculated using Equation 2. The relationships between overburden height, H, strip length, L and the factor of safety (F.S.) are shown in Figure 44-d.

Because the residual load, representing a complete slippage failure, is much lower than the peak load, a conservative factor of safety of 4 is recommended for design purposes to select the minimum length of strip at different overburden heights. According to Figure 44-d, for a factor of safety of 4 and under a fill height of 10 feet, the minimum strip length required is about 9 feet.

Referring to Figures 39-a and 39-b, during pulling tests, the externally applied pulling force strained the 46-foot strip only up to Gage Point 10. There was no increase in axial stress in the 46-foot strip beyond Gage Point 10. The 46-foot strips were all broken at the external extended portion. It appears that the frictional grip was so great along the 46-foot strip that the strip was acting as though fixed at Gage Point 10, so that there was no change in stress occurring beyond this point due to the externally applied pulling load. In the 23-foot strip, only a slight increase in stresses were observed beyond Gage Point 15 due to the externally applied pulling load.

Figure 45 shows the relationship between peak pull load and the calculated skin friction force. It is interesting to note that the peak pull loads exceed the skin friction force as the strip length exceeds 10 feet. It may be concluded that strip length should be at least 10 feet.

## G. Theoretical Analysis by the Finite Element Method

A finite element computer program was developed by Professors L. R. Herrmann and K. M. Romstad of the University of California, Davis, under a special service contract. A detailed description of the formulation of the material properties of reinforced earth are given in Appendix B with the user's manual for the computer program in Appendix C.

In the theoretical analysis, the reinforced earth is assumed to be a composite material, and that if the pattern of the reinforcement is repeated a sufficiently large number of times, the composite material can be considered homogeneous at the phenomenological level. Each strip of reinforcement bounded by the centerline of both the vertical and horizontal spacing can be viewed as a "unit cell" which, when it is repeated in all directions, results in the configuration at the phenomenological level of a composite material.

The "unit cell" of the reinforced earth mass shown in Figure B-2 (Appendix B), consists of a soil with thin steel strips parallel to each other at chosen spacings and extend deep into the soil mass. In formulating the composite stress-strain relationship it is assumed that the composite stress-strain state in the 2 and 3 directions equals the stress-strain state of soil, and the displacements of all points in any 2-3 plane are equal for both soil and strip, therefore, the composite material exhibits an isotropic behavior with perfect bond at the soil-strip contact. The mathematical expression of the composite stress-strain state is given in Appendix B.

Although this program was specifically designed for the analysis of reinforced earth embankments, it can be applied to a wide range of problems such as the calculation of stresses and deformations in embankments and foundations; computation of rebound in slope and foundation excavations; and determination of stresses and strains developed in embedded conduit in a large soil mass. The program calculates the composite stresses and strains of the composite material in the "unit cell". Using the composite stresses and strains the corresponding stresses and strains in the soil and axial forces and moments developed in the reinforcing strips are then determined. Several special provisions contained in this program are as follows:

1. The incremental construction sequence

2. Overburden dependent material properties

3. Orthotropic material behavior

4. Reinforced earth construction

5. Bending members

The details of using this program to solve various problems relating to the above provisions are referred to in Appendix C.

1. Elastic Property of Fill Material

For evaluating the elastic property of the fill material, three soil samples as identified in Table 11 were taken during construction. These soil samples were subjected to triaxial compression tests for determining the shear strength parameters (Table 12), which are required for evaluating the elastic constants. To arrive at the shear strength parameters, three failure criteria as suggested by Chang, et. al., (34) were investigated.

1. The peak or the maximum deviator stress represents the "failure stress" of the specimen.

2. When the deviator stress and the axial strain increase continuously during the test and there is no well defined peak on the stress-strain curve, the deviator stress at 15 percent axial strain is considered the "failure stress".

3. The ultimate deviator stress, represented by the deviator stress at the asymptote of an idealized hyperbolic fit of the stress-strain curve, is to be considered as the "failure stress".

According to Chang, et. al., (35) the equation for computing the tangent modulus, $E_t$, of soil is

$$E_t = E_i\left[1 - \frac{\gamma H \sin\phi(1-\sin\phi)}{2C\cos\phi+2q\sin\phi}\right]^2 \qquad (10)$$

where

$E_i$ = $A+B(1-\sin\phi)\gamma H$ = initial tangent modulus in pounds per square foot,

$c, \phi$ = shear strength parameters determined from ultimate strength criterion (c is expressed with unit in pounds per square foot),

$\gamma$ = density of soil in pounds per cubic foot,

$H$ = height of embankment overburden in feet,

$N_\phi = \tan^2 (45 \text{ deg} + \frac{\phi}{2})$, and

$$q = \frac{\gamma H}{N_\phi} - \frac{2c}{(N_\phi)^{1/2}}$$

A and B are constants to be determined from the arithmetic plots of the initial tangent modulus, $E_i$, and the confining pressure, $\sigma_3$, obtained from the triaxial compression stress-strain curve.

The calculated tangent modulus values are shown in Table 13. Figure 46 shows typical stress-strain curves obtained from triaxial compression test on Sample No. RE-7. Figure 47 is a plot of the stress-strain data in a transformed hyperbolic form from which the ultimate deviator stress and the initial tangent modulus, $E_i$, was determined (34). Figure 48 shows the typical Mohr Circles on which the ultimate friction angle for Sample No. RE-7 was determined based on the ultimate deviator stress obtained from Figure 47. The variation of the initial modulus with confining pressure is shown in Figure 49 from which the A and B constants was then obtained.

Poisson's ratio of the fill material was also evaluated using the method and equations developed by Kulhawy, Duncan and Seed (36). The computed results of Poisson's ratio are shown in Figures 50 and 51. Tables 14 and 15 show respectively, the values of the calculated parameters and Poisson's ratio based on the equations suggested by Kulhawy, et. al(36). The Poisson's ratio ranges from 0.13 to 0.78 for the fill material. Based on previous experience for the finite element analysis of the stresses and strains in the Jail Gulch embankment (34), a Poisson's ratio of 0.3 was chosen in this study.

## 2. Finite Element Analysis

In the finite element method, the cross-section of a continuous body is idealized as a set of small, but finite elements connected at their joints or nodal points. The finite element mesh or assemblage of elements for this study is shown in Figure 52, which represents a section at Station 551+75 of the reinforced earth fill. The assumed boundary condition construction sequence and representative materials samples are also shown in Figure 52.

The boundary on foundation rock is considered to be fixed assuming no deformation. The right side vertical boundary is considered to be a free surface assuming that a crack is developed in the slide debris area behind the reinforced earth fill (crack lines were observed in that area in the field). Several roller joints were assumed along the rock foundation immediately below the right side vertical boundary to allow the downward movement of the slide debris upon loading. The vertical boundary at the left side is considered to be on rollers to allow downward movement due to settlement of the embankment.

The material of the model consists of foundation rock, original overburden, slide debris, and borrow material. Each material was represented by the elastic property of the selected soil samples as indicated in Figure 52. Soil Sample No. RE-8 which was taken from the borrow material represents the soil material for the original overburden, the embankment, the berm, and the backfill. The slide debris is represented by Soil Sample No. 1384-85 which was obtained from the slide debris material. The reinforced earth fill is represented by Soil Sample No. RE-7, which was obtained from the borrow material during construction of the reinforced earth fill. Composite elastic properties were evaluated by considering the elastic property of the reinforcing strip and the soil. Due to variations of spacing of the reinforcing strip at three different elevations, the composite material is represented by three fictitious sub-grouped soil samples, RE-7-A through RE-7-C, representing the composite material in the reinforced earth fill as shown in Figure 52. The elastic property of the composite material was automatically computed by the computer with the special provisions in the finite element program.

The construction sequence is divided in 12 sequential stages as shown in Figure 52 by circled numbers.

3. Analyzed Results and Comparison With Field Data

The theoretically analyzed results by the finite element method are all compared with the field data obtained at Station 551+75 on November 1, 1973, which is about two weeks after completion of the reinforced earth fill coinciding with the date of completion of the embankment berm and the roadway pavement. Most of the field data at Station 551+75 has continued to change. It appears that the field data obtained on November 1, 1972 in general compared more favorably to the theoretically analyzed results.

a. Vertical Soil Stresses

The theoretical vertical soil stresses are shown by contours in Figure 53. Field data are also shown in parentheses. The contours of the theoretical vertical soil stress indicate two particularly interesting characteristics:

1. Stress concentration at the toe of the reinforced earth fill which is also substantiated by the field data. This phenomenon may be due to the combination effect of the overturning moment from the backfill earth pressure and the lateral restraint of the berm;

2. A substantial reduction in vertical soil stress occurs along the boundary line (the inclined dashed line - Fig. 53) between the slide debris and the backfill and embankment (Figure 52). This characteristic is obviously due to the sudden change in rigidity of the soil from a high value of tangent modulus in the embankment and backfill to the low tangent modulus in the slide debris.

   Figure 54 shows a comparison of vertical soil stress distribution between the theoretical results and field data. It is seen that a relatively good agreement exists between the theoretical results and field data.

b. Horizontal Soil Stresses

The contours of the theoretical horizontal soil stress are shown in Figure 55. It is interesting to note that the backfill behind the reinforced fill is almost completely in tension which obviously cannot be sustained by the soil. Field observation indicated numerous seam cracks in the backfill area (Photo 16). The observed substantial

settlement and horizontal movement of the wall face of the reinforced earth fill could be the evidence that a slight slide movement occurred along the boundary line of the slide debris due to considerable densification of the slide debris material. Figure 55 shows an extremely large buildup of horizontal stress at the toe of the wall corresponding to the concentration of the vertical soil stress shown in Figure 53.

The comparison of the distribution of the horizontal soil stress between the field data and the analytical results are shown in Figure 56. It also indicates moderately good agreement.

Figure 57 shows the contours of the theoretical stress ratio, K ($\sigma_x/\sigma_y$), which is in poor agreement with the field data (Figure 35).

c. Shear Stresses

Figure 58 shows the contours of the theoretical shear stress. It shows additional evidence of the stress concentration at the toe of the reinforced earth fill. The calculated maximum shear stress of 1600 pounds per square foot is well below the available shear strength of the soil at that location. Contours of zero shear stress developed at the upper part, the back part of the reinforced earth fill, and also the berm of the embankment. This indicates changes in direction of shear stresses occurred along the zero contours.

Figure 59 shows contours of factor of safety based on the ratio of the available shear strength and the theoretical maximum shear stress.

d. Theoretical Steel Strip Forces

The contours of the forces developed in the reinforcing steel strip are shown in Figure 60. All the theoretical strip forces are in tension with force concentrations at Level B and at back side on Level A. The field data are much smaller than the theoretical results at Levels B and C. At Level A, the field data indicates compression forces developed in the steel strip at the toe of the reinforced earth fill. Therefore, the comparison between the analytical and field data shows rather poor quantitative agreement but similar patterns of stress distribution (Figure 61).

e. Stresses in the Skin Plate

A comparison of the theoretical and observed stresses in the skin plate is shown in Figure 62. The theoretical

stresses are generally smaller than those measured. This discrepancy is due to the assumption that the skin plate is treated as a hoop tension member in the finite element program and no bending stress is considered. In the field data the predominant stresses are due to bending.

f. Settlement in the Reinforced Earth Fill

A relative comparison of the theoretical and field settlements is shown in Figure 63. These settlement data are with respect to the reference point at the berm by assuming zero settlement at the berm reference point. The actual settlement should be the sum of the actual settlement at the berm reference point and the data shown in Figure 63.

The theoretical settlements are smaller than those of the field data at Levels A and C, but larger at Level B. The agreement between the theoretical and field data is rather poor in magnitude.

g. Horizontal Movement of Berm and Wall Face

The results of finite element analysis for the horizontal movement at three different levels along the wall face are compared with field data in Figures 28 through 31. It is seen that the theoretical results agree well with the field data observed in March through May 1973 for all three levels of measurement.

The theoretical results of wall face displacement agree well with the field data at the lower part of the wall face, however, they are much smaller than the field data near the top of the wall (Figure 31).

h. Horizontal Movement in Embankment

The theoretical horizontal movements in the embankment are also plotted in Figures 21 and 23 for comparison with the field data measured by slope indicators. The results of finite element analysis agree well with the field data measured by slope indicator SI-1 in November 1972 through April 1973 (Figure 21). However, in Figure 23 only part of the theoretical results agree with the field data observed by slope indicator SI-3 in April 1973. Within a 10 to 30 feet depth, the theoretical results are much smaller than the field data (Figure 23).

## 4. Discussion of Finite Element Results

The results of the finite element study were very encouraging, in consideration of the complexity of the geometry and of the materials. The analyses show that:

a. The use of the "composite material property" in the analysis is a satisfactory approach.

b. The general trend of stress and deformation patterns agree reasonably well with the field data.

c. Further improvements of the finite element analysis program are needed which take into consideration the factors such as the edge effect by the skin plate, the number and size of construction increments, the linearity of the Poisson's ratio of the soil, the time effects, and three dimensional nature of field behavior.

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TABLE 1 - LABORATORY SOIL TEST RESULTS

| Soil Property | Slide Debris | | Borrow Material | | |
|---|---|---|---|---|---|
| | 1384-85 | 1617 | RE-2 | RE-7 | RE-8 |
| | May 1970 | June 1971 | June 1971 | April 1972 | August 1972 |
| Frictional Angle, $\phi$ | 35.5° | 44° | 37° | 38.5° | 40° |
| Cohesion C (psi) | 2.5 | 0 | 4.2 | 5.6 | 4.2 |
| Max. Dry Density, (pcf) | 141 | 141 | 141 | 143 | 139 |
| $K_a = \frac{1-\sin\phi}{1+\sin\phi}$ | 0.27 | 0.18 | 0.25 | 0.23 | 0.22 |
| $K_o = 1-\sin\phi$ | 0.42 | 0.31 | 0.40 | 0.38 | 0.36 |
| Grading | Percent Passing by Weight | | | | |
| 3" | 100 | 93 | 100 | 98 | 99 |
| 2½" | 100 | 87 | 99 | 96 | 98 |
| 2" | 99 | 79 | 98 | 94 | 97 |
| 1½" | 97 | 71 | 89 | 90 | 92 |
| 1" | 92 | 59 | 83 | 83 | 84 |
| 3/4" | 86 | 48 | 77 | 78 | 77 |
| 1/2" | 79 | 35 | 66 | - | 68 |
| 3/8" | 75 | 30 | 59 | 66 | 62 |
| #4 | 66 | 23 | 46 | 54 | 49 |
| #8 | 55 | 19 | 35 | 50 | 41 |
| #16 | 48 | 14 | 24 | 36 | 30 |
| #30 | 40 | 10 | 17 | 25 | 23 |
| #50 | 32 | 8 | 11 | 17 | 16 |
| #100 | 21 | 5 | 8 | 12 | 12 |
| #200 | 13 | 4 | 6 | 9 | 9 |

TABLE 2 - FIELD NUCLEAR GAGE DENSITY READINGS

| Date | Location | Elevation | Density Reading (PCF) | | | Average Density |
|---|---|---|---|---|---|---|
| 3-23-72 | Embankment | 6136. | 131.2 | | | 131.2 |
| 4-21-72 | " | 6225. | 124.8 | 127.8 | | 126.3 |
| 4-26-72 | " | 6246. | 125.6 | 127.0 | 127.0 | 126.5 |
| 4-28-72 | " | 6260. | 125.0 | 126.2 | 126.1 | 125.8 |
| 5-16-72 | " | 6312. | 131.0 | | | 131.0 |
| 8-3-72 | " | 6357.4 | 143.6 | 144.0 | 140.5 | 142.7 |
| 8-9-72 | " | 6361.5 | 147.0 | 142.0 | 144.5 | 144.5 |
| 8-14-72 | Instrument Trench | 6362.7 | 132.5 | 139.0 | 135.5 | 135.7 |
| 8-31-72 | Reinforced Earth Fill | 6373.8 | 142.0 | 145.0 | 142.0 | 143.0 |
| 9-8-72 | Instrument Trench | 6378.3 | 136.2 | 135.0 | | 135.6 |
| 9-13-72 | Reinforced Earth Fill | 6382.0 | 142.0 | 142.0 | 139.0 | 141.0 |
| 10-2-72 | Instrument Trench | 6400.0 | 139.5 | 130.5 | | 135.0 |
| 10-10-72 | Reinforced Earth Fill | 6406.6 | 142.0 | 142.5 | 144.0 | 142.8 |

TABLE 3: Construction Equipment and Rental Rate

| Item | Type or Model | Rental Rate | Function |
|---|---|---|---|
| Crawler Tractor | Cat. D-8 | $28.50/hr | Spreading of fill material |
| Crawler Tractor | John Deer JD-450 | $5.35/hr | Towing vibratory roller |
| Vibratory Roller | Essick V72S | $7.75/hr | Compaction of fill material |
| Road Grader | Cat | $7.50/hr | Leveling of fill material |
| Front End Loader | Cat 966 B & C | $17.00/hr | Spreading of fill material |
| Water Truck | | $11.00/hr | Moisture conditioning fill material |
| Water Monitor | | $2.00/day | Adding moisture to fill material |
| Generator | 10 KW | $1.80/hr | Provide electrical power as necessary for small tools, etc. |
| Acetylene Torch | | $2.00/day | Cutting skin and strip |
| Surveying Equipment | State supplied | | Transit & level for alignment & elevations |
| Water pump | | $4.50/day | High pressure supply to water monitor |

TABLE 4: Construction Labor Description and Hourly Rate

| Item | Description | No. of Laborers | Hourly Rate |
|---|---|---|---|
| Carpenter | Set batter boards and erect skin elements | 2 | $9.50/hr |
| Equipment Operator | Operate construction equipment such as hauling, spreading, compacting of fill material & handling of steel strips & skin elements | 4 | $9.69/hr |
| Common Laborer | Erection of skin element & steel strips, hand shoveling & hand compacting fill material near the wall face | 3 | $7.54/hr |
| Grade Setter | Insure the proper thickness & grade of fill material | 1 | $10.18/hr |

TABLE 5 - AVERAGE UNIT QUANTITIES AND COSTS

| ITEM DESCRIPTION | QUANTITY OR COST |
|---|---|
| STEEL PER SQUARE FOOT OF WALL FACE | $9.876 \times 10^{-3}$ TONS |
| STEEL PER CUBIC YARD OF FILL | 0.164 TONS |
| BORROW MATERIAL COST PER CUBIC YARD | $1.80 |
| STEEL COST PER SQ. FT. OF WALL FACE | $7.40 |
| FILL COST " " " " " " | 8.15 |
| TOTAL COST " " " " " " | 15.55 |
| STEEL COST PER CU. YD. OF WALL FILL | $4.55 |
| FILL COST PER CU. YD. " " " | 5.00 |
| TOTAL COST " " " " " " | 9.55 |

TABLE 6 - COST COMPARISON BETWEEN FOUR TYPES OF WALLS

(Cost in Dollars per Sq. Ft. of Wall Face)

| Type of Wall | Description | Height of Wall (ft) | | | | | |
|---|---|---|---|---|---|---|---|
| | | 10 | 20 | 30 | 36 | 40 | 50 |
| Reinforced Earth Wall | Cost of Wall Members | $3.70 | $4.30 | $5.20 | $6.00 | $6.60 | $8.40 |
| | Cost of Backfill | 2.40 | 3.50 | 4.50 | 5.10 | 5.60 | 6.00 |
| | Total | 6.10 | 7.80 | 9.70 | 11.10 | 12.20 | 14.40 |
| Metal Crib Wall | Cost of Wall Members | 8.50 | 9.35 | 12.00 | 15.00 | - | - |
| | Cost of Backfill | 1.50 | 2.80 | 4.10 | 4.80 | - | - |
| | Total | 10.00 | 12.15 | 16.10 | 19.80 | - | - |
| Reinforced Concrete Crib Wall | Cost of Wall Members | 9.50 | 10.50 | 13.00 | 15.60 | 17.30 | 22.30 |
| | Cost of Backfill | 3.10 | 4.50 | 5.90 | 6.80 | 7.40 | 8.00 |
| | Total | 12.60 | 15.00 | 18.90 | 22.40 | 24.70 | 30.30 |
| Reinforced Concrete Retaining Wall Type I | Cost of Wall Members | 10.50 | 13.75 | 20.80 | 26.10 | - | - |
| | Cost of Backfill | 1.20 | 2.05 | 3.05 | 3.60 | - | - |
| | Total | 11.70 | 15.80 | 23.85 | 29.70 | - | - |

TABLE 7 - INSTRUMENTATION INSTALLATION DATA

LEVEL "A"

| Item | Station 550+25 Designation No. | Station 550+25 Elevation (ft) | Station 550+25 Distance From Wall Face (ft) | Station 551+75 Designation No. | Station 551+75 Elevation (ft) | Station 551+75 Distance From Wall Face (ft) |
|---|---|---|---|---|---|---|
| Settlement Platform | SP-13 | 6391.96 | 36.5 | SP-1 | 6359.55 | 46 |
| | SP-14 | 6392.07 | 24.8 | SP-2 | 6358.83 | 31 |
| | SP-15 | 6392.12 | 16.1 | SP-3 | 6358.57 | 16 |
| | SP-16 | 6392.14 | 5.6 | SP-4 | 6358.40 | 2 |
| Soil Pressure Cell | 137 H | 6391.6 | 37.5 | 101 V | 6359.0 | 44 |
| | 138 V | 6391.6 | 39.6 | 102 H | 6359.1 | 46 |
| | 139 H | 6391.8 | 24.2 | *103 I | 6358.8 | 42 |
| | 140 V | 6391.9 | 27.8 | 104 V | 6358.4 | 32.3 |
| | 142 H | 6392.0 | 16.6 | 105 H | 6358.7 | 34.3 |
| | 141 V | 6391.9 | 19.2 | *106 I | 6358.6 | 30.5 |
| | 144 H | 6391.8 | 4.3 | 107 V | 6358.4 | 17.0 |
| | 143 V | 6391.9 | 6.6 | 108 H | 6358.5 | 18.6 |
| | | | | *109 I | 6358.5 | 15.3 |
| | | | | 110 V | 6358.2 | 5.0 |
| | | | | 111 H | 6358.3 | 6.5 |
| | | | | *112 I | 6358.5 | 3.0 |
| Extensometer | 75 | 6392.2 | 33.2 | 69 | 6359.90 | 46.5 |
| | 76 | 6392.2 | 28.3 | 68 | 6359.70 | 41.8 |
| | 83 | 6392.4 | 8.1 | 88 | 6359.38 | 31.5 |
| | 84 | 6392.4 | 12.9 | 87 | 6359.33 | 26.5 |
| | | | | 86 | 6359.00 | 11.5 |
| | | | | 85 | 6359.00 | 6.8 |
| Strain Gage on Reinforcing Strips | 17-18 | 6393.8 | 25.1 | 17-18 | 6358.5 | 30.2 |
| | 15-16 | 6393.6 | 15.1 | 15-16 | 6358.5 | 15.2 |
| | 13-14 | 6393.5 | 1.2 | 13-14 | 6358.5 | 1.1 |

NOTE: The soil pressure cell designation numbers with the asterisk (*) are Gentran cells, the rest are Glotzel cells. V, H, & I indicate vertical, horizontal, or 45° inclinations.

TABLE 8 - INSTRUMENTATION INSTALLATION DATA

LEVEL "B"

| Item | Station 550+25 Designation No. | Station 550+25 Elevation (ft) | Station 550+25 Distance from Wall Face (ft) | Station 551+75 Designation No. | Station 551+75 Elevation (ft) | Station 551+75 Distance From Wall Face (ft) |
|---|---|---|---|---|---|---|
| Settlement Platform | SP-17 | 6399.52 | 39.7 | SP-5 | 6372.04 | 44.7 |
| | SP-18 | 6399.44 | 29.5 | SP-6 | 6371.99 | 29.8 |
| | SP-19 | 6399.40 | 17.2 | SP-7 | 6371.77 | 14.9 |
| | SP-20 | 6399.14 | 5.5 | SP-8 | 6371.56 | 5.2 |
| Soil Pressure Cell | 145 V | 6399.5 | 40.5 | 113 V | 6371.6 | 45.4 |
| | 146 H | 6399.3 | 38.7 | 114 H | 6371.6 | 44.0 |
| | 147 V | 6399.4 | 30.2 | *115 I | 6371.7 | 42.4 |
| | 148 H | 6399.2 | 28.3 | 116 V | 6371.8 | 32.2 |
| | 149 V | 6399.2 | 18.2 | 117 H | 6371.6 | 30.7 |
| | 150 H | 6398.9 | 16.1 | *118 I | 6371.5 | 29.2 |
| | 151 V | 6399.0 | 8.2 | 119 V | 6371.4 | 17.0 |
| | 152 H | 6398.9 | 6.2 | 120 H | 6371.3 | 15.0 |
| | | | | *121 I | 6371.2 | 13.5 |
| | | | | 122 V | 6371.3 | 7.3 |
| | | | | 123 H | 6371.2 | 6.0 |
| | | | | *124 I | 6371.1 | 4.5 |
| Extensometer | 89 | 6399.5 | 7.9 | 73 | 6372.3 | 11.9 |
| | 90 | 6399.5 | 12.7 | 74 | 6372.4 | 16.7 |
| | 80 | 6399.7 | 28.2 | 67 | 6372.8 | 27.4 |
| | 79 | 6399.7 | 33.05 | 70 | 6372.9 | 32.2 |
| | | | | 93 | 6373.1 | 41.8 |
| | | | | 94 | 6373.1 | 46.8 |
| Strain Gage on Reinforcing Strips | 13-14 | 6400.8 | 1.5 | 13-14 | 6371.4 | 1.5 |
| | 15-16 | 6401.0 | 15.6 | 15-16 | 6371.6 | 15.0 |
| | 17-18 | 6401.0 | 25.6 | 17-18 | 6371.9 | 30.0 |

NOTE: The soil pressure cell designation numbers with the asterisk (*) are Gentran cells, the rest are Glotzel cells. V, H, & I indicate vertical, horizontal, or 45° inclinations.

TABLE 9 - INSTRUMENTATION INSTALLATION DATA

LEVEL "C"

| Item | Station 550+25 Designation No. | Station 550+25 Elevation (ft) | Station 550+25 Distance From Wall Face (ft) | Station 551+75 Designation No. | Station 551+75 Elevation (ft) | Station 551+75 Distance From Wall Face (ft) |
|---|---|---|---|---|---|---|
| Settlement Platform | SP-21 | 6407.06 | 34.5 | SP-9 | 6387.16 | 44.5 |
| | SP-22 | 6407.31 | 24.5 | SP-10 | 6387.09 | 28.7 |
| | SP-23 | 6407.37 | 14.2 | SP-11 | 6387.18 | 14.9 |
| | SP-24 | 6407.22 | 5.4 | SP-12 | 6387.14 | 4.0 |
| Soil Pressure Cell | 153 V | 6406.61 | 36.7 | 125 V | 6386.9 | 47.6 |
| | 154 H | 6406.60 | 34.4 | 126 H | 6386.9 | 45.7 |
| | 155 V | 6407.18 | 26.8 | *127 I | 6386.7 | 43.7 |
| | 156 H | 6407.06 | 24.8 | 128 V | 6386.7 | 31.8 |
| | 157 V | 6407.43 | 16.8 | 129 H | 6386.8 | 29.5 |
| | 158 H | 6407.14 | 14.4 | *130 I | 6386.8 | 27.5 |
| | 159 V | 6407.21 | 7.0 | 131 V | 6386.9 | 17.7 |
| | 160 H | 6407.00 | 4.5 | 132 H | 6387.1 | 15.9 |
| | | | | *133 I | 6387.1 | 14.2 |
| | | | | 134 V | 6387.0 | 6.5 |
| | | | | 135 H | 6387.0 | 4.7 |
| | | | | *136 I | 6387.0 | 2.9 |
| Extensometer | 71 | 6407.3 | 7.55 | 77 | 6388.2 | 7.2 |
| | 72 | 6407.3 | 12.8 | 78 | 6388.2 | 12.1 |
| | 91 | 6407.2 | 28.05 | 81 | 6388.1 | 26.6 |
| | 92 | 6407.0 | 32.9 | 82 | 6388.0 | 31.5 |
| | | | | 95 | 6388.0 | 42.2 |
| | | | | 96 | 6388.0 | 47.1 |
| Strain Gages on Reinforcing Strips | 13-14 | 6408.79 | 1.05 | 13-14 | 6387.1 | 1.2 |
| | 15-16 | 6408.81 | 15.10 | 15-16 | 6387.3 | 15.0 |
| | 17-18 | 6408.58 | 25.20 | 17-18 | 6387.0 | 30.0 |

NOTE: The soil pressure cell designation numbers with the asterisk (*) are Gentran cells, the rest are Glotzel cells. V, H, & I indicate vertical, horizontal, or 45° inclinations.

TABLE 10 - SLOPE INDICATOR INSTALLATION DATA

a. SLOPE INDICATOR HOLE ELEVATIONS

| Description | SI No. 1 | SI No. 2 | SI No. 3 |
|---|---|---|---|
| Surface of slide debris | 6122.0 | 6156.0 | 6249.0 |
| Top of bedrock | 6097.0 | 6140.5 | 6192.0 |
| Bottom of hole | 6092.0 | 6136 | 6188.0 |

b. INSTALLATION DATA OF SLOPE INDICATOR CASING

| Description | SI No. 1 | | SI No. 2 | | SI No. 3 | |
|---|---|---|---|---|---|---|
| Installation date of casing No. 1 | 12-17-71 | | 3-13-72 | | 3-25-72 | |
| Coordinates at top of casing surveyed on 3-29-72 | Casing No. 12 | N4238750.01 E4332717.86 | Casing No. 6 | N4238784.07 E4332829.48 | Casing No. 12 | N4238811.29 E4333024.98 |
| Elevation at top of casing | | 6156.86 | | 6167.65 | | 6254.63 |
| Bottom of casing | El. 6094.89 | | El. 6136.44 | | El. 6189.32 | |

TABLE 11 - IDENTIFICATION OF SOIL SAMPLES

| Sample No. | Material | Elevation | Description |
|---|---|---|---|
| 1384-85 | Slide Debris | 6150-6410 | Loose granular combination of cobbles and sand. Located immediately below embankment material. |
| RE-8 | Embankment | 6150-6356 | Weathered Gneiss embankment compacted above slide debris. Forms R.E. wall foundation. |
| RE-7 | R.E. Backfill | 6356-6400 | Weathered Gneiss backfill used in R.E. wall construction. 10" maximum material. |

TABLE 12 - SHEAR STRENGTH PARAMETERS

| Sample Number | Percent Compaction | Peak Value Criteria | | 15% Strain Criteria | | Ultimate Deviator Stress Criteria | | Triaxial Test |
|---|---|---|---|---|---|---|---|---|
| | | ø Degrees | c (PSF) | ø Degrees | c (PSF) | ø Degrees | c (PSF) | |
| 1384-85 | 90 | 35.5 | 400 | 39 | 200 | 40 | 0 | CD |
| | 90 | 34 | 400 | 34 | 400 | 30 | 0 | CU[e] |
| RE-7 | 95 | 38.5 | 800 | 39 | 800 | 39.5 | 1000 | CD |
| RE-8 | 95 | 40 | 600 | 40 | 600 | 40 | 900 | CD |

TABLE 13 - TANGENT MODULUS VALUES

| Sample No. | Fill Height | Initial Modulus, $E_i$ (PSF) | Tangent Modulus, $E_T$ (PSF) |
|---|---|---|---|
| 1384-85 | 5 | $5.97 \times 10^5$ | $1.92 \times 10^4$ |
| | 10 | $6.40 \times 10^5$ | $2.05 \times 10^4$ |
| | 15 | $6.82 \times 10^5$ | $2.18 \times 10^4$ |
| | 20 | $7.24 \times 10^5$ | $2.31 \times 10^4$ |
| | 25 | $7.67 \times 10^5$ | $2.45 \times 10^4$ |
| | 50 | $9.78 \times 10^5$ | $3.12 \times 10^4$ |
| | 100 | $1.40 \times 10^6$ | $4.47 \times 10^4$ |
| | 200 | $2.25 \times 10^6$ | $7.17 \times 10^4$ |
| | 300 | $3.09 \times 10^6$ | $9.87 \times 10^4$ |
| RE-7 | 5 | $1.53 \times 10^6$ | $7.41 \times 10^5$ |
| | 10 | $1.61 \times 10^6$ | $5.02 \times 10^5$ |
| | 15 | $1.70 \times 10^6$ | $3.88 \times 10^5$ |
| | 20 | $1.79 \times 10^6$ | $3.24 \times 10^5$ |
| | 25 | $1.88 \times 10^6$ | $2.84 \times 10^5$ |
| | 50 | $2.31 \times 10^6$ | $2.09 \times 10^5$ |
| | 75 | $2.75 \times 10^6$ | $1.93 \times 10^5$ |
| RE-8 | 5 | $1.19 \times 10^6$ | $5.36 \times 10^5$ |
| | 10 | $1.38 \times 10^6$ | $3.88 \times 10^5$ |
| | 15 | $1.56 \times 10^6$ | $3.20 \times 10^5$ |
| | 20 | $1.75 \times 10^6$ | $2.84 \times 10^5$ |
| | 25 | $1.94 \times 10^6$ | $2.63 \times 10^5$ |
| | 50 | $2.88 \times 10^6$ | $2.35 \times 10^5$ |
| | 100 | $4.76 \times 10^6$ | $2.65 \times 10^5$ |
| | 150 | $6.65 \times 10^6$ | $3.15 \times 10^5$ |
| | 200 | $8.53 \times 10^6$ | $3.70 \times 10^5$ |
| | 300 | $1.23 \times 10^7$ | $4.85 \times 10^5$ |

TABLE 14 - TANGENT POISSON'S RATIO PARAMETERS

| Sample Number | Percent Compaction | Confining Pressure (PSI) | f | d | $\nu_i$ | G | F | d |
|---|---|---|---|---|---|---|---|---|
| 1384-85 | 90 | 6.94 | .554 | .418 | .55 | 0.44 | 0.36 | 1.63 |
| | | 14.0 | .432 | 1.04 | .43 | | | |
| | | 28.1 | .384 | 1.40 | .38 | | | |
| | | 56.1 | .211 | 3.67 | .21 | | | |
| RE-7 | 95 | 6.94 | .526 | .218 | .53 | 0.42 | 0.34 | 1.80 |
| | | 15.0 | .423 | 1.12 | .42 | | | |
| | | 30.0 | .271 | 2.75 | .27 | | | |
| | | 60.0 | .238 | 3.13 | .24 | | | |
| RE-8 | 95 | 8.06 | .408 | 1.77 | .41 | 0.39 | 0.24 | 2.64 |
| | | 15.0 | .466 | .751 | .47 | | | |
| | | 30.0 | .297 | 2.69 | .30 | | | |
| | | 60.0 | .219 | 5.37 | .22 | | | |

TABLE 15 - TANGENT POISSON'S RATIO VALUES

| Fill Height (Ft) | Confining Pressure (TSF) | Initial Poisson's Ratio, $\nu_i$ | | | Tangent Poisson's Ratio, $\nu_T$ | | |
|---|---|---|---|---|---|---|---|
| | | #1384-85 | #RE-7 | #RE-8 | #1384-85 | #RE-7 | #RE-8 |
| 5 | .13 | .773 | .726 | .611 | .784 | .727 | .613 |
| 10 | .26 | .664 | .624 | .538 | .682 | .626 | .541 |
| 15 | .38 | .601 | .564 | .495 | .624 | .568 | .500 |
| 20 | .51 | .556 | .522 | .464 | .582 | .527 | .471 |
| 25 | .64 | .521 | .489 | .441 | .551 | .495 | .448 |
| 50 | 1.28 | .413 | .388 | .367 | .450 | .397 | .378 |
| 75 | 1.92 | .349 | .328 | .324 | .389 | .340 | .337 |
| 100 | 2.55 | .304 | .286 | .294 | .344 | .298 | .307 |
| 150 | 3.83 | .241 | .226 | .251 | .278 | .239 | .264 |
| 200 | 5.11 | .196 | .184 | .220 | .229 | .196 | .233 |
| 250 | 6.39 | .161 | .151 | .197 | .189 | .162 | .208 |
| 300 | 7.66 | .133 | .125 | .177 | .157 | .134 | .188 |

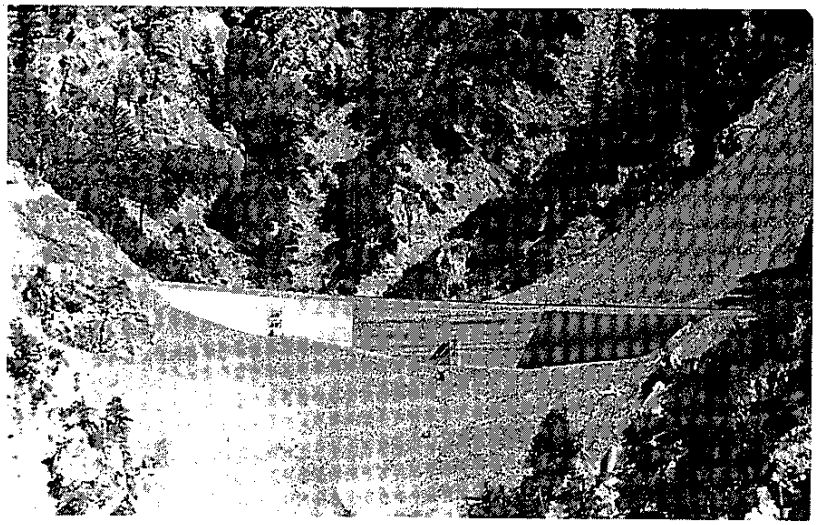


Photo 1 - Completed view of the reinforced earth embankment

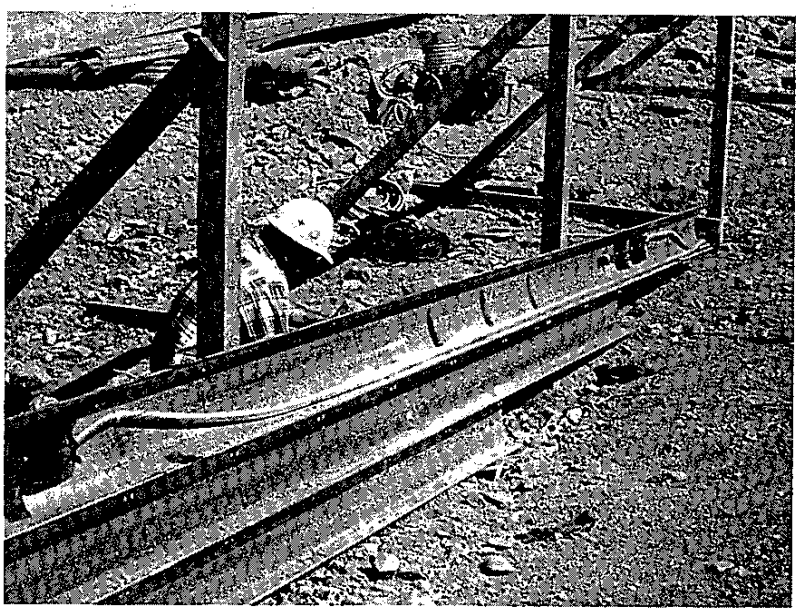


Photo 2 - Batter boards and instrumented skin element

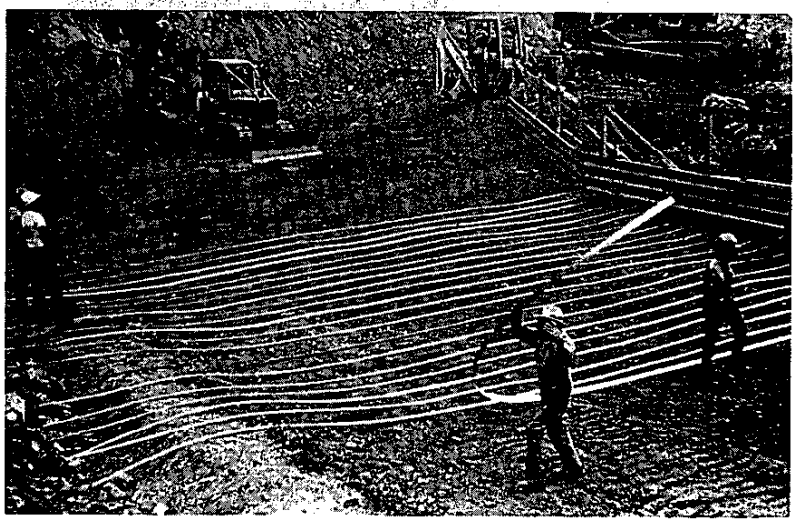


Photo 3 - Placing reinforcing strips

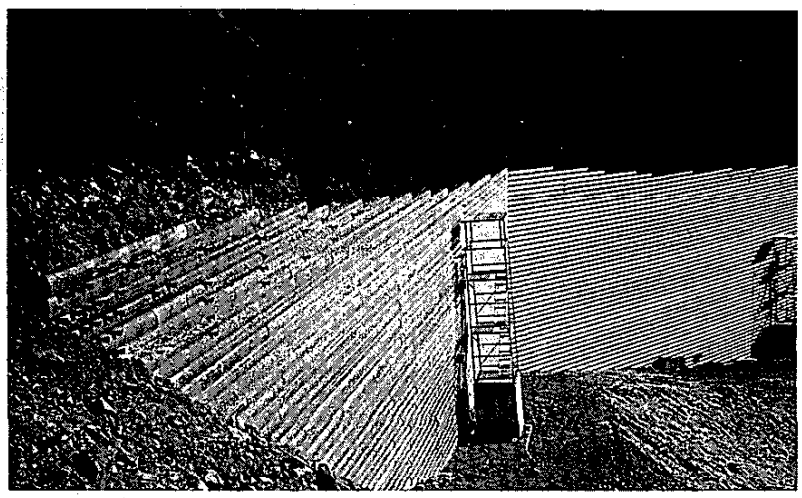


Photo 4 - Completed wall face with wooden wedges between skin elements and instrumentation shelters on berm

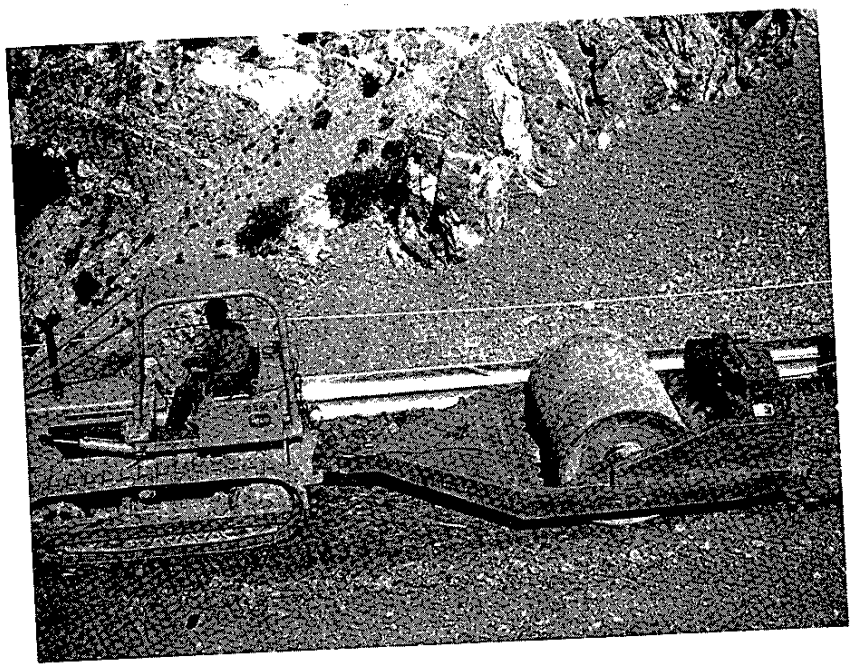


Photo 5 - Compaction operation

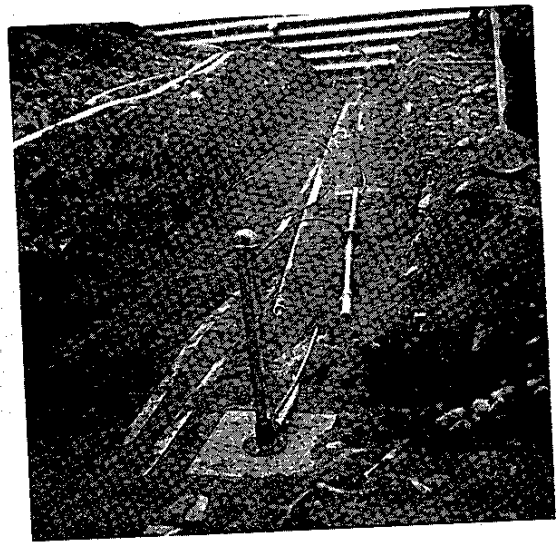


Photo 6 - Instrumentation Trench with settlement platform in place

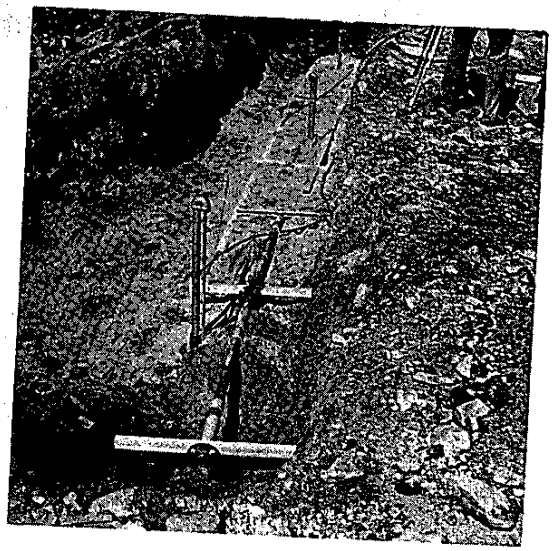


Photo 7 - Extensometer installed

Photo 8

a. Installation of soil pressure cell

b. Soil pressure cell on vertical, horizontal and inclined planes

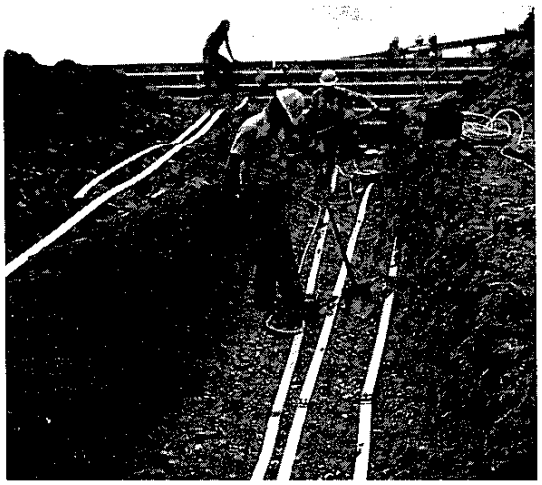


Photo 9 - Instrumented reinforcing strips with strain gages protected by sand

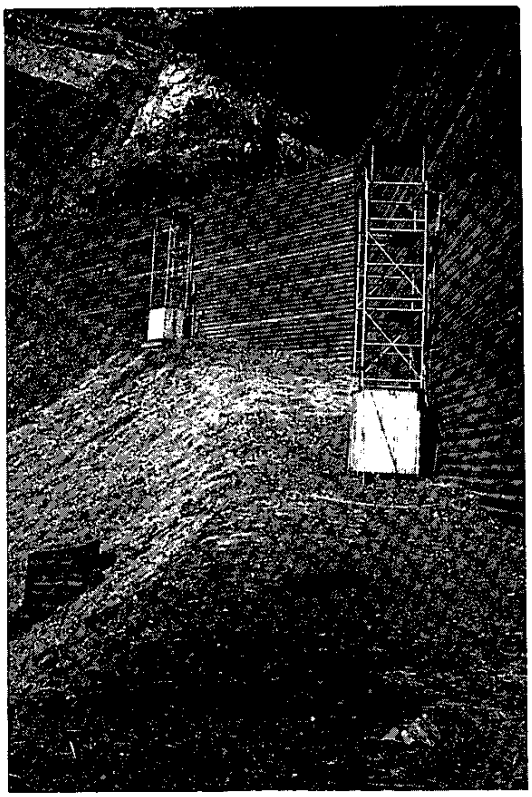


Photo 10 - Instrumentation shelters at three locations for housing the readout devices

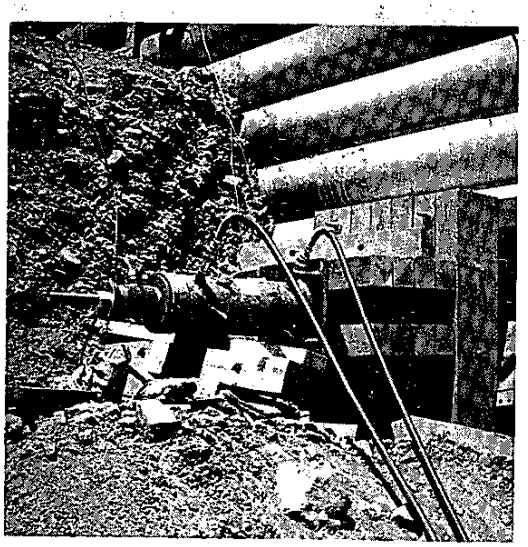


Photo 11 - Hydraulic jack acting against wooden bearing pad

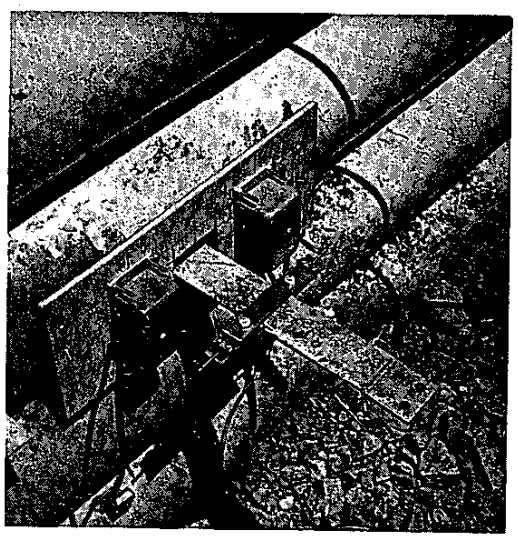


Photo 12 - Dummy steel strip with two extensometers fastened at each side

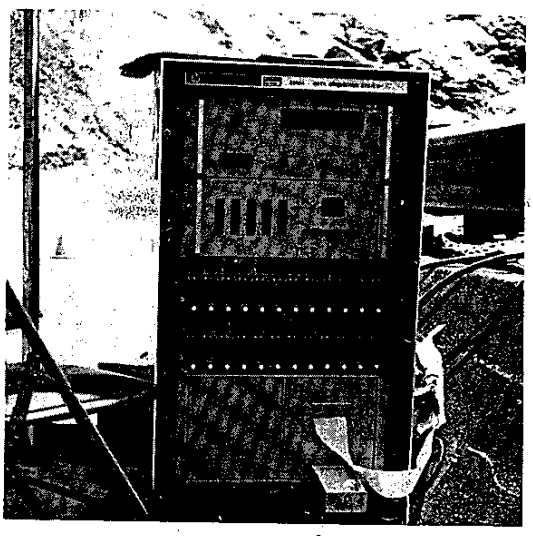


Photo 13 - Data acquisition system utilized during pulling tests

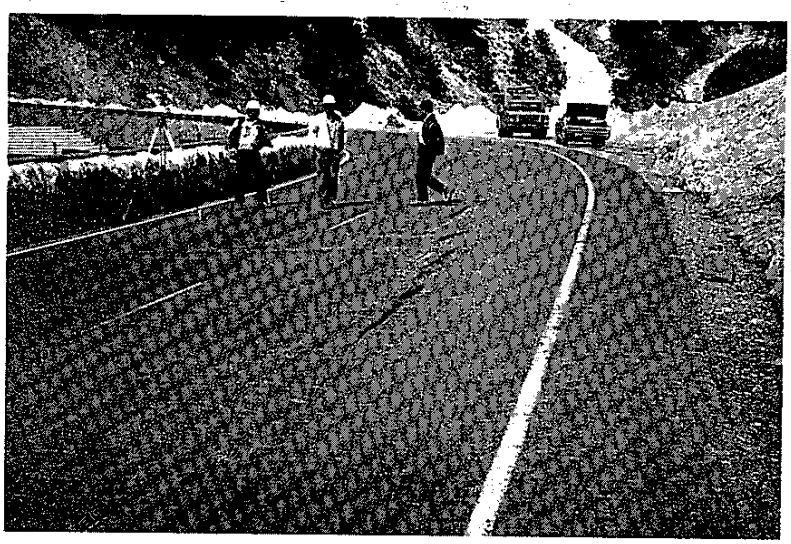


Photo 14 - Pavement cracks observed behind the reinforced earth fill in April 1973 Station 552+90 - 553+75

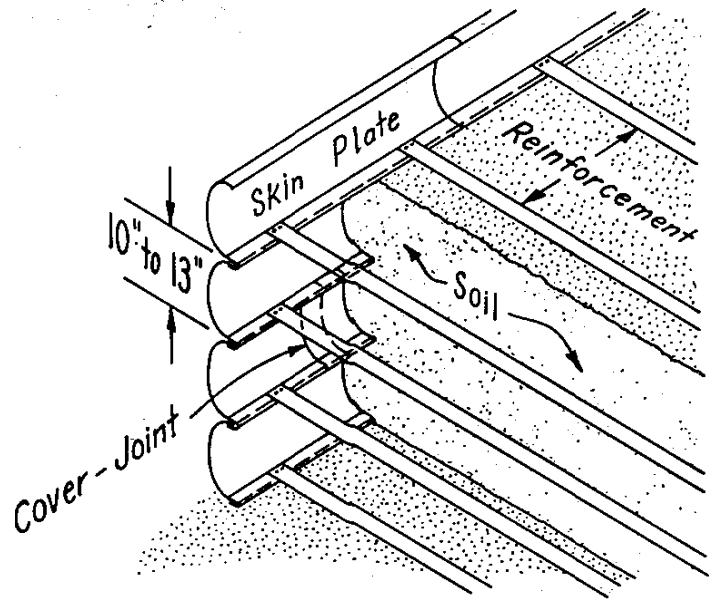



Figure 1 SCHEMATIC OF REINFORCED EARTH FILL

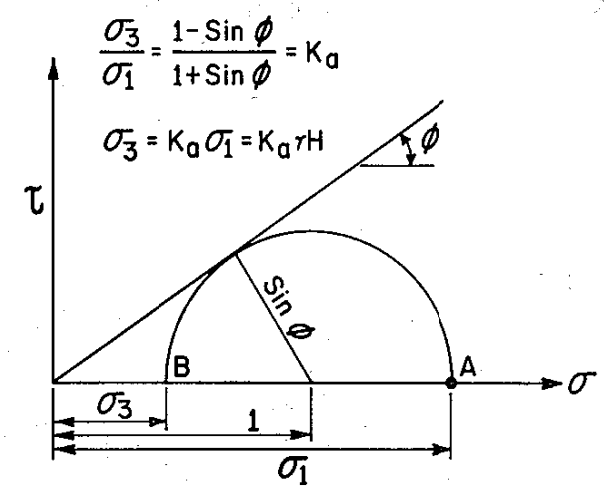



Figure 4 MOHR CIRCLE (AT IMMINENT FAILURE)

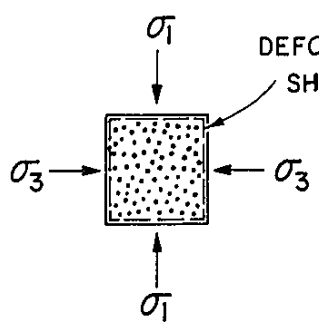



Figure 2 SAND CUBE ($\sigma_1 = \sigma_3$)

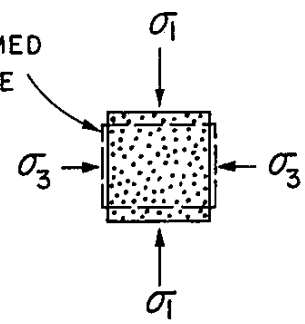



Figure 3 SAND CUBE ($\sigma_1 > \sigma_3$)

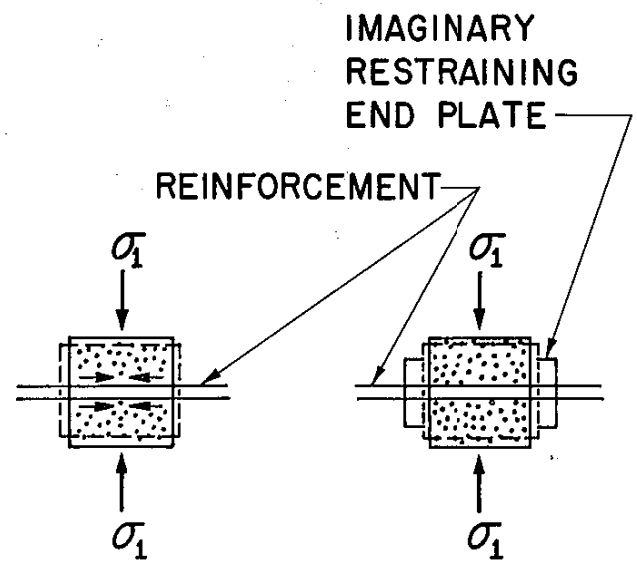



Figure 5 REINFORCED SOIL ELEMENT

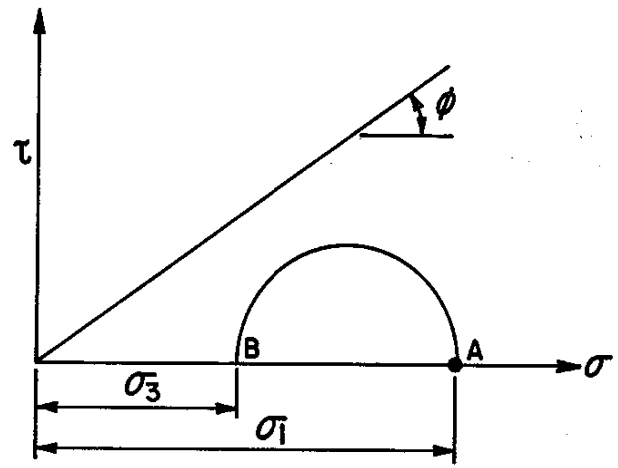



Figure 6

MOHR CIRCLE (WITHOUT IMMINENT FAILURE)

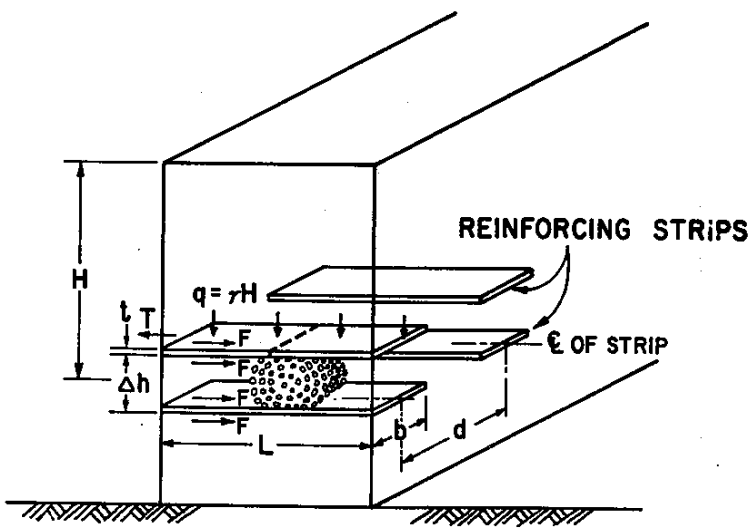
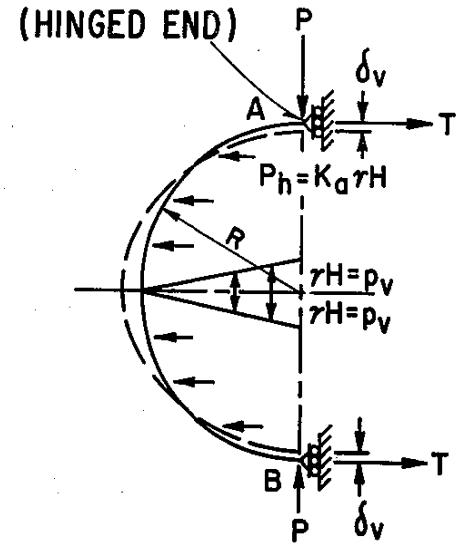



Figure 7

SCHEMATIC OF REINFORCED EARTH BLOCK



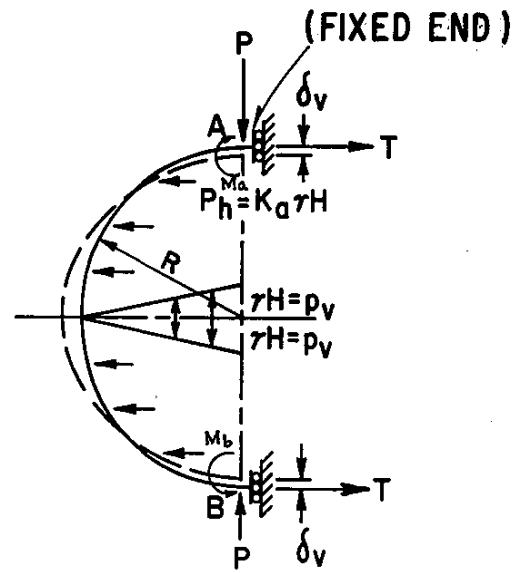
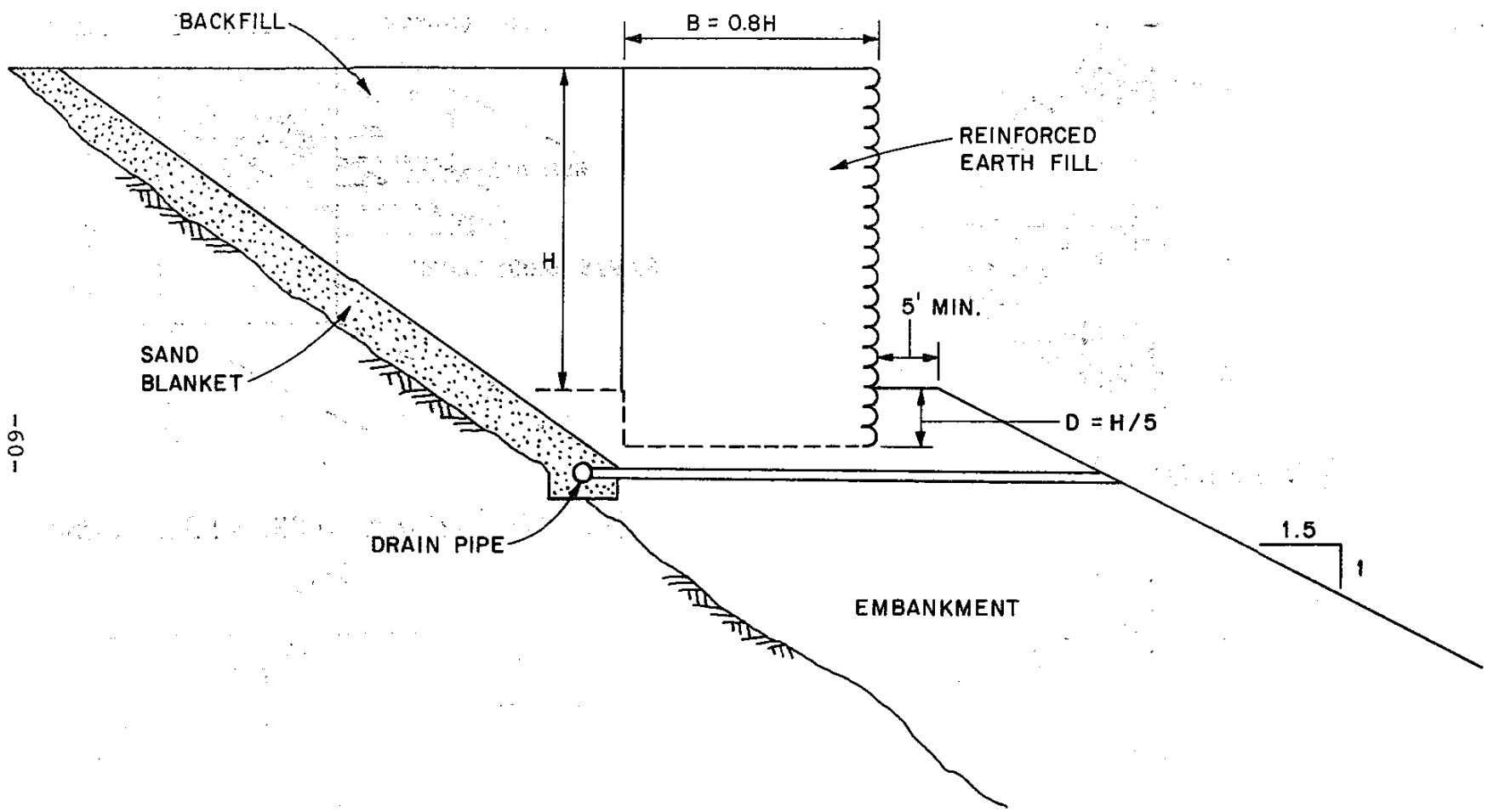




Figure 8

LOADING DIAGRAM ON SKIN PLATE




STABILITY REQUIREMENTS
(RULE OF THUMB)

Figure 9

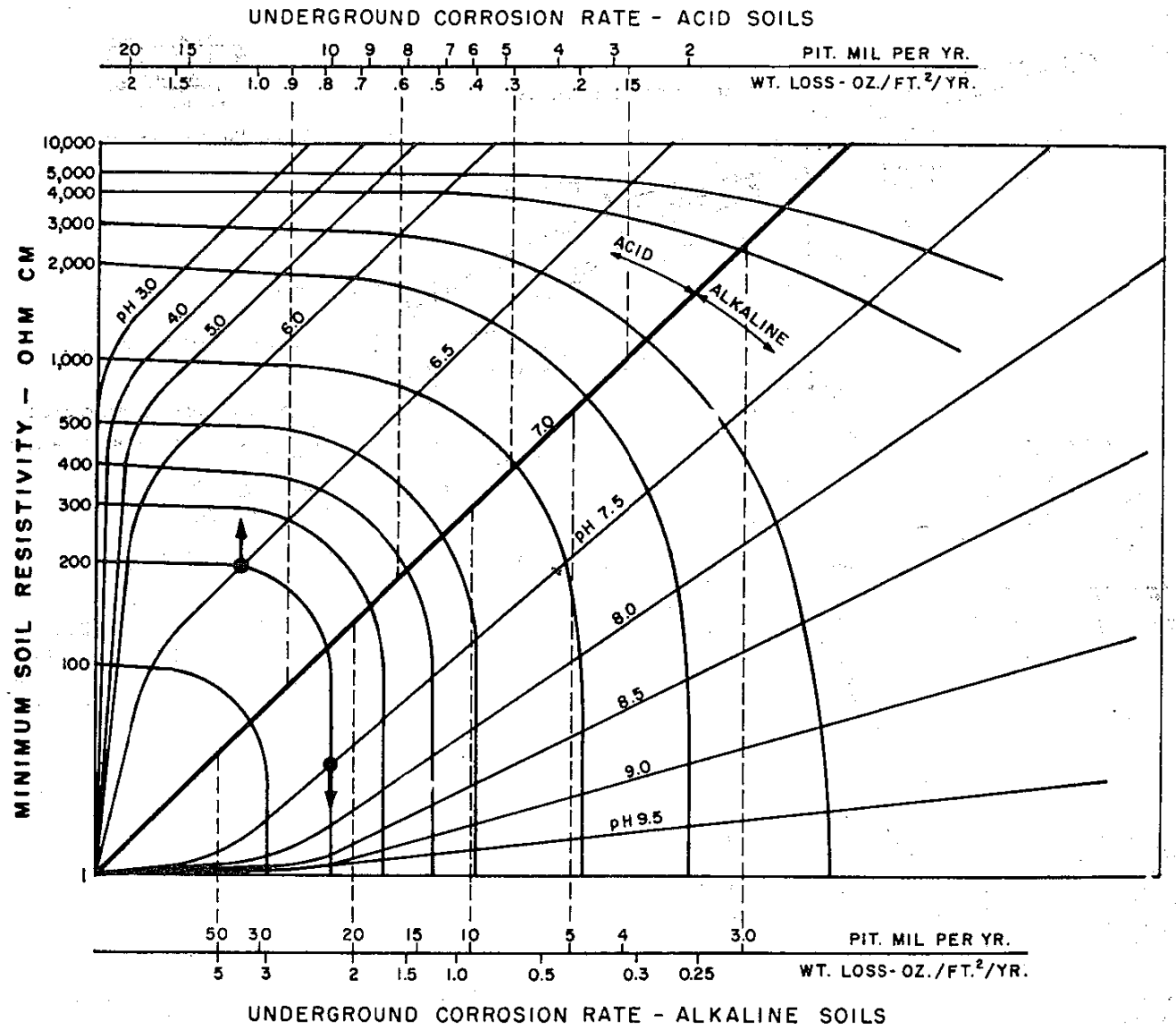
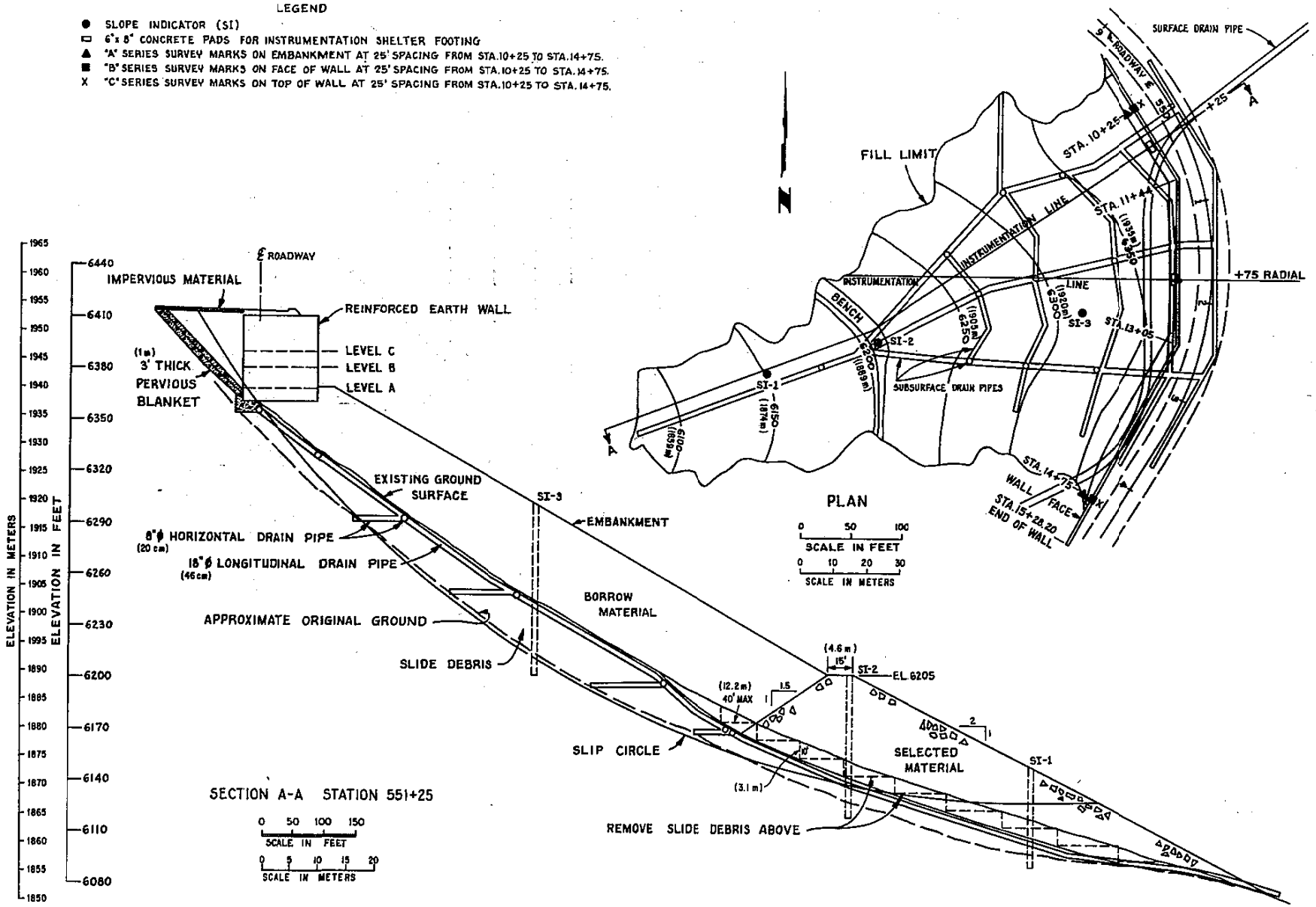



Figure 10—Chart for estimating corrosion rate of steel pipe. Example 1: with pH of 6.5 and resistivity of 200 ohm cm, the underground pipe loss is about 1.0 oz/sq ft/yr and the pitting rate about 0.013 ipy. Example 2: with pH of 7.5 and resistivity of 200 ohm cm, the underground pipe loss is about 2.2 oz; sq ft/yr and the pitting rate is about 0.022 ipy.




PLAN AND SECTION

FIGURE 11

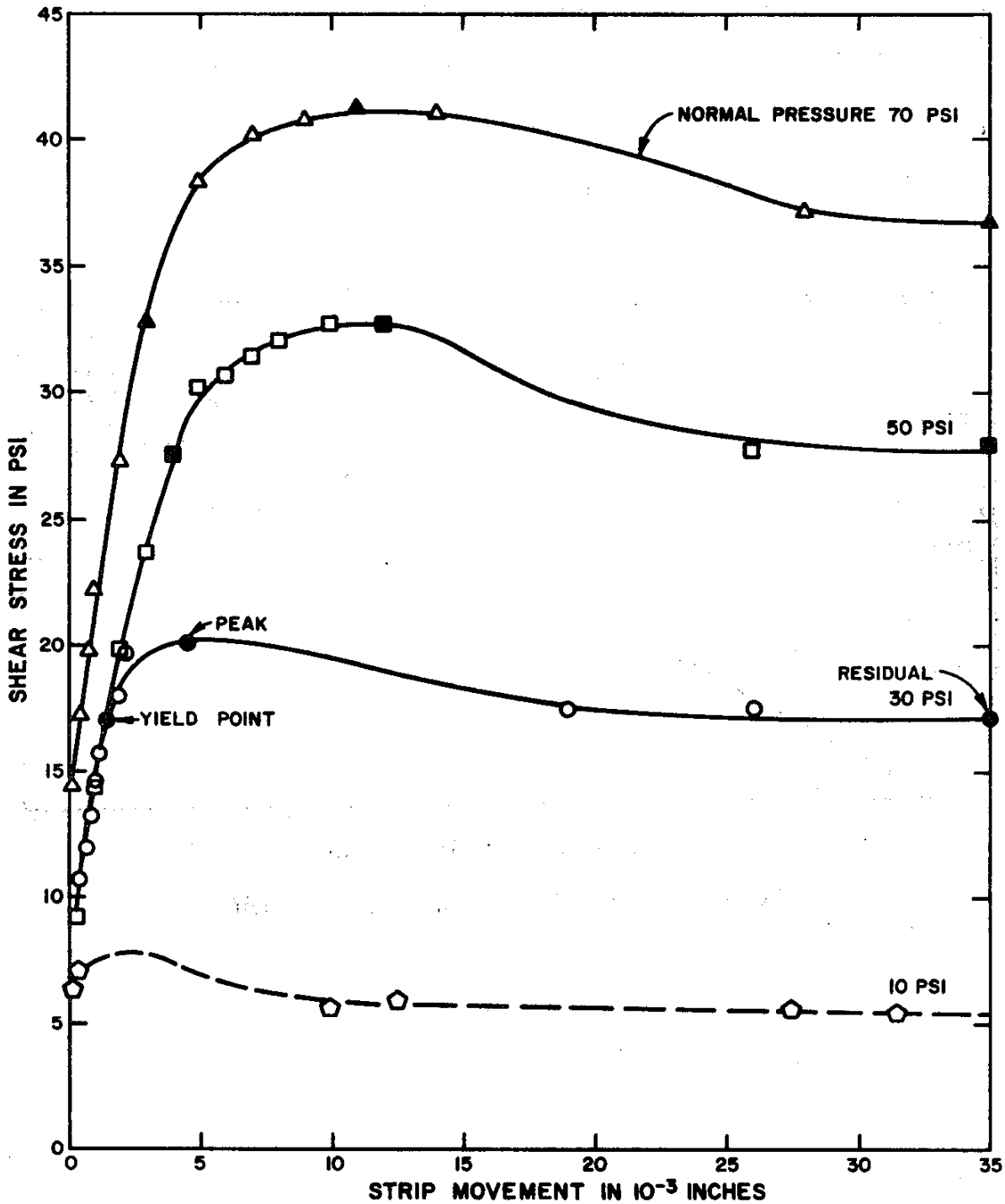



Figure 12: STRESS-DEFORMATION CURVE FROM LABORATORY PULLING TESTS

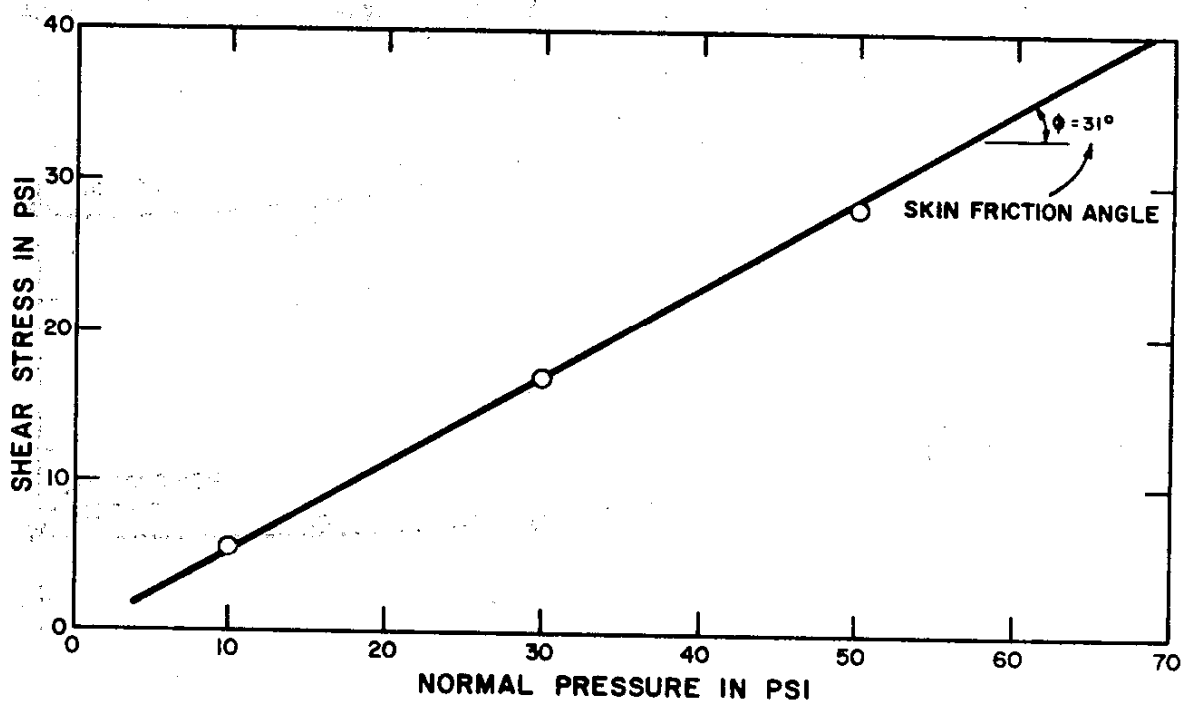



**Figure 13: SKIN FRICTION ENVELOPE LINE**

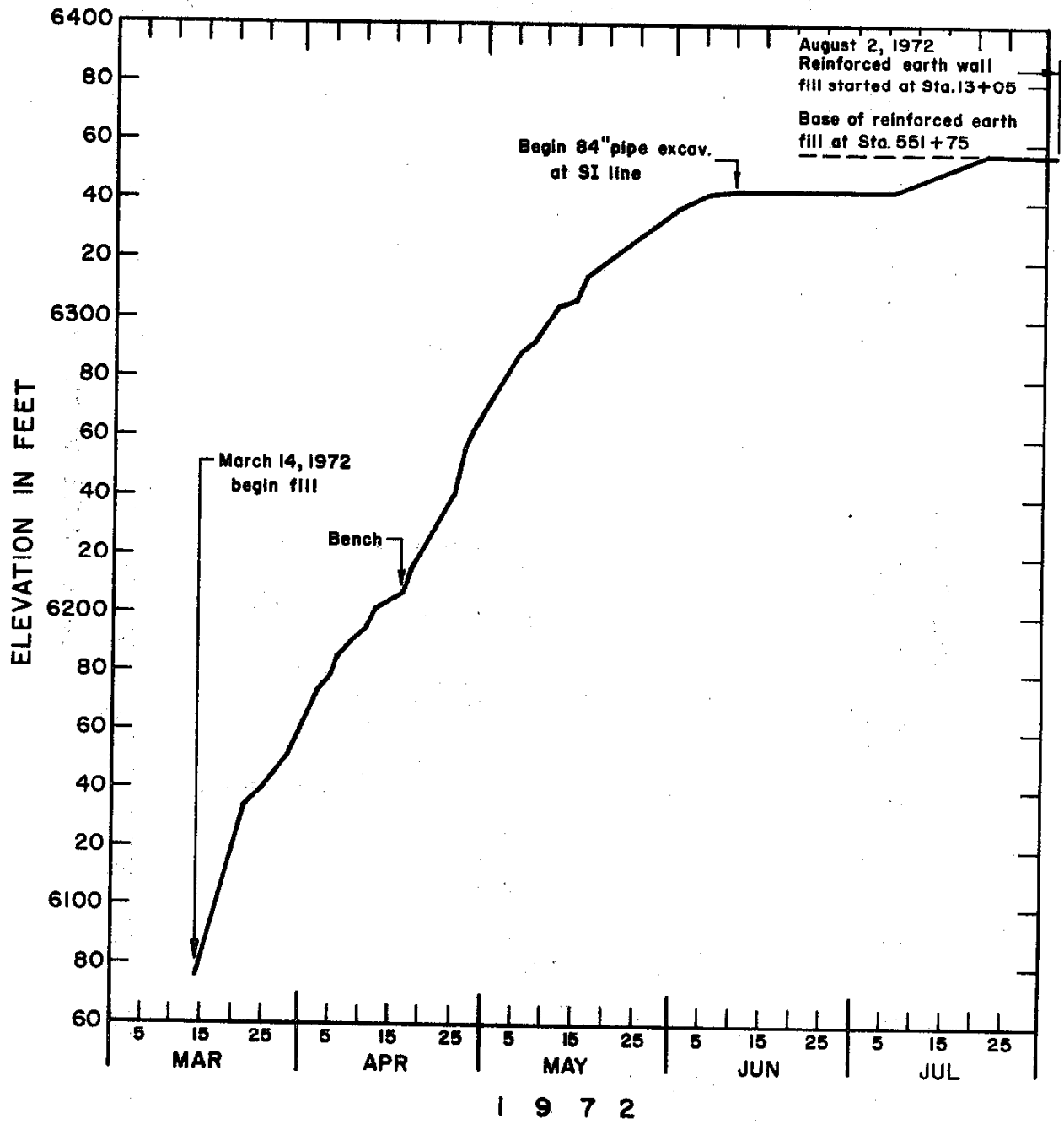
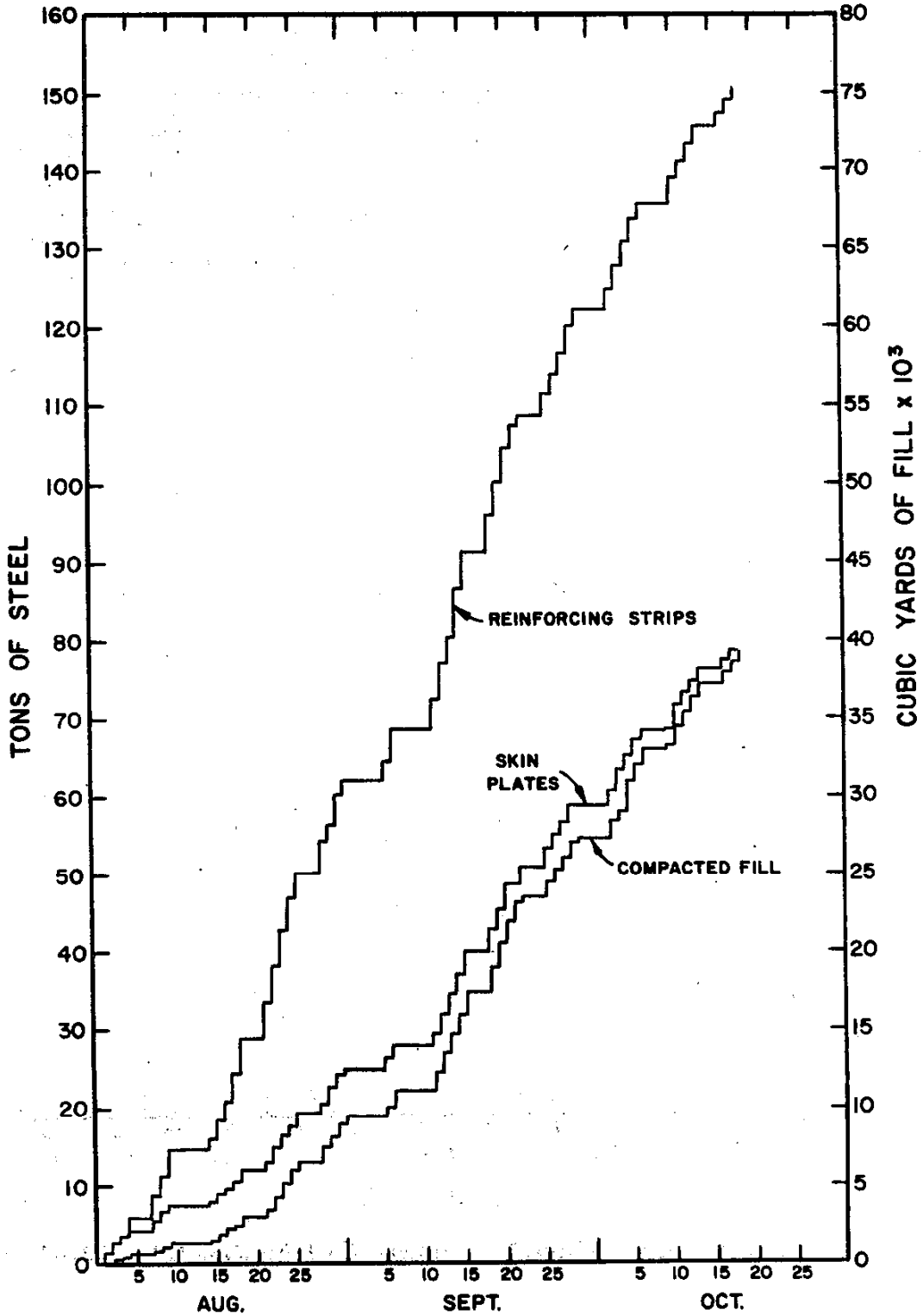


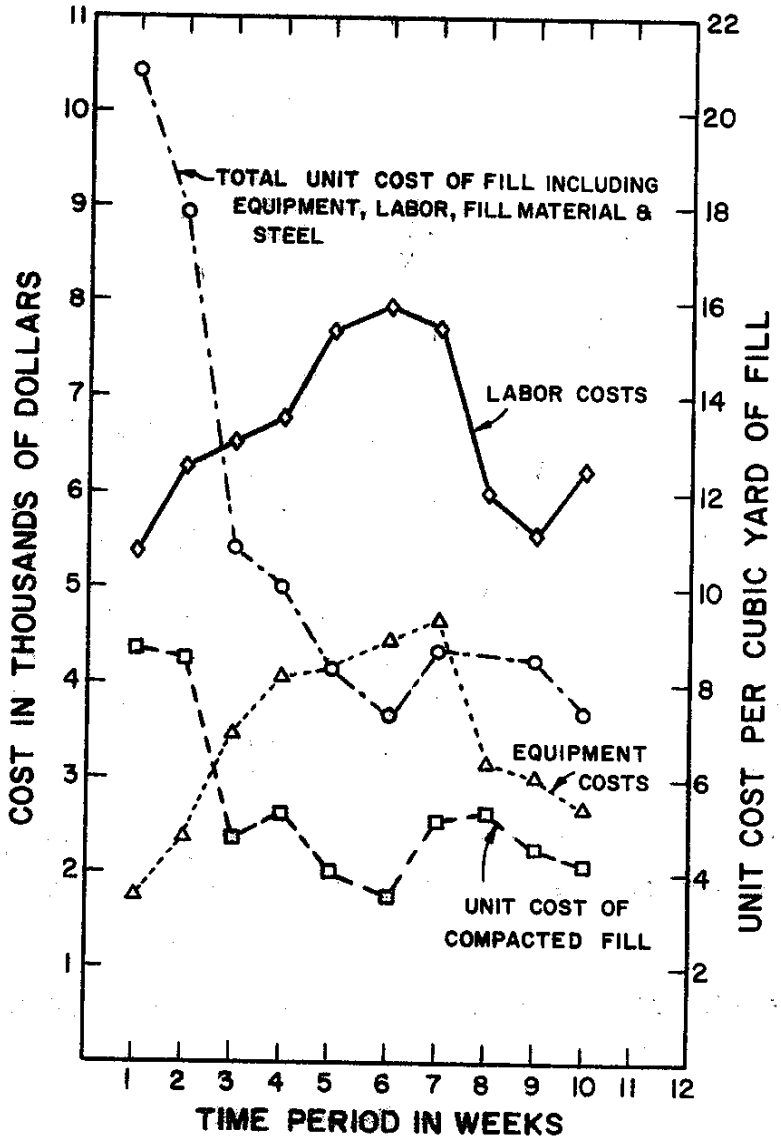

Figure 14: DAILY RECORD OF HEIGHT DURING EMBANKMENT CONSTRUCTION




DAILY RECORD OF CONSTRUCTION QUANTITIES

Figure 15

NOTE (1) EACH WEEK IS COMPOSED OF FIVE WORK DAYS.
(2) ALL COSTS PLOTTED ARE THE TOTAL COSTS IN EACH WEEK.
(3) UNIT COSTS PLOTTED ARE THE AVERAGE UNIT COSTS WITHIN EACH WEEK.




WEEKLY RECORD OF CONSTRUCTION COSTS

Figure 16

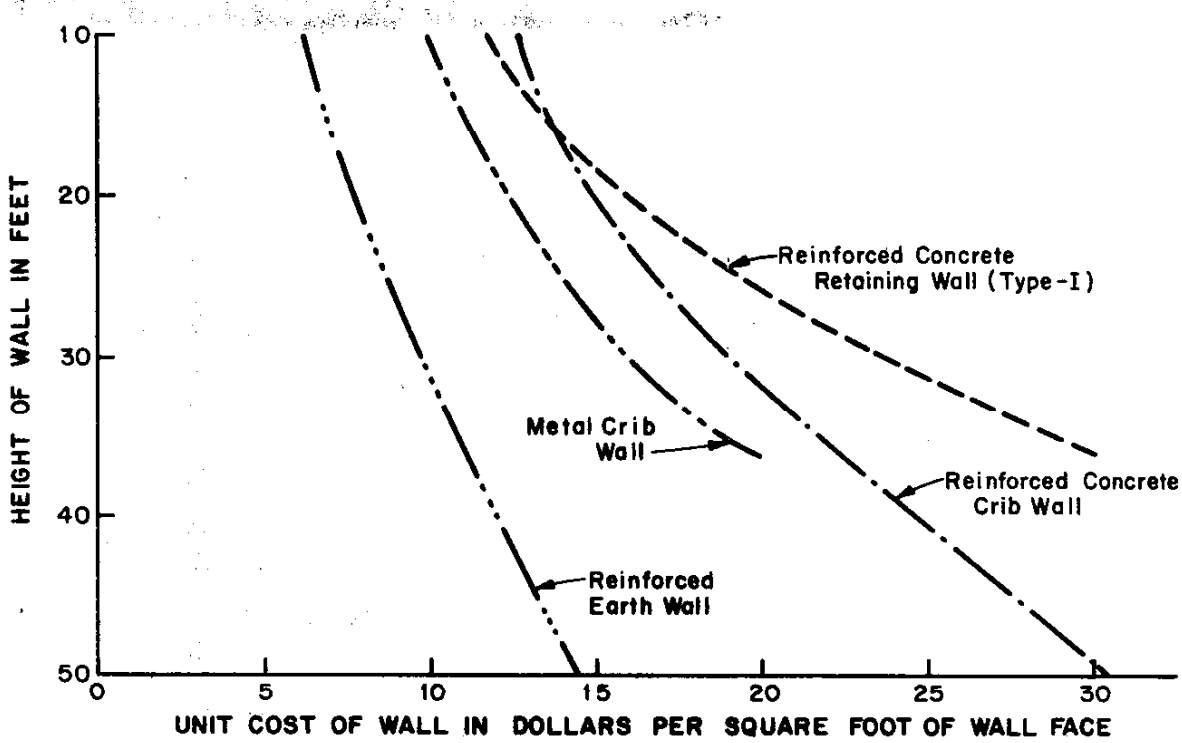
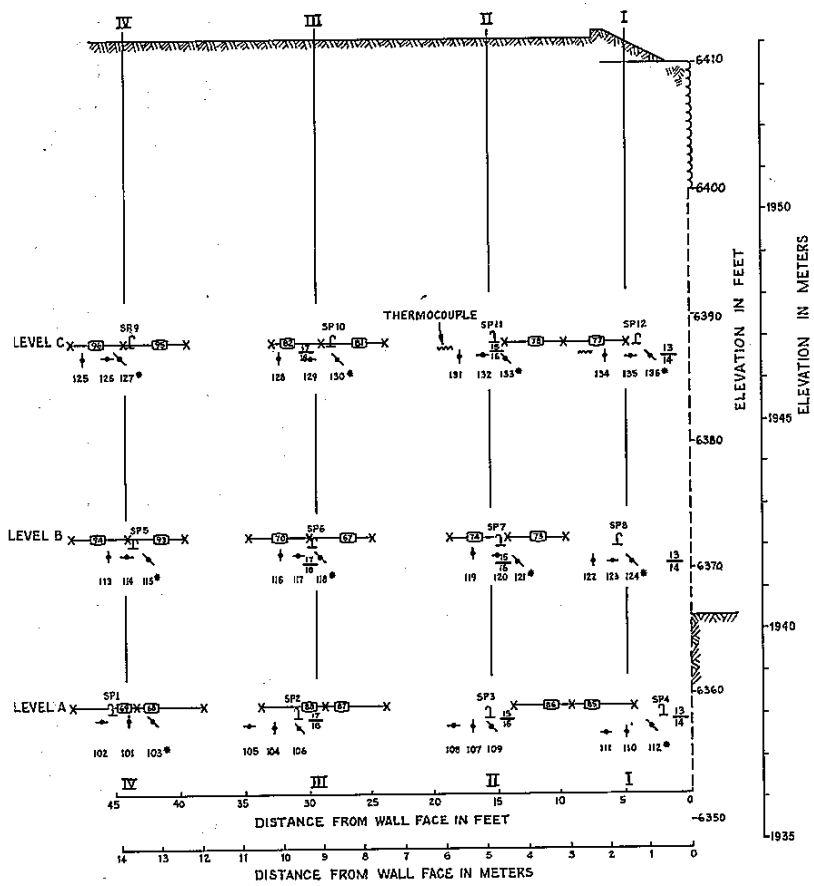
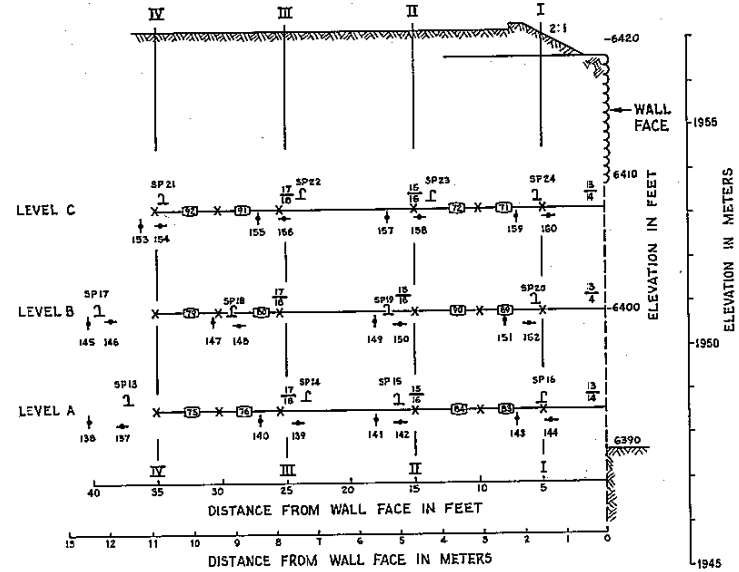



Figure 17: COST COMPARISON BETWEEN FOUR TYPES OF WALLS




INSTRUMENTATION SECTION
STA 551+75




INSTRUMENTATION SECTION
STA 550+25

LEGEND

SP9 SETTLEMENT PLATFORM
95—X EXTENSOMETER
17/18 STRAIN GAGE ON STRIP
116 117 118* PRESSURE CELLS WITH CORRESPONDING IDENTIFICATION NUMBER BENEATH THE CELL. CELL I.D. NUMBERS WITH ASTERISK (*) INDICATE A GENTRAN PRESSURE CELL. ALL OTHERS ARE GLOETZL PRESSURE CELLS.

# INSTRUMENTATION SECTIONS

FIGURE 18

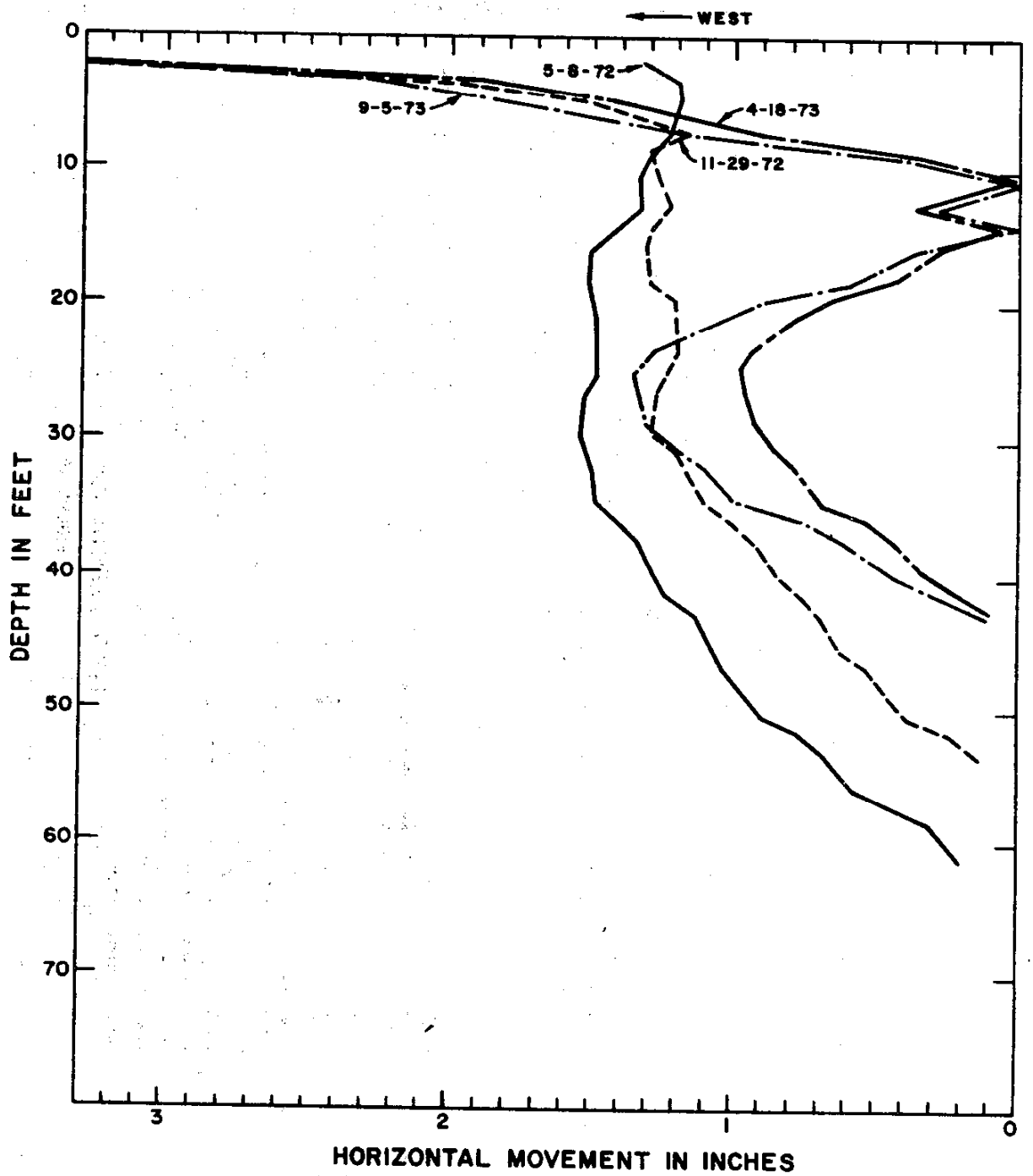



Figure 19: HORIZONTAL MOVEMENT IN THE E-W DIRECTION MEASURED BY SLOPE INDICATOR SI-1

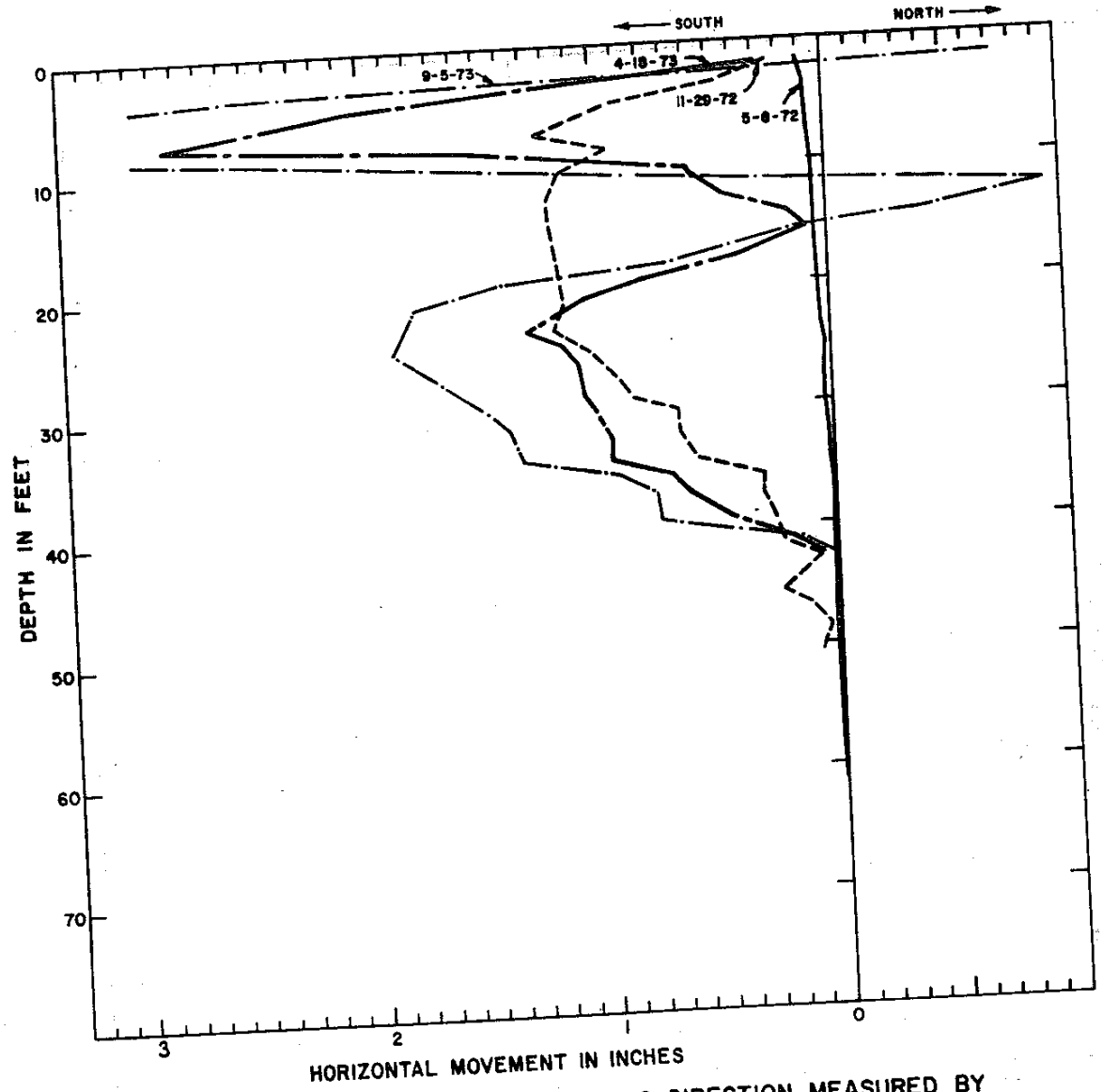



Figure 20: HORIZONTAL MOVEMENT IN THE N-S DIRECTION MEASURED BY SLOPE INDICATOR SI-1

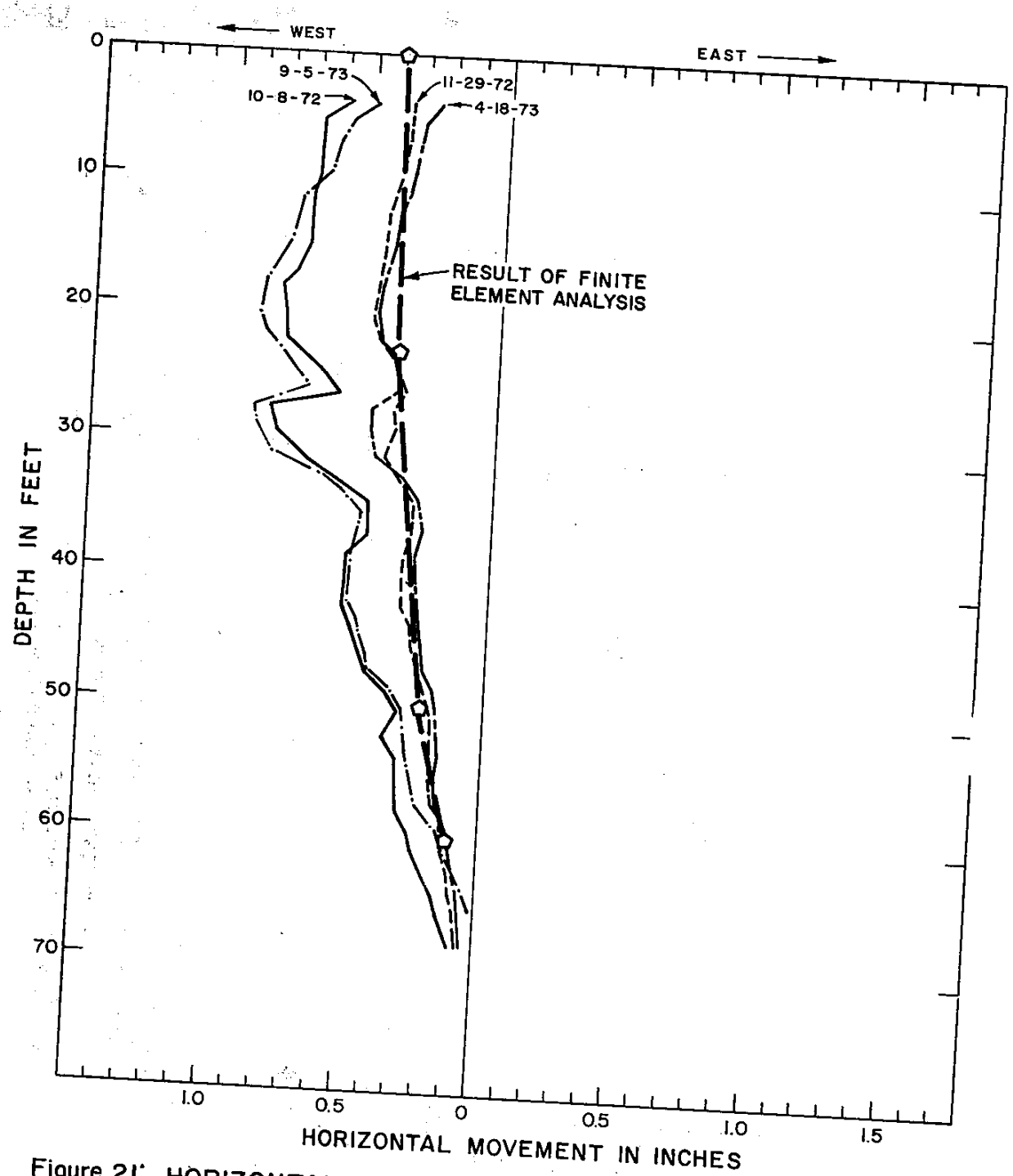



Figure 21: HORIZONTAL MOVEMENT IN THE E-W DIRECTION MEASURED BY SLOPE INDICATOR SI-2

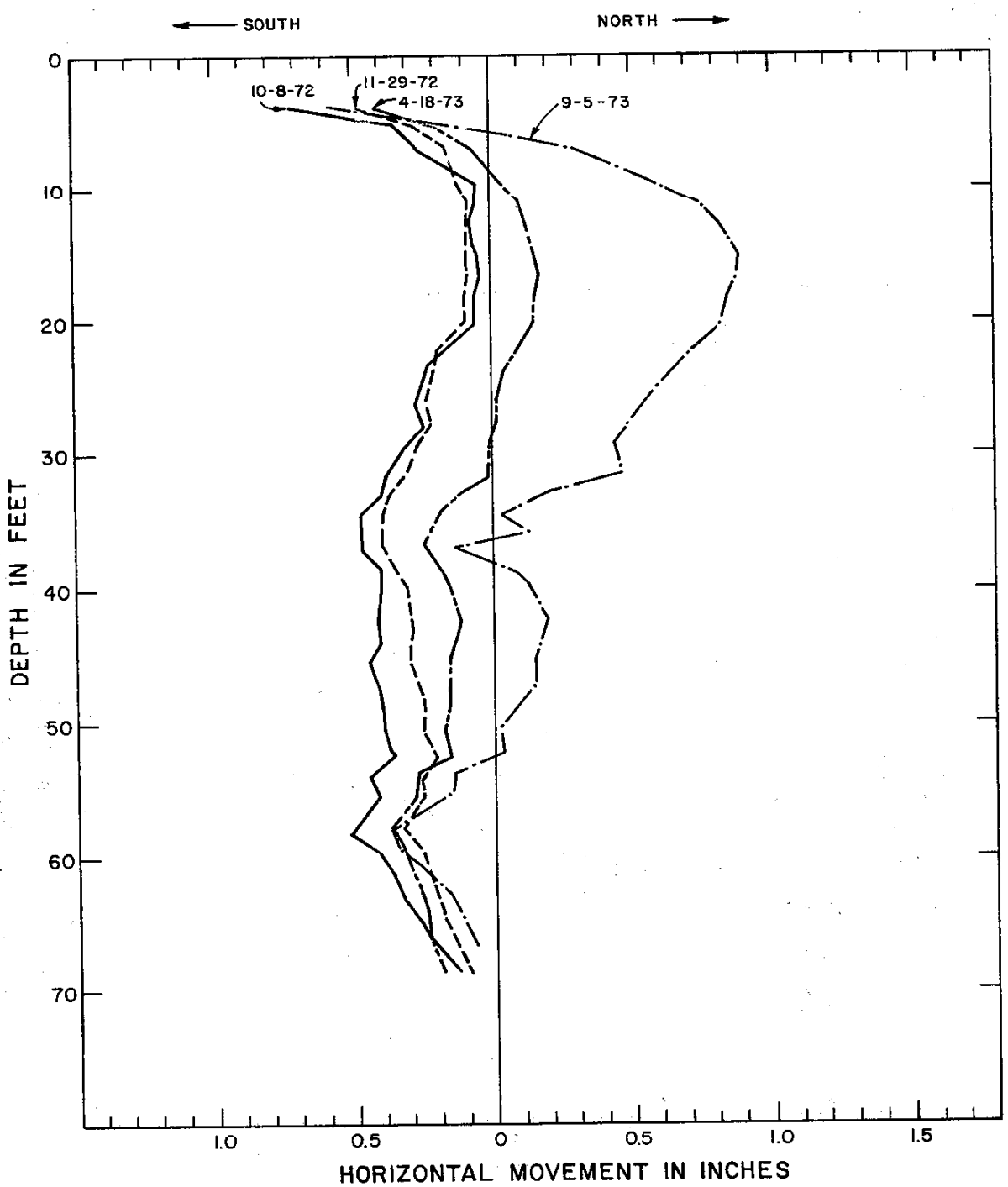



Figure 22: HORIZONTAL MOVEMENT IN THE N-S DIRECTION MEASURED BY SLOPE INDICATOR SI-2

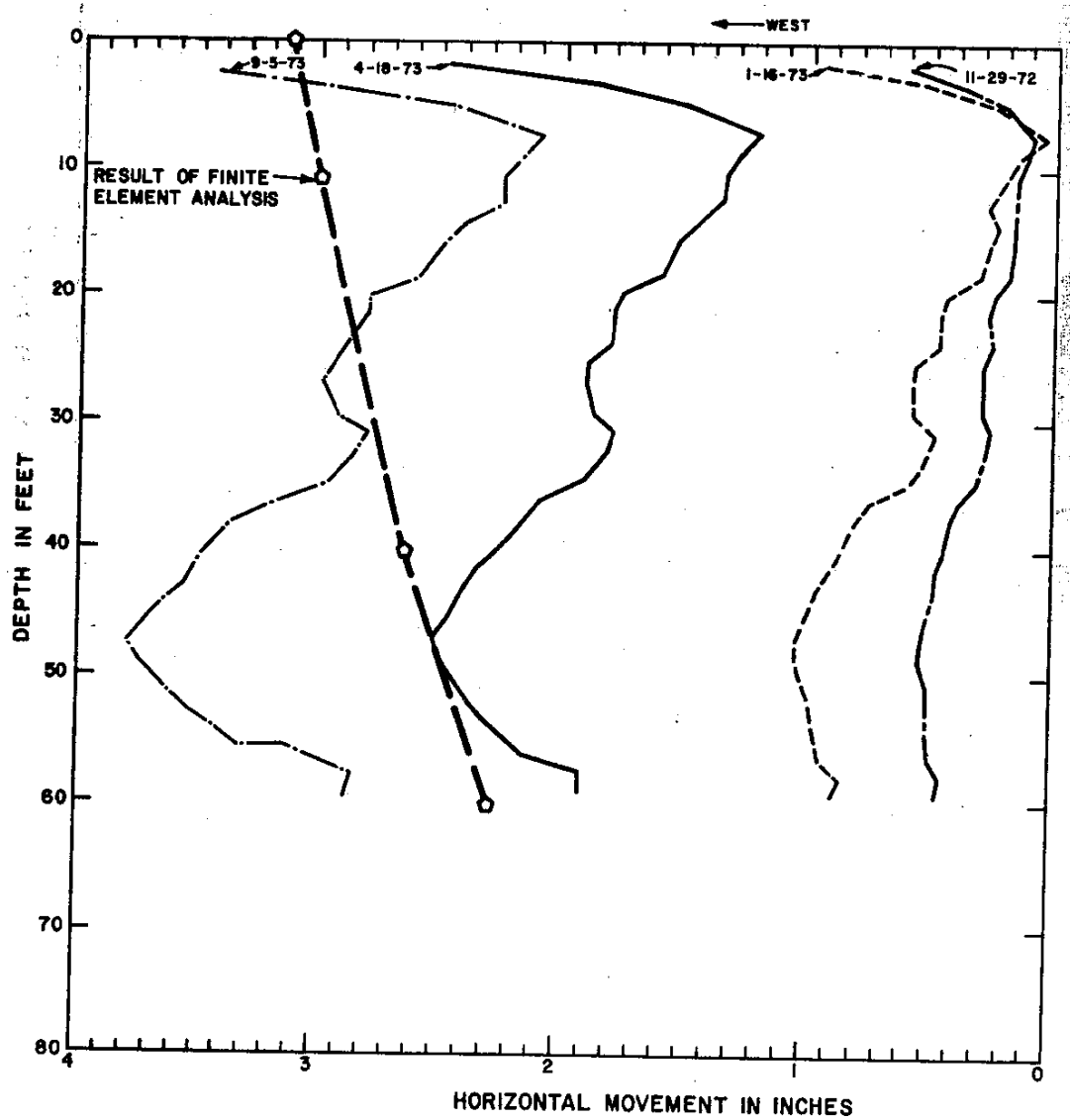



Figure 23: HORIZONTAL MOVEMENT IN THE E-W DIRECTION MEASURED BY SLOPE INDICATOR SI-3

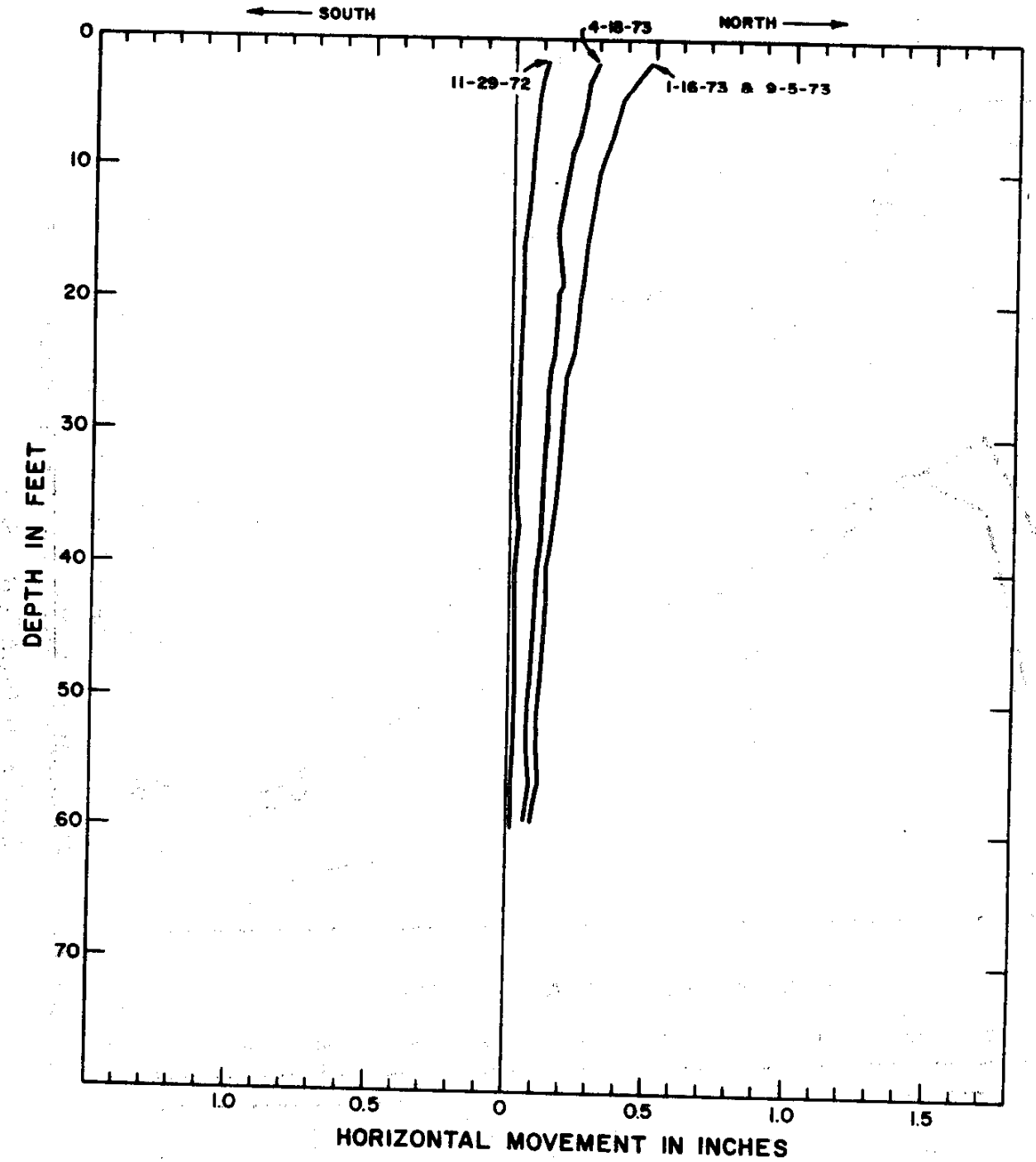



Figure 24: HORIZONTAL MOVEMENT IN THE N-S DIRECTION MEASURED BY SLOPE INDICATOR SI-3

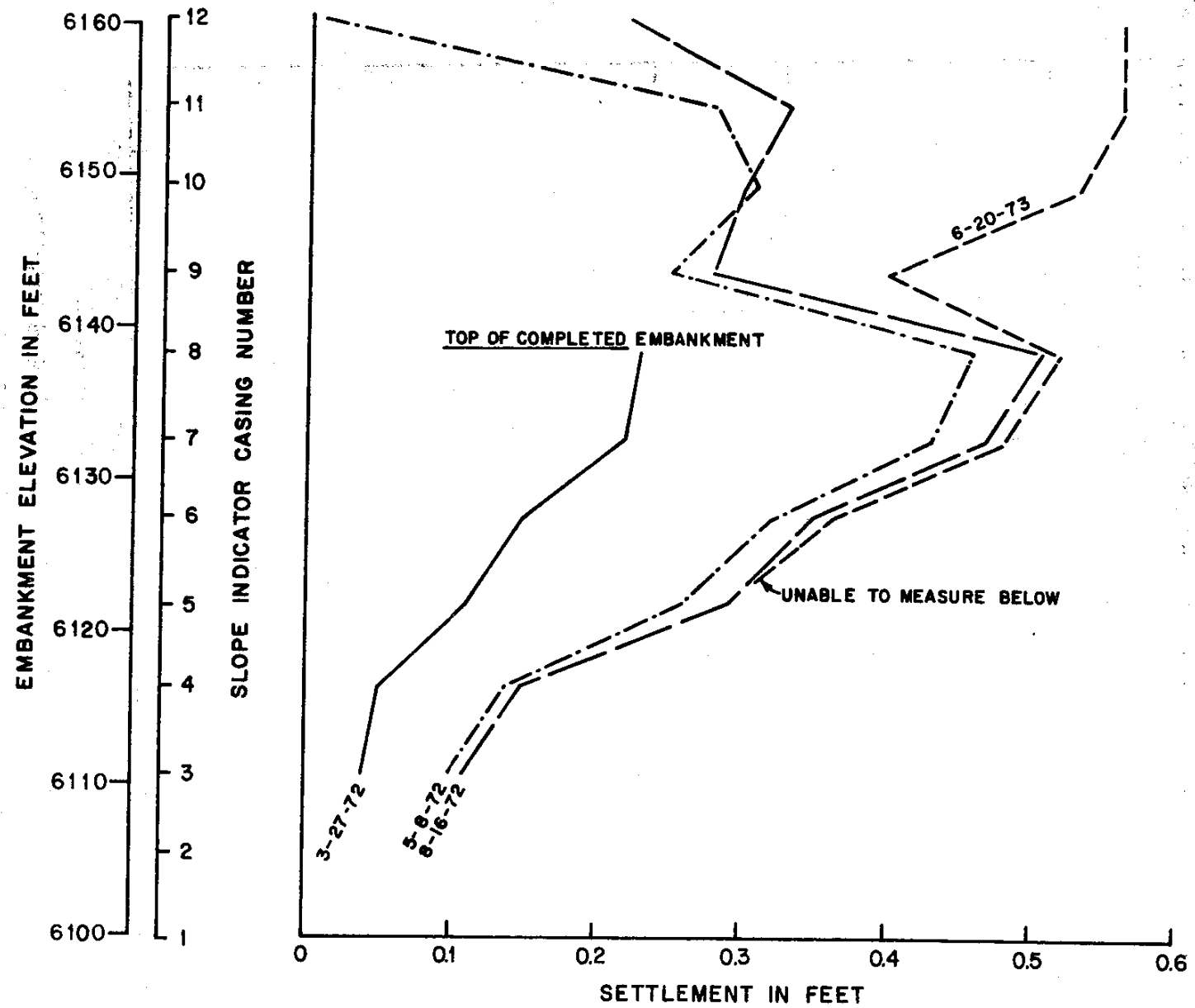



Figure 25: EMBANKMENT SETTLEMENT MEASURED BY SLOPE INDICATOR SI-1

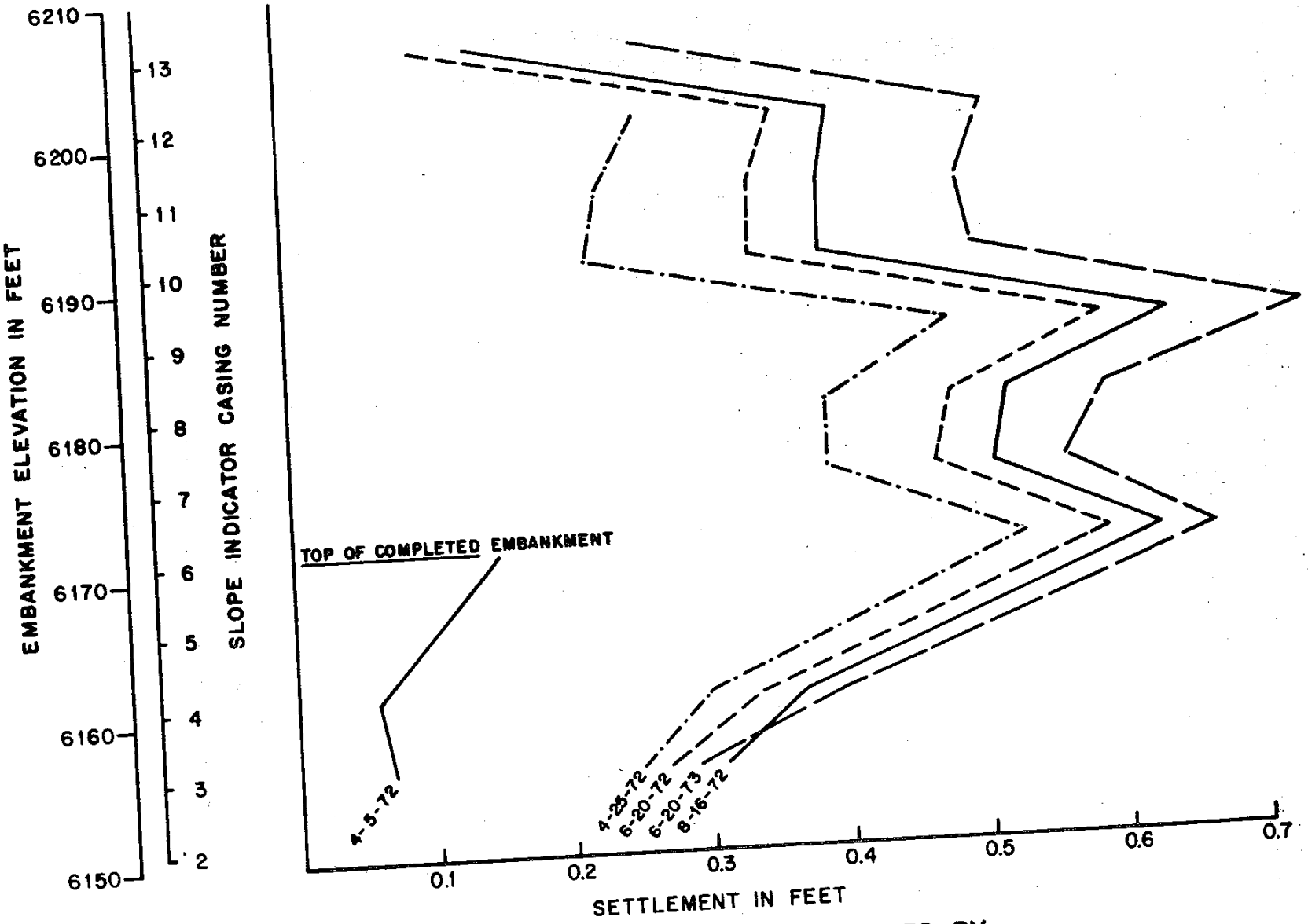



Figure 26: EMBANKMENT SETTLEMENT MEASURED BY SLOPE INDICATOR SI-2

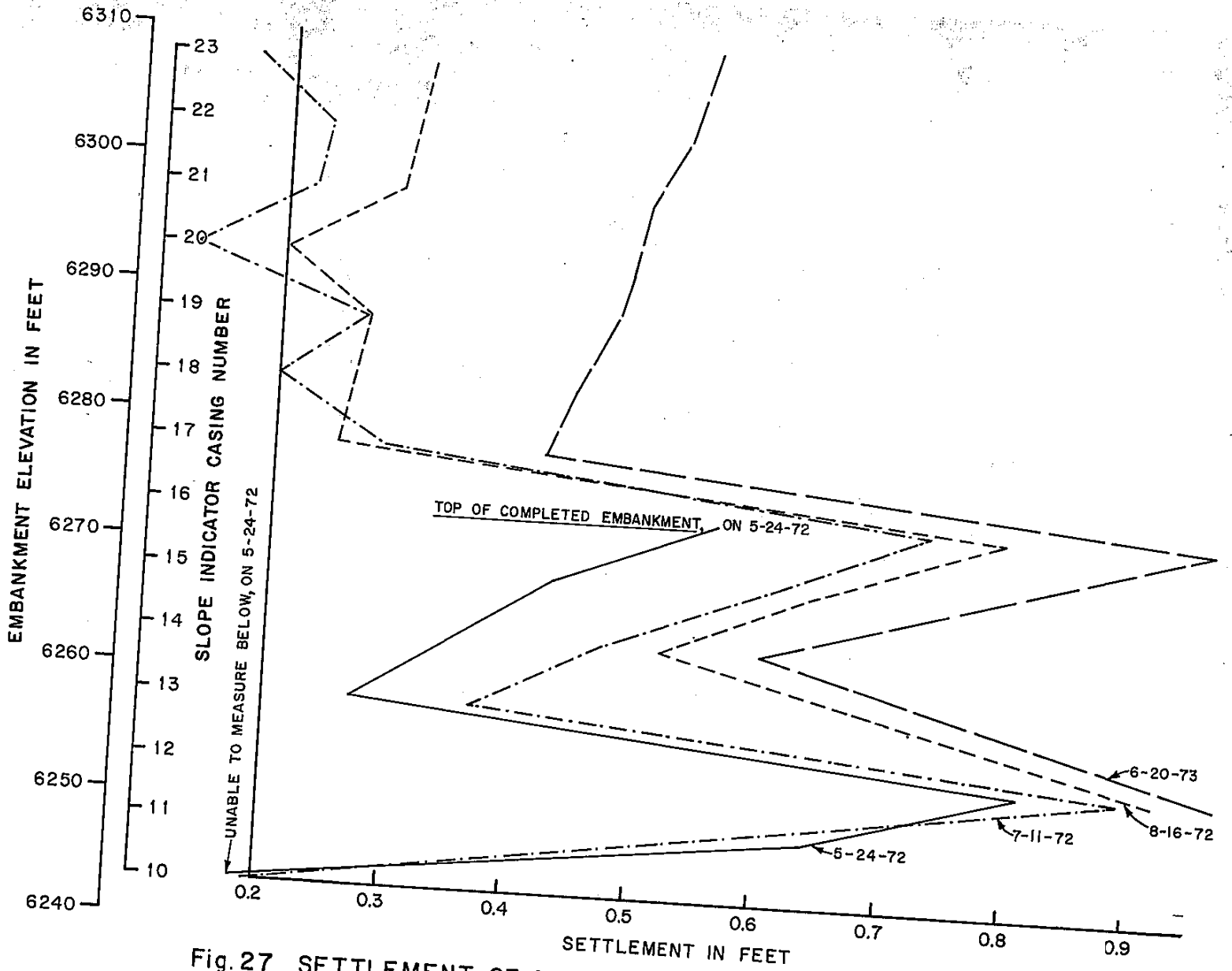
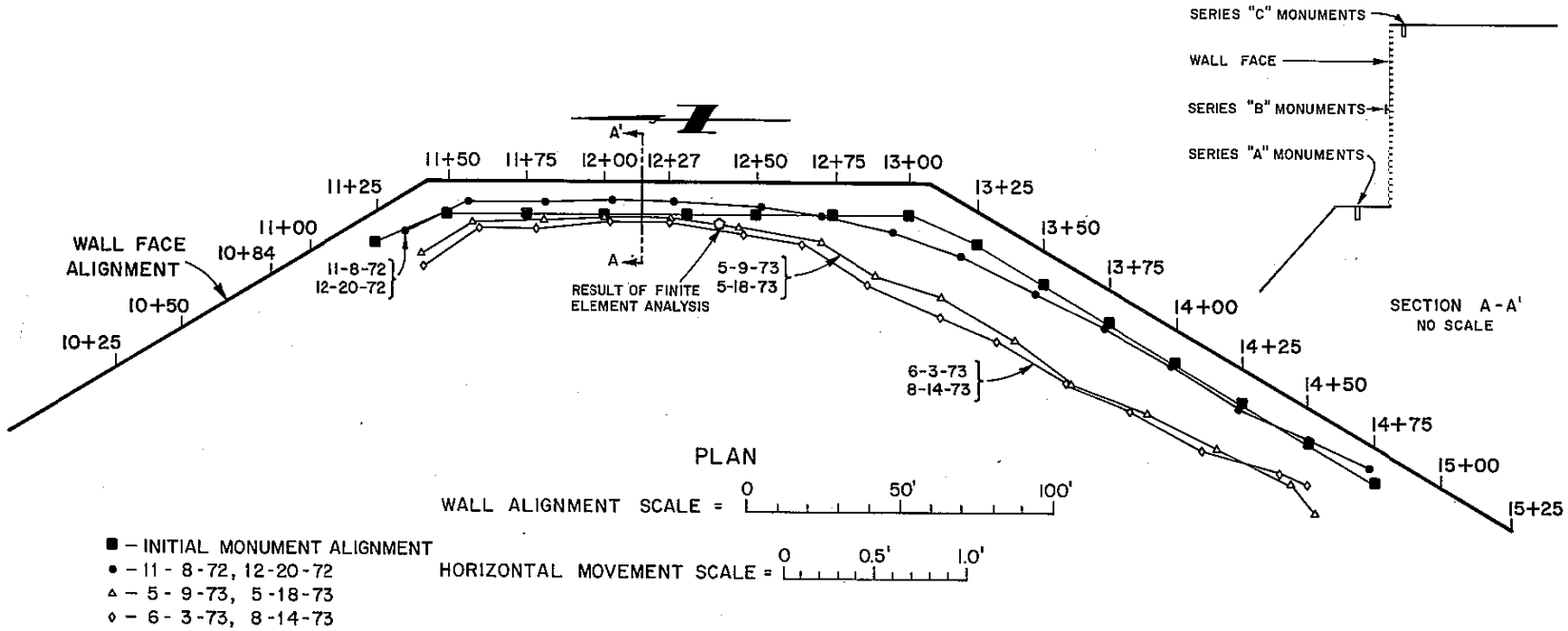
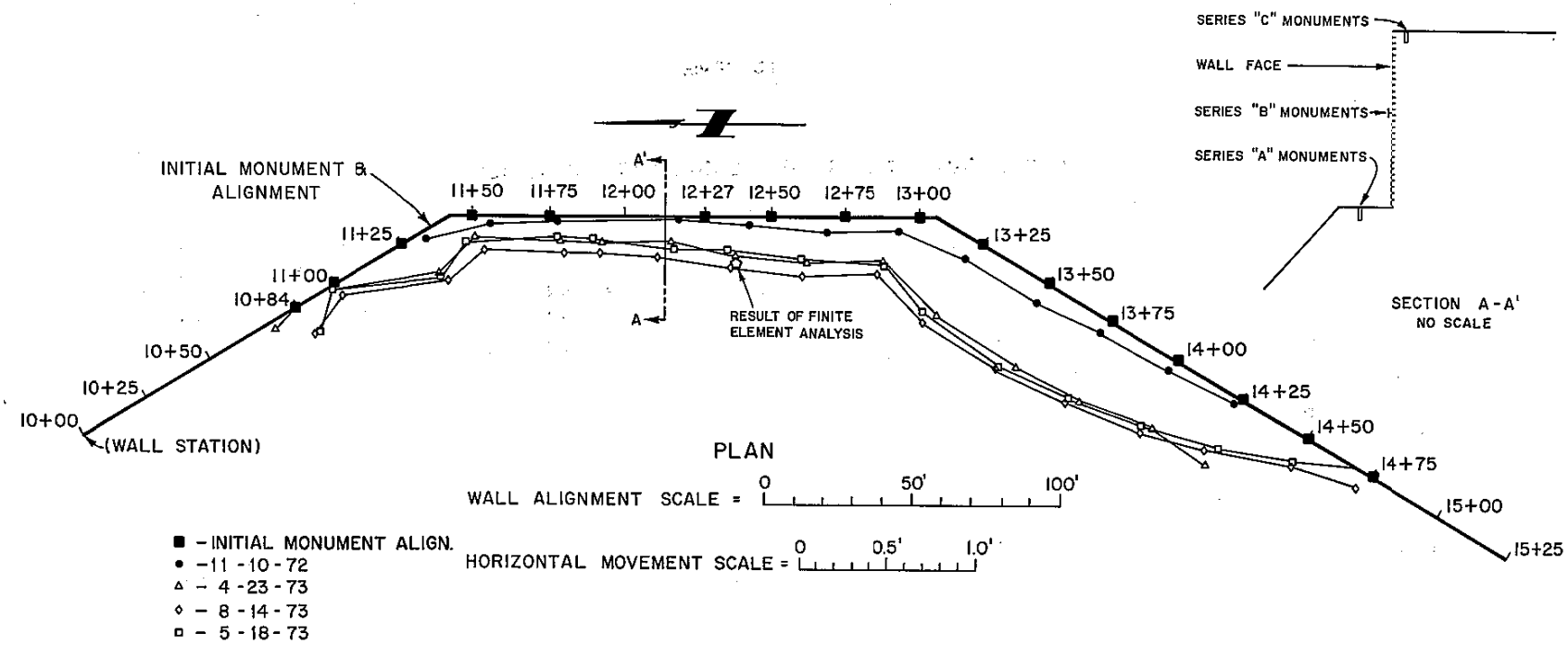



Fig. 27 SETTLEMENT OF EMBANKMENT MEASURED BY SLOPE INDICATOR, SI-3



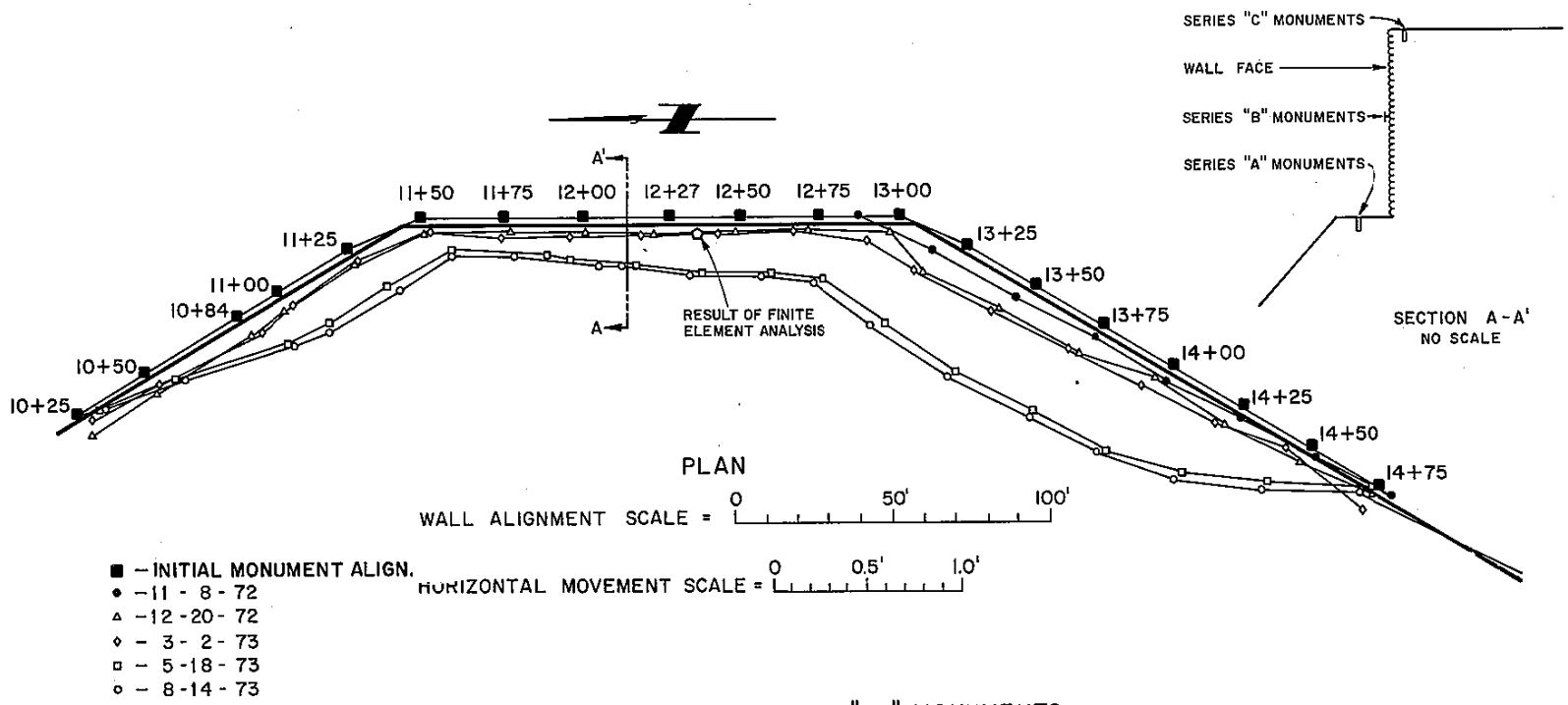

HORIZONTAL MOVEMENT - SERIES " A " MONUMENTS

Figure: 28



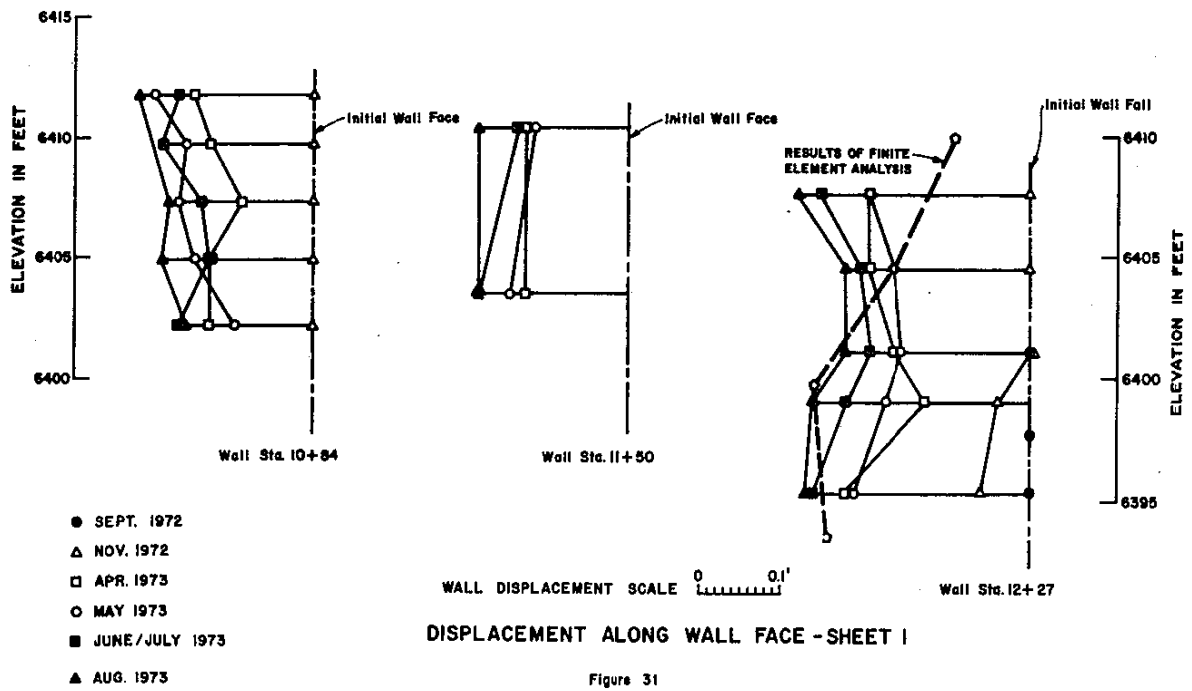

HORIZONTAL MOVEMENT - SERIES " B " MONUMENTS

Figure: 29



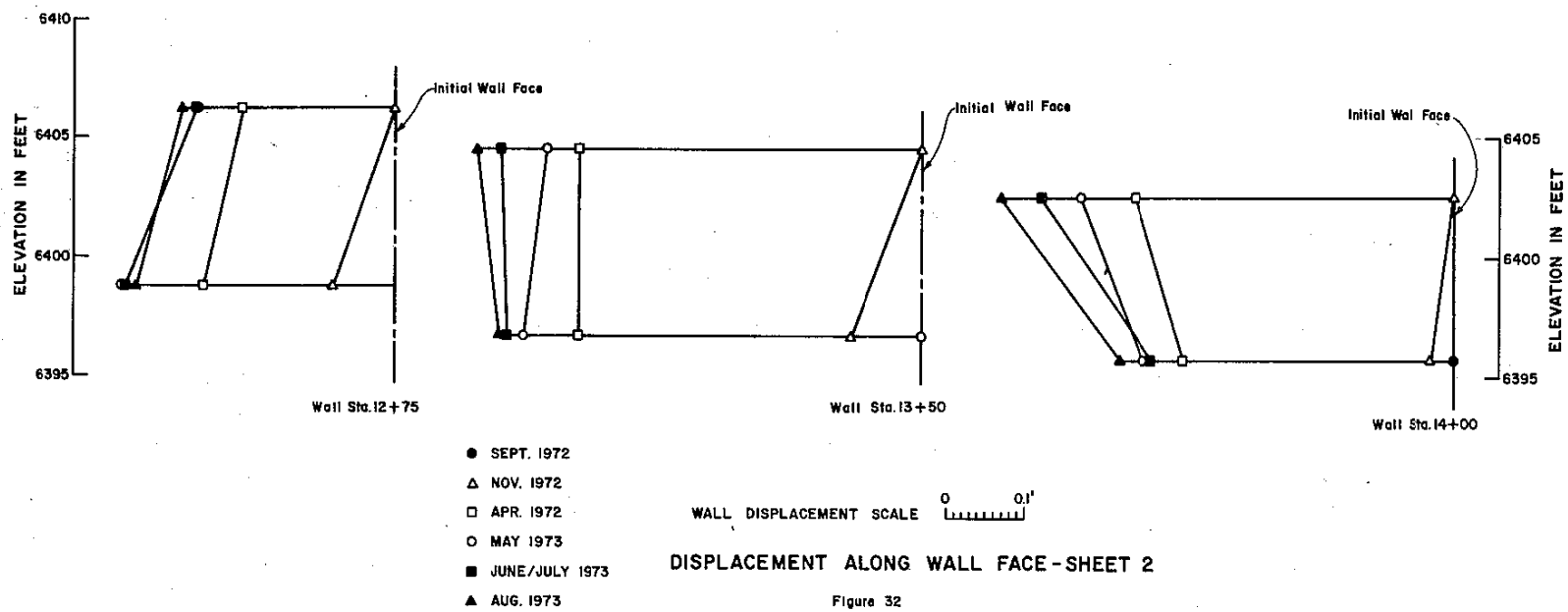

HORIZONTAL MOVEMENT – SERIES "C" MONUMENTS

Figure: 30



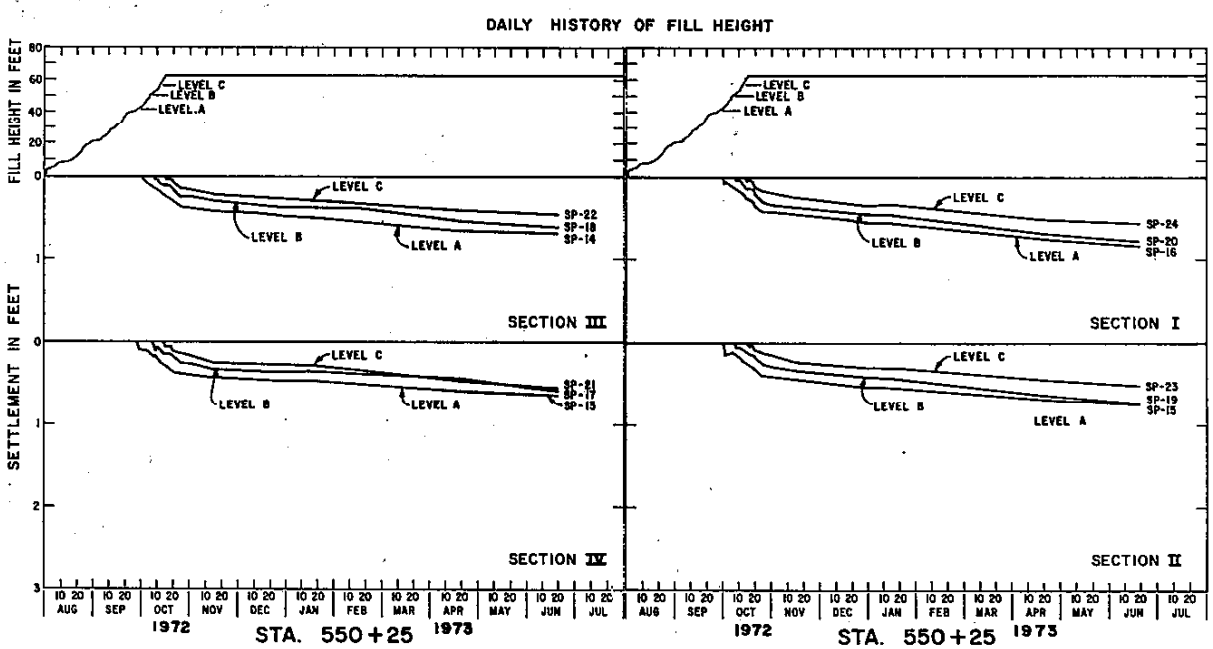

DISPLACEMENT ALONG WALL FACE - SHEET I

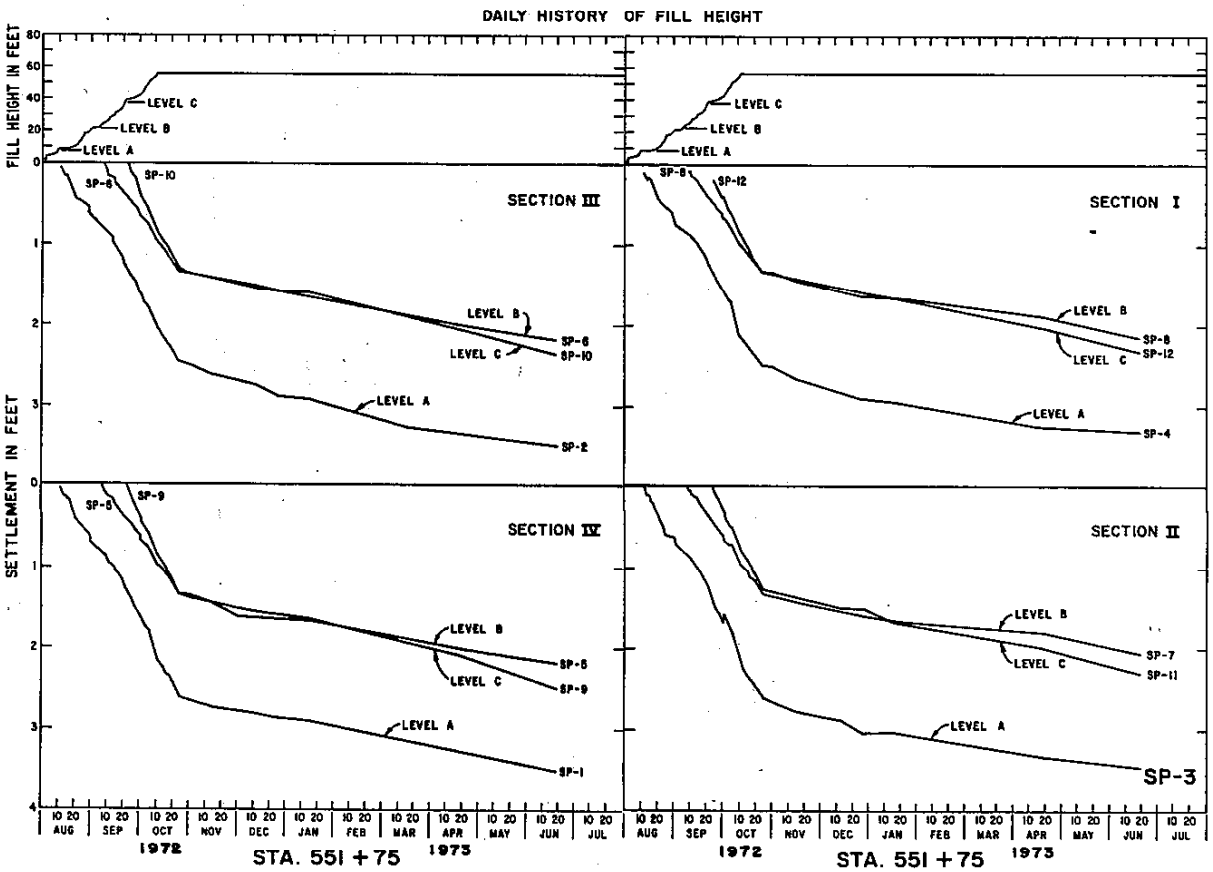
Figure 31




DISPLACEMENT ALONG WALL FACE-SHEET 2

Figure 32

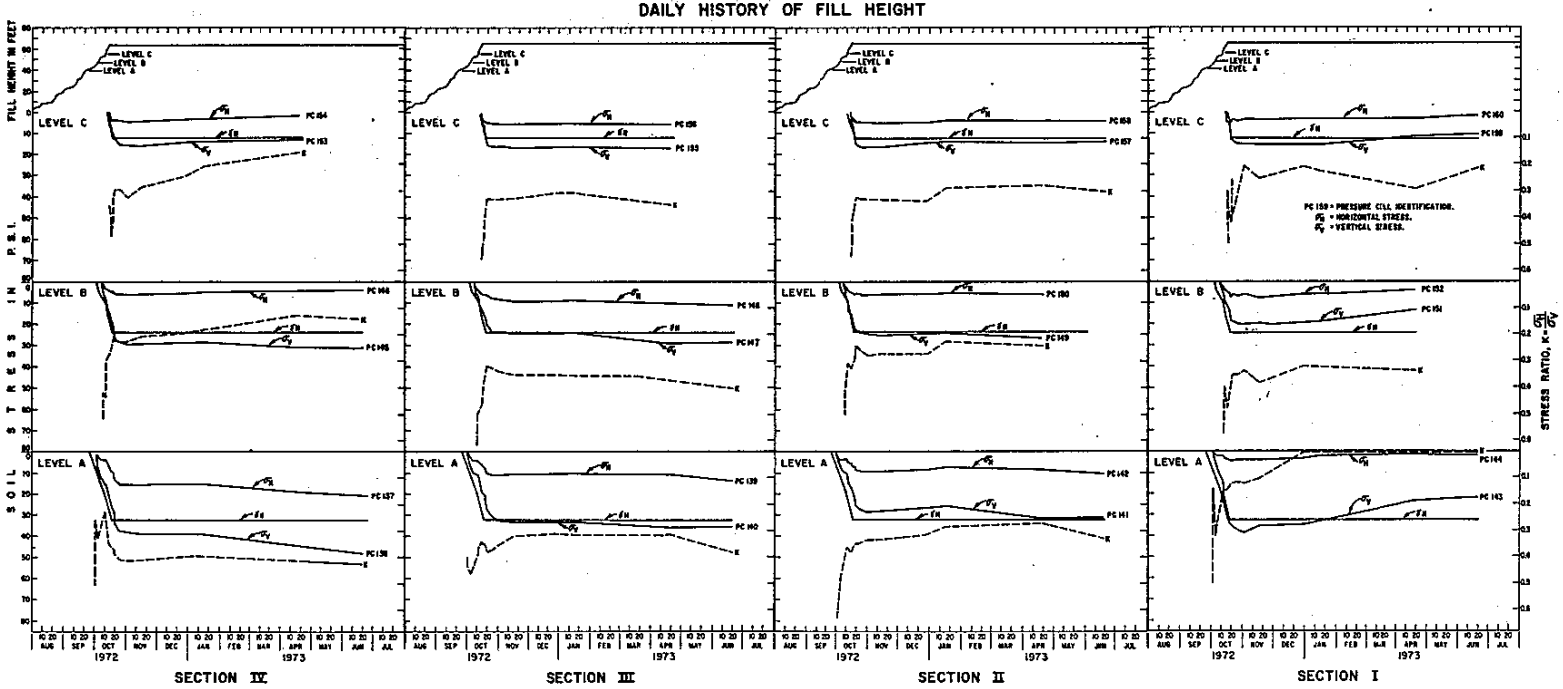



DAILY HISTORY OF SETTLEMENT

Figure 33

DAILY HISTORY OF FILL HEIGHT




STATION 550+25

DAILY HISTORY OF SOIL STRESS

Figure 34

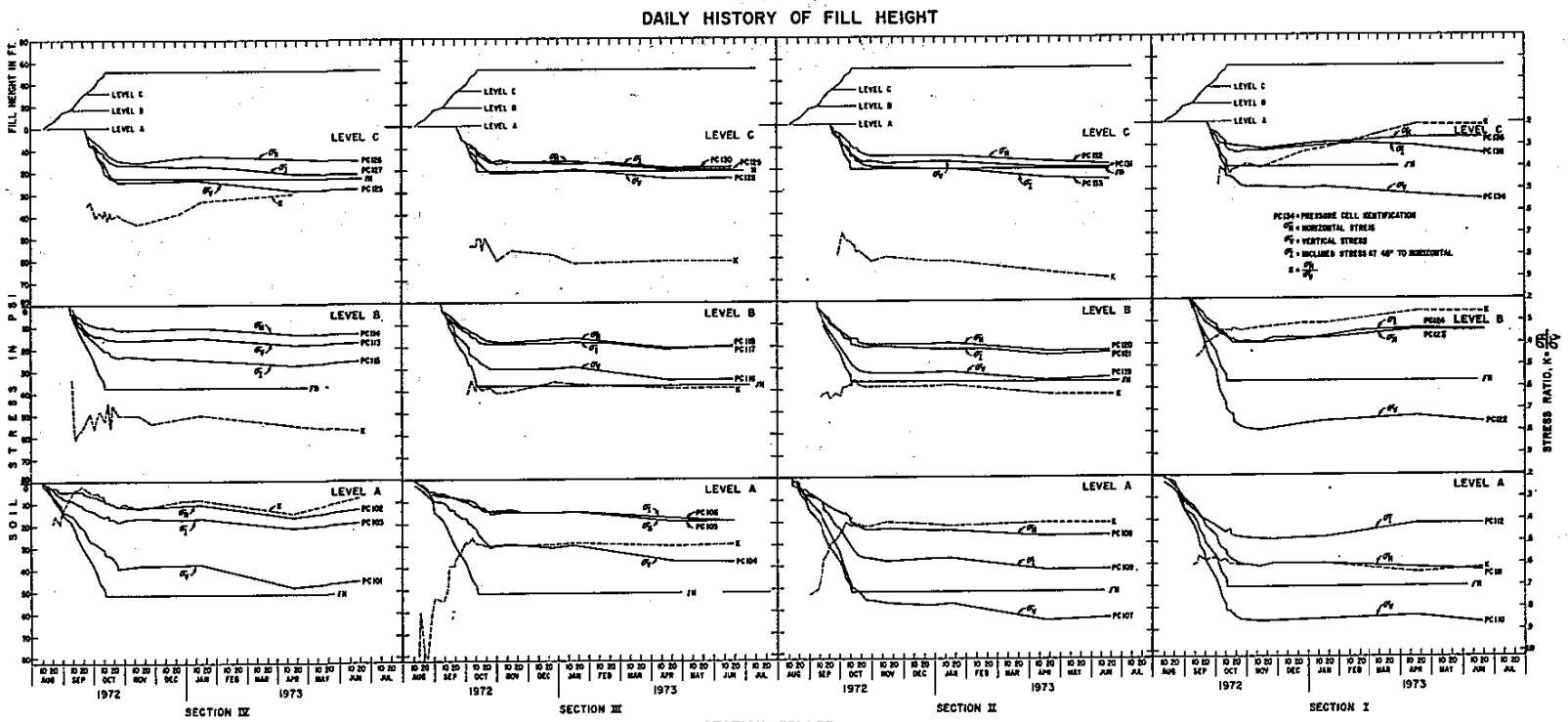
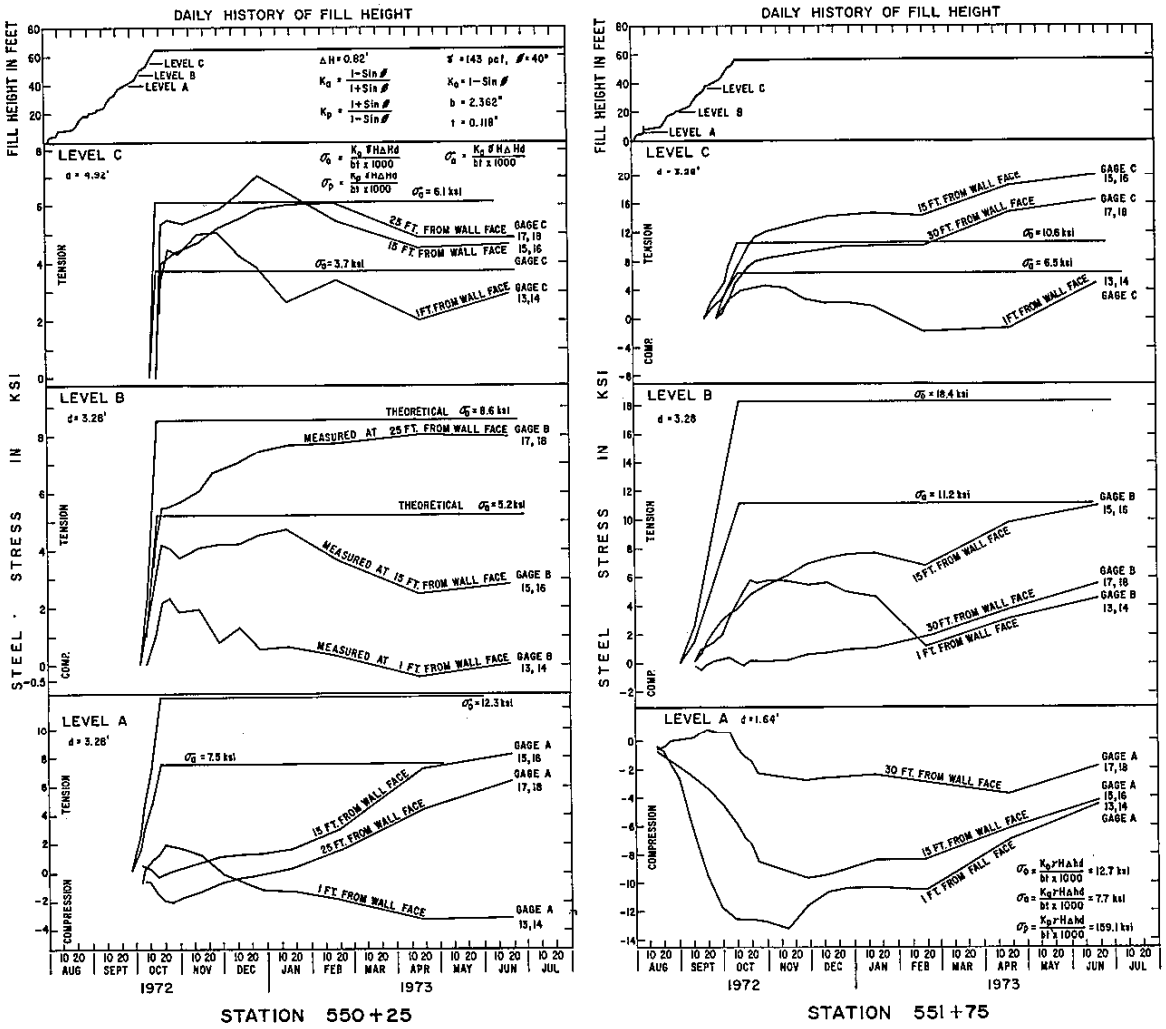
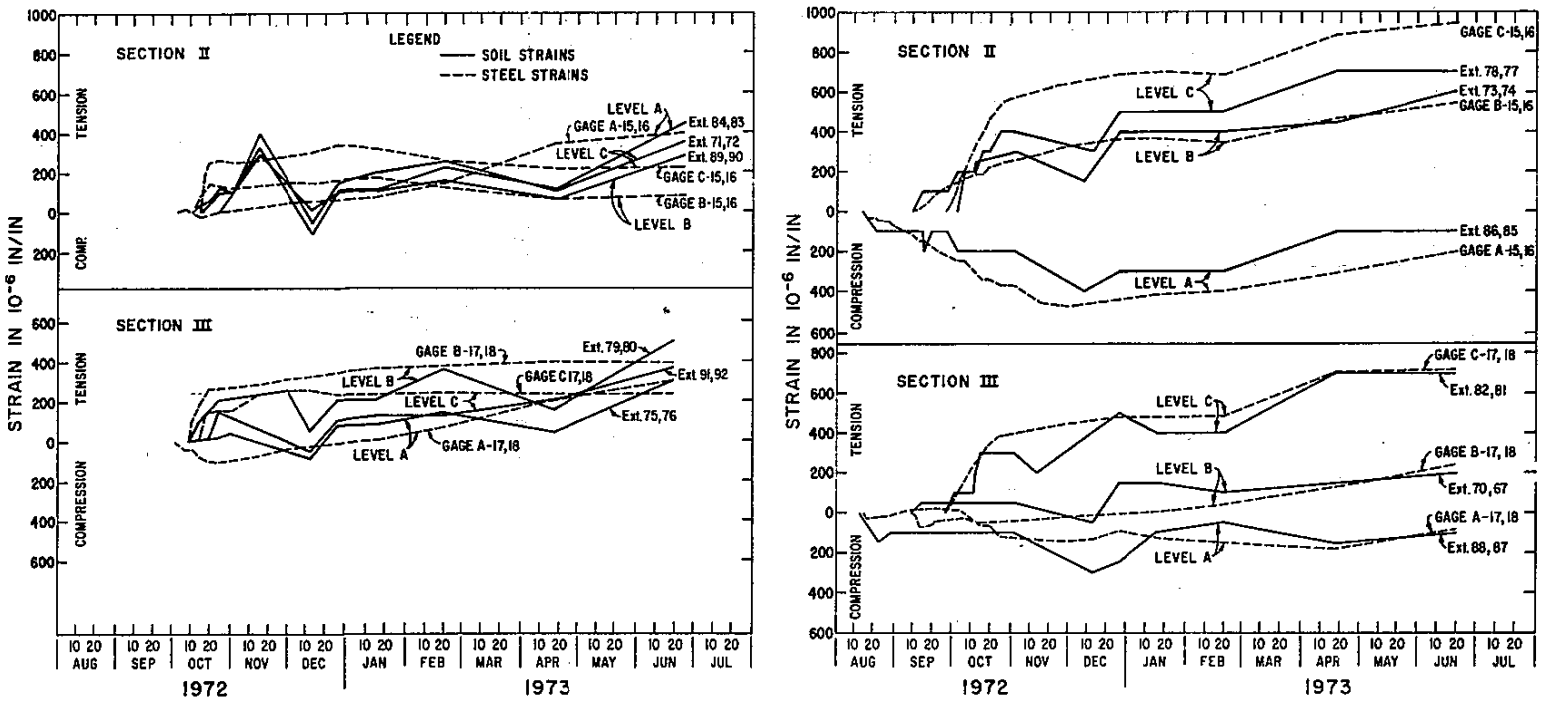

DAILY HISTORY OF FILL HEIGHT
FILL HEIGHT IN FT.
SOIL STRESS IN PSI
STRESS RATIO, K = σH/σV
LEVEL C
LEVEL B
LEVEL A
PC134 = PRESSURE CELL IDENTIFICATION
σH = HORIZONTAL STRESS
σV = VERTICAL STRESS
σI = INCLINED STRESS AT 45° TO HORIZONTAL
K = σH/σV
1972
1973
SECTION IV
SECTION III
SECTION II
SECTION I
STATION 551+75
DAILY HISTORY OF SOIL STRESS

Figure 35




DAILY HISTORY OF STRESSES IN STEEL STRIP

Figure 36

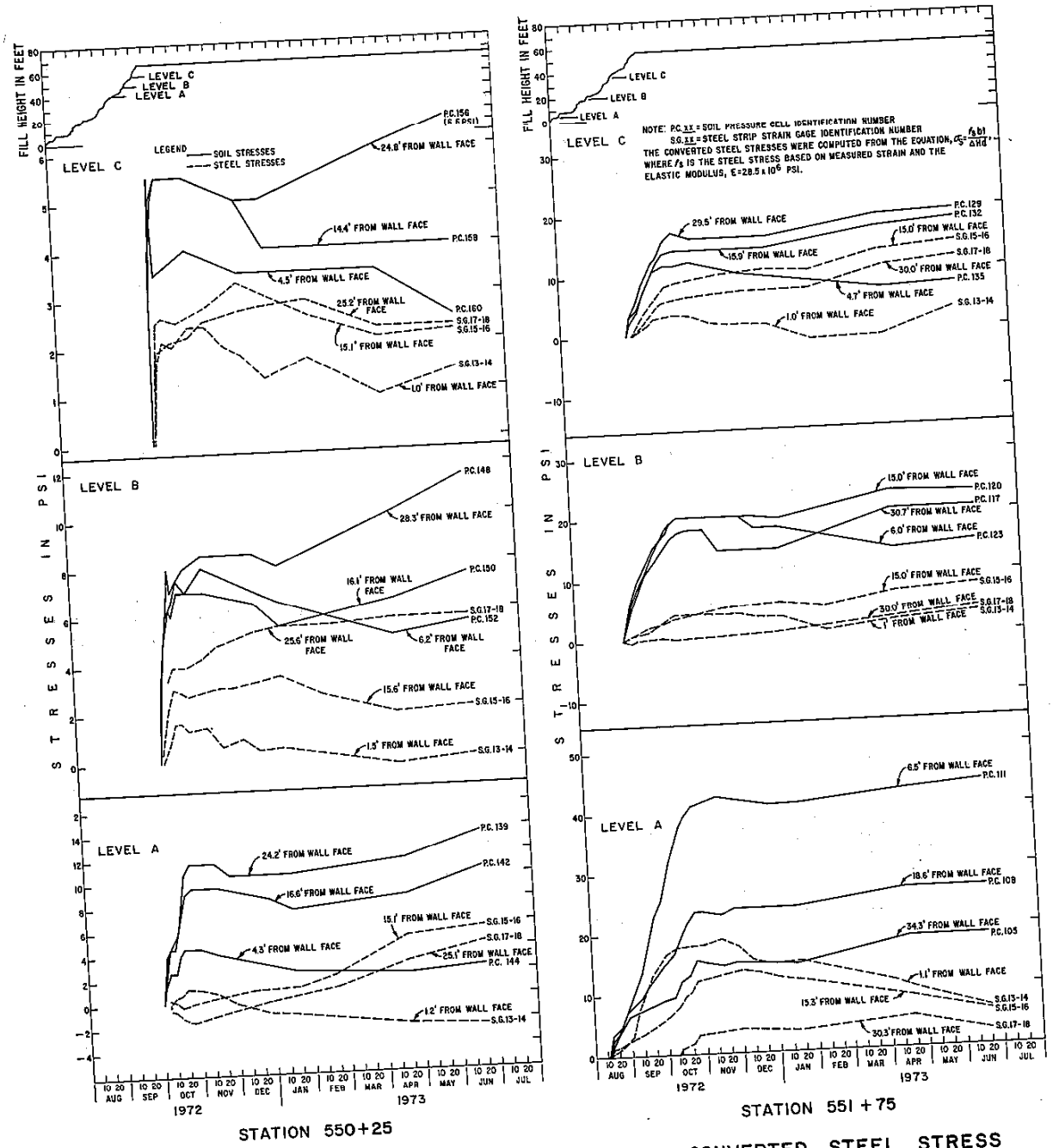



STATION 550+25 SECTIONS II & III

STATION 551+75 SECTIONS II & III

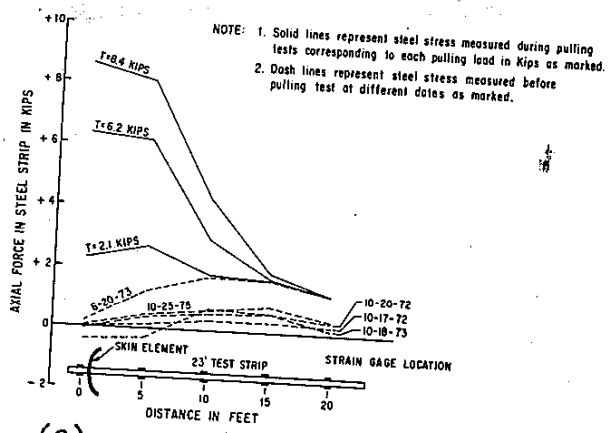
DAILY HISTORY OF HORIZONTAL STRAIN IN STEEL STRIP AND SOIL

FIGURE 37

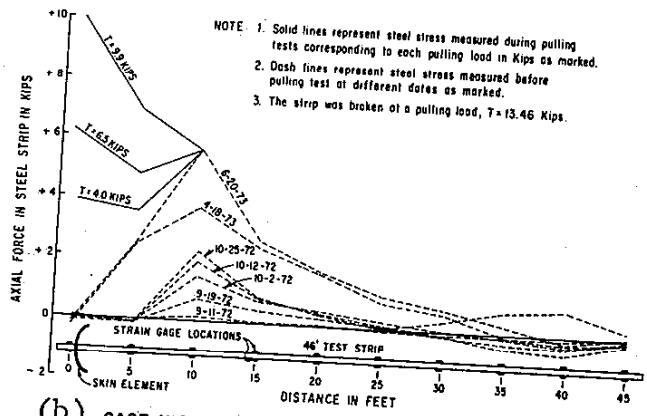



DAILY HISTORY OF HORIZONTAL SOIL STRESS AND CONVERTED STEEL STRESS

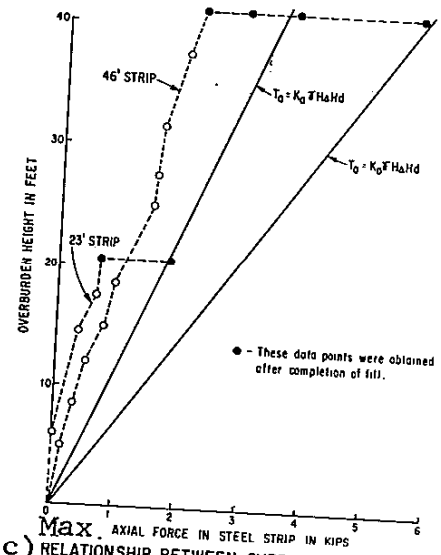
Figure 38




(a) CASE HISTORY OF AXIAL FORCE IN STEEL STRIP

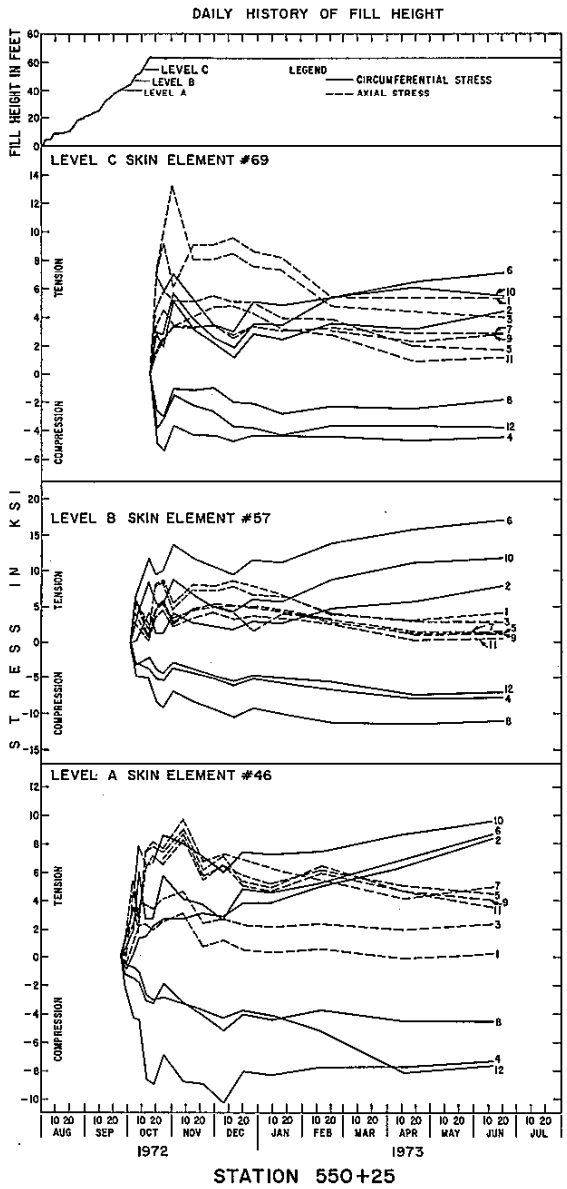



(b) CASE HISTORY OF AXIAL FORCE IN STEEL STRIP

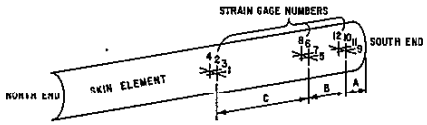



(c) RELATIONSHIP BETWEEN OVERBURDEN HEIGHT AND AXIAL FORCE IN STEEL STRIP

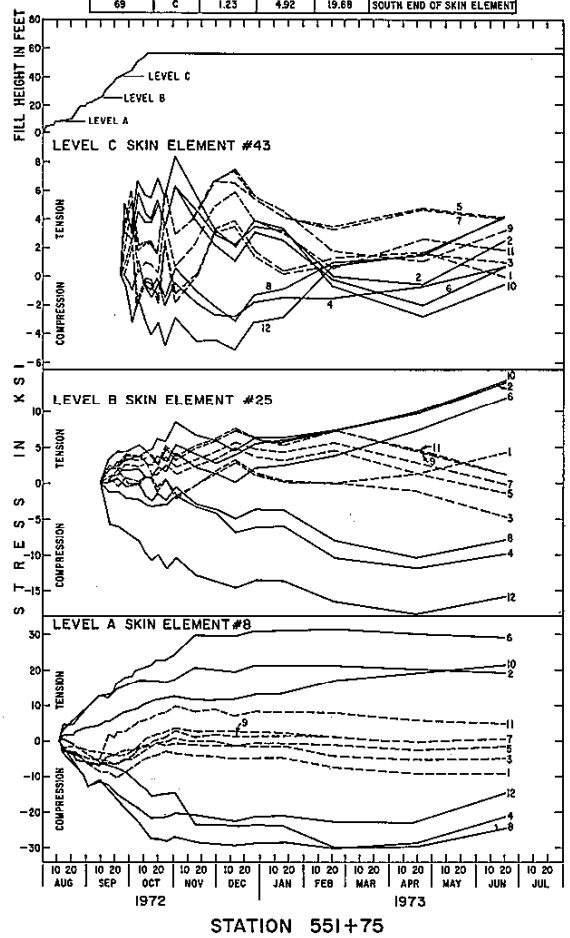
**Figure 39: AXIAL FORCE IN DUMMY STRIPS**




STATION 550+25



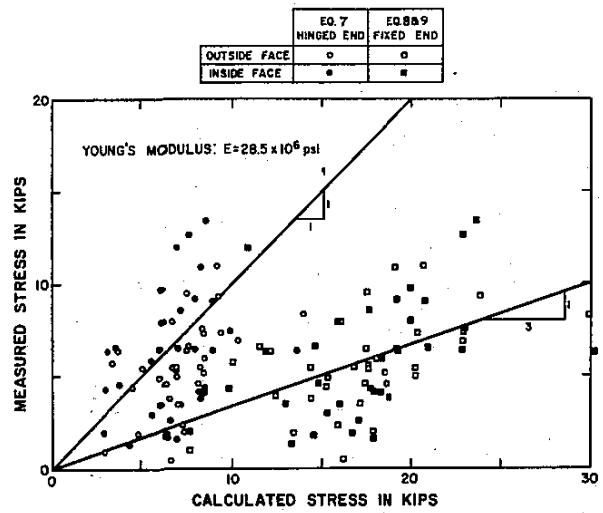

| SKIN ELEMENT | LEVEL | HORIZONTAL DISTANCE BETWEEN STRAIN GAGES AND END OF SKIN ELEMENT IN FEET A | B | C | REMARKS |
|---|---|---|---|---|---|
| 8 | A | 4.20 | 5.05 | 19.68 | STATION 551+75, A, B, C |
| 25 | B | 0.82 | 3.28 | 18.00 | REFERENCED FROM |
| 43 | C | 0.82 | 3.28 | 18.00 | NORTH END OF SKIN ELEMENT |
| 46 | A | 0.82 | 3.28 | 19.68 | STATION 550+25, A, B, C |
| 57 | B | 0.82 | 3.28 | 19.68 | REFERENCED FROM |
| 69 | C | 1.23 | 4.92 | 19.68 | SOUTH END OF SKIN ELEMENT |



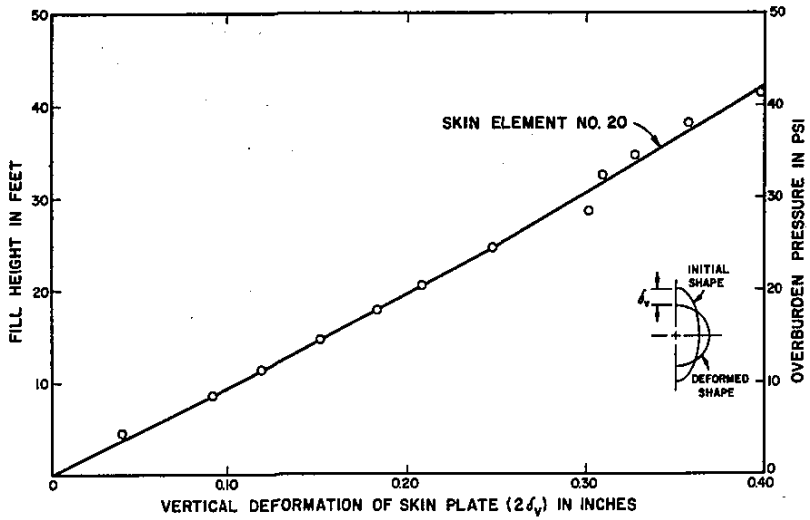

STATION 551+75

DAILY HISTORY OF STRESS IN SKIN ELEMENT

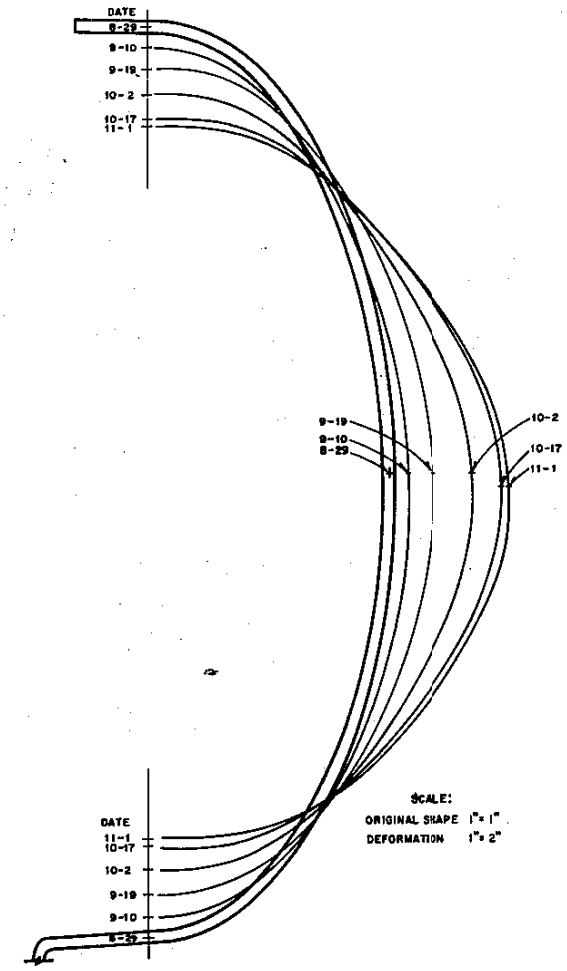
Figure 40




(a) COMPARISON OF MEASURED AND CALCULATED CIRCUMFERENTIAL STRESS AT SPRING LINE OF SKIN PLATE




(b) RELATIONSHIP BETWEEN FILL HEIGHT AND SKIN PLATE DEFORMATION STATION 551+75

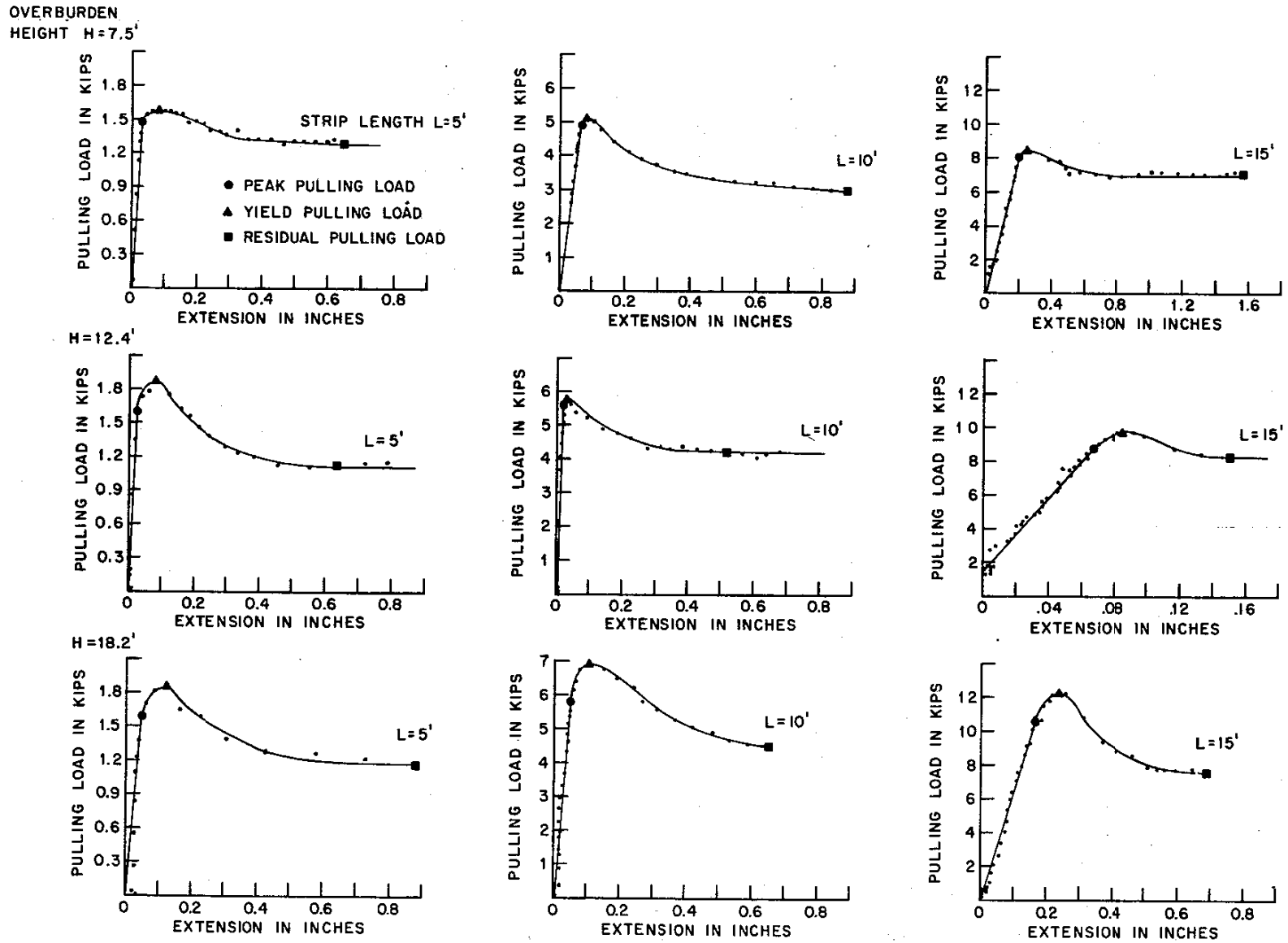



STATION 551+75, LEVEL A, SKIN ELEMENT NO. 20

(c) CASE HISTORY OF DEFORMATION OF SKIN PLATE

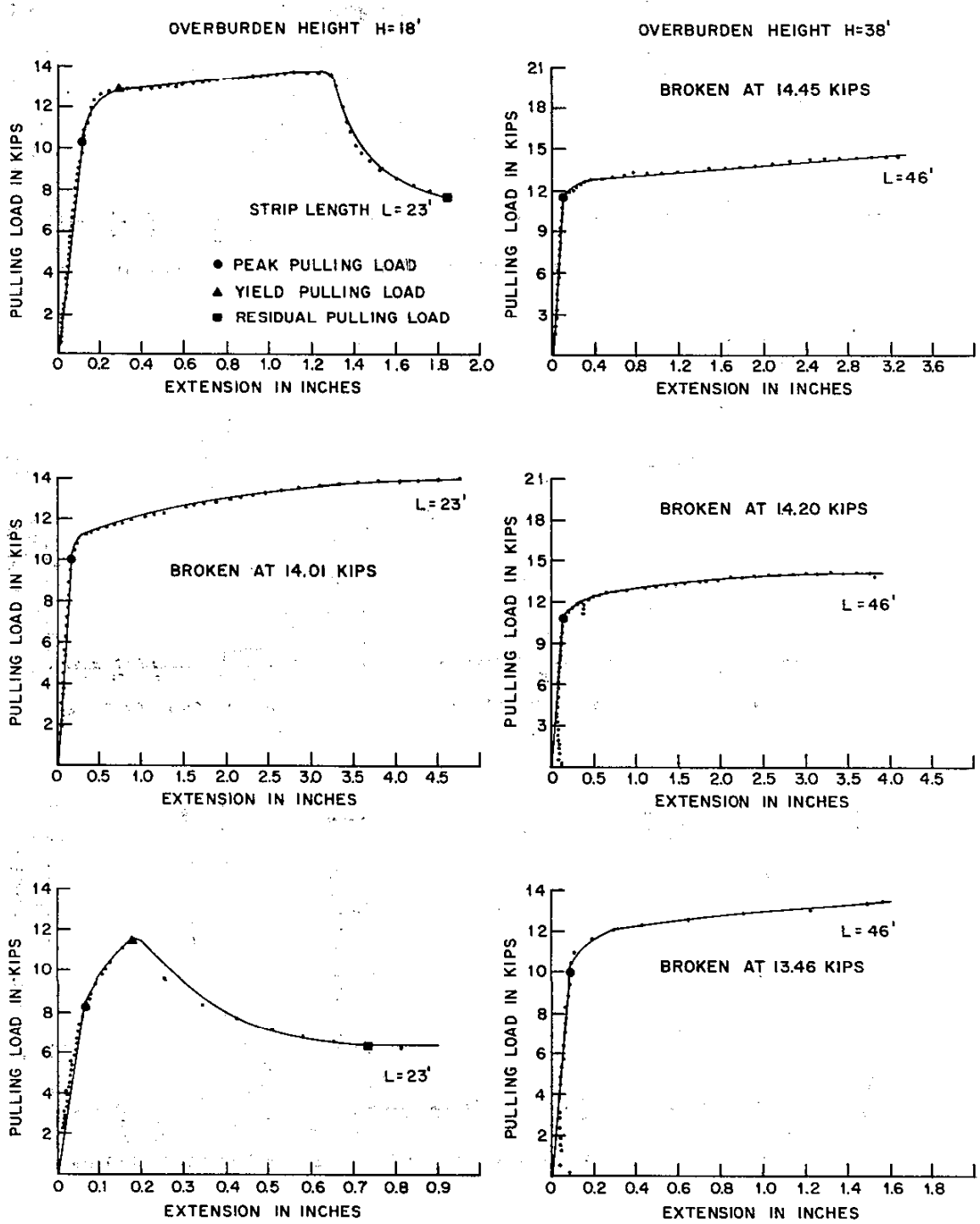
FIELD BEHAVIOR OF STEEL SKIN ELEMENT

Figure 41



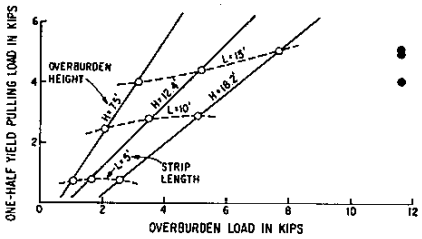

LOAD DEFORMATION CURVE FROM FIELD PULLING TESTS-SHEET I

Figure 42

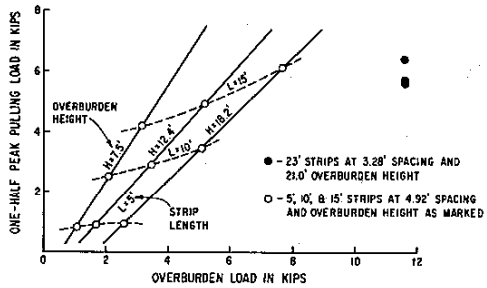



LOAD DEFORMATION CURVE FROM FIELD PULLING TESTS-SHEET 2

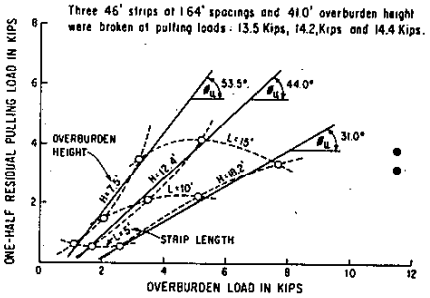
Figure 43



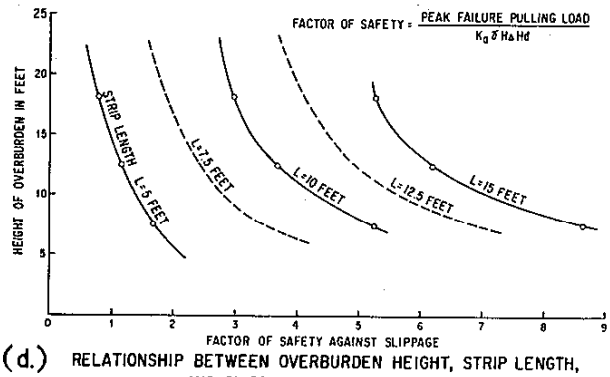

(a.) RELATIONSHIP BETWEEN YIELD PULLING LOAD, OVERBURDEN LOAD, OVERBURDEN HEIGHT AND STRIP LENGTH




(b.) RELATIONSHIP BETWEEN PEAK PULLING LOAD, OVERBURDEN LOAD, OVERBURDEN HEIGHT, AND STRIP LENGTH




(c.) RELATIONSHIP BETWEEN RESIDUAL PULLING LOAD, OVERBURDEN LOAD, OVERBURDEN HEIGHT AND STRIP LENGTH




(d.) RELATIONSHIP BETWEEN OVERBURDEN HEIGHT, STRIP LENGTH, AND SLIPPING FACTOR OF SAFETY

## FIELD PULLING TEST RESULTS

Figure 44

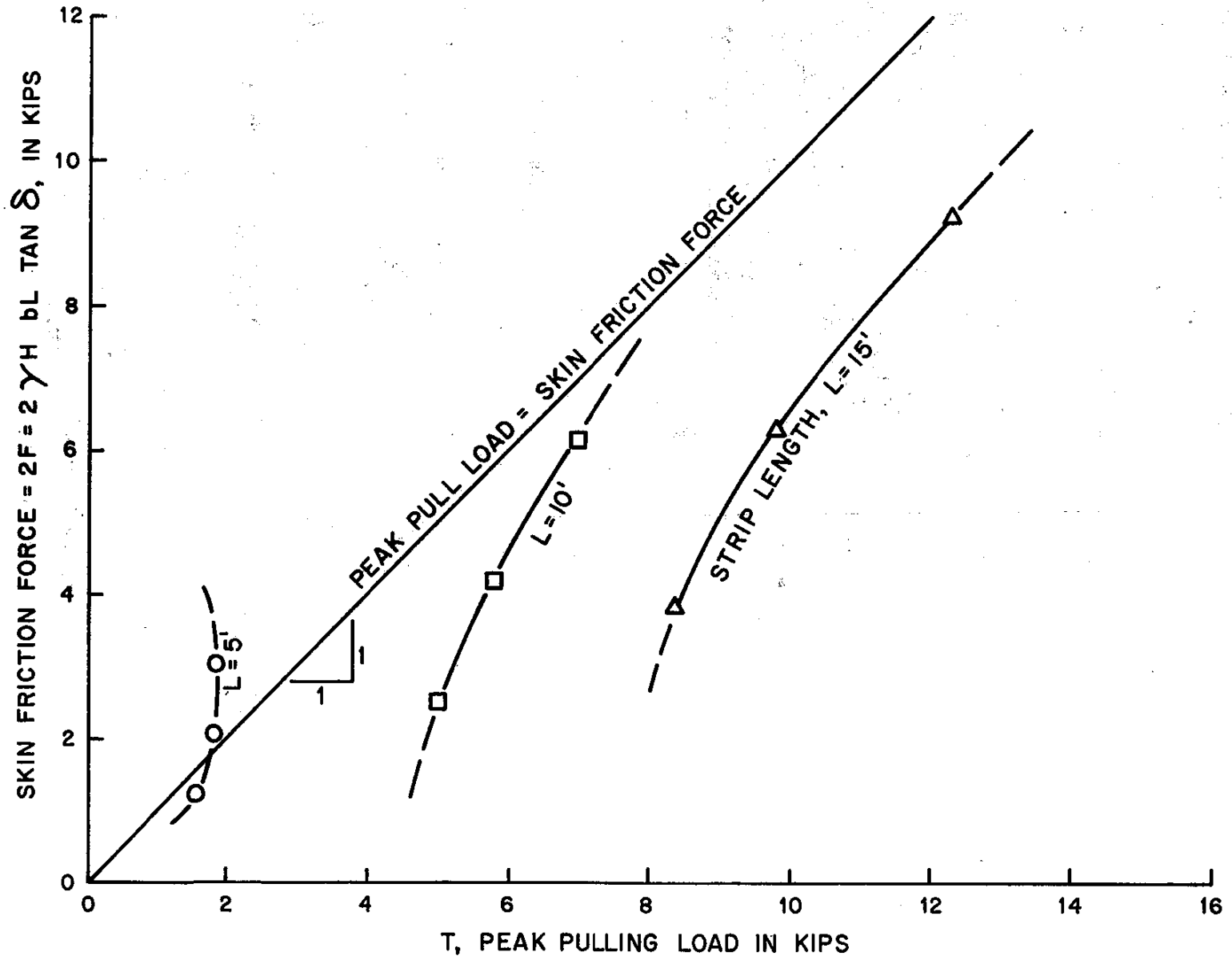



Figure 45: RELATIONSHIP BETWEEN PULL LOAD AND SKIN FRICTION FORCE

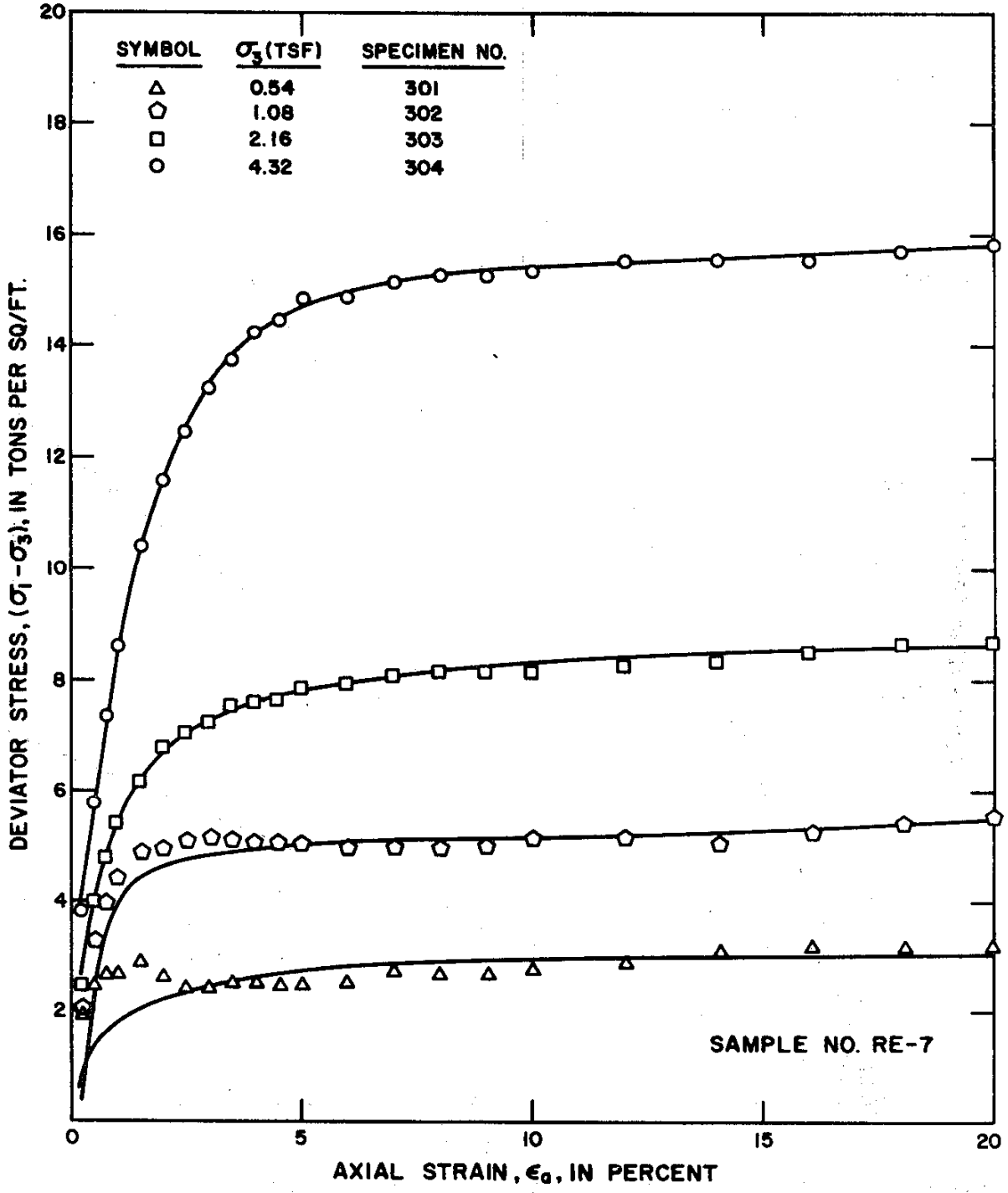



Figure 46: TYPICAL STRESS - STRAIN CURVE OF SOIL SAMPLE

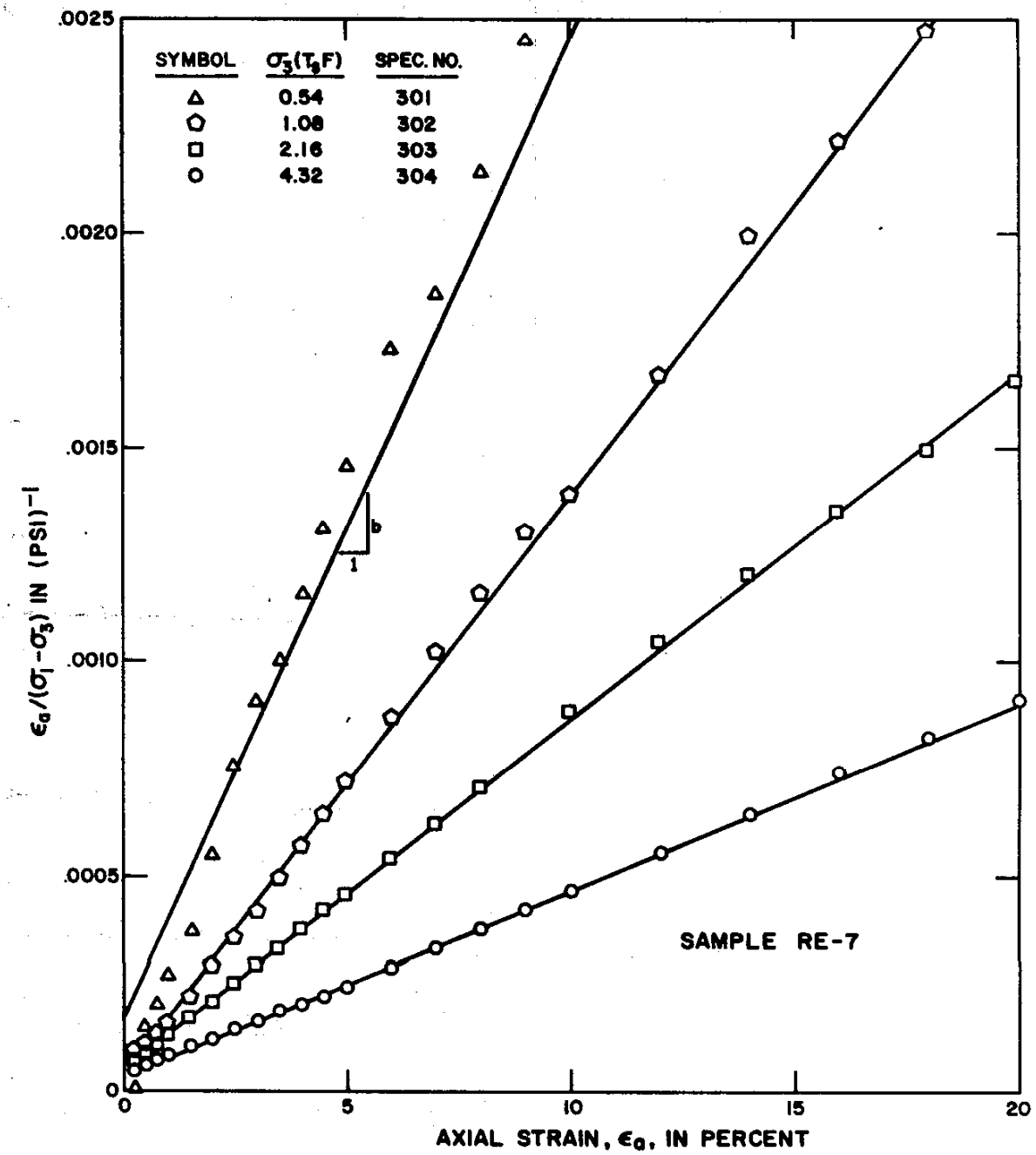



Figure 47: TYPICAL TRANSFORMED HYPERBOLIC STRESS-STRAIN CURVES

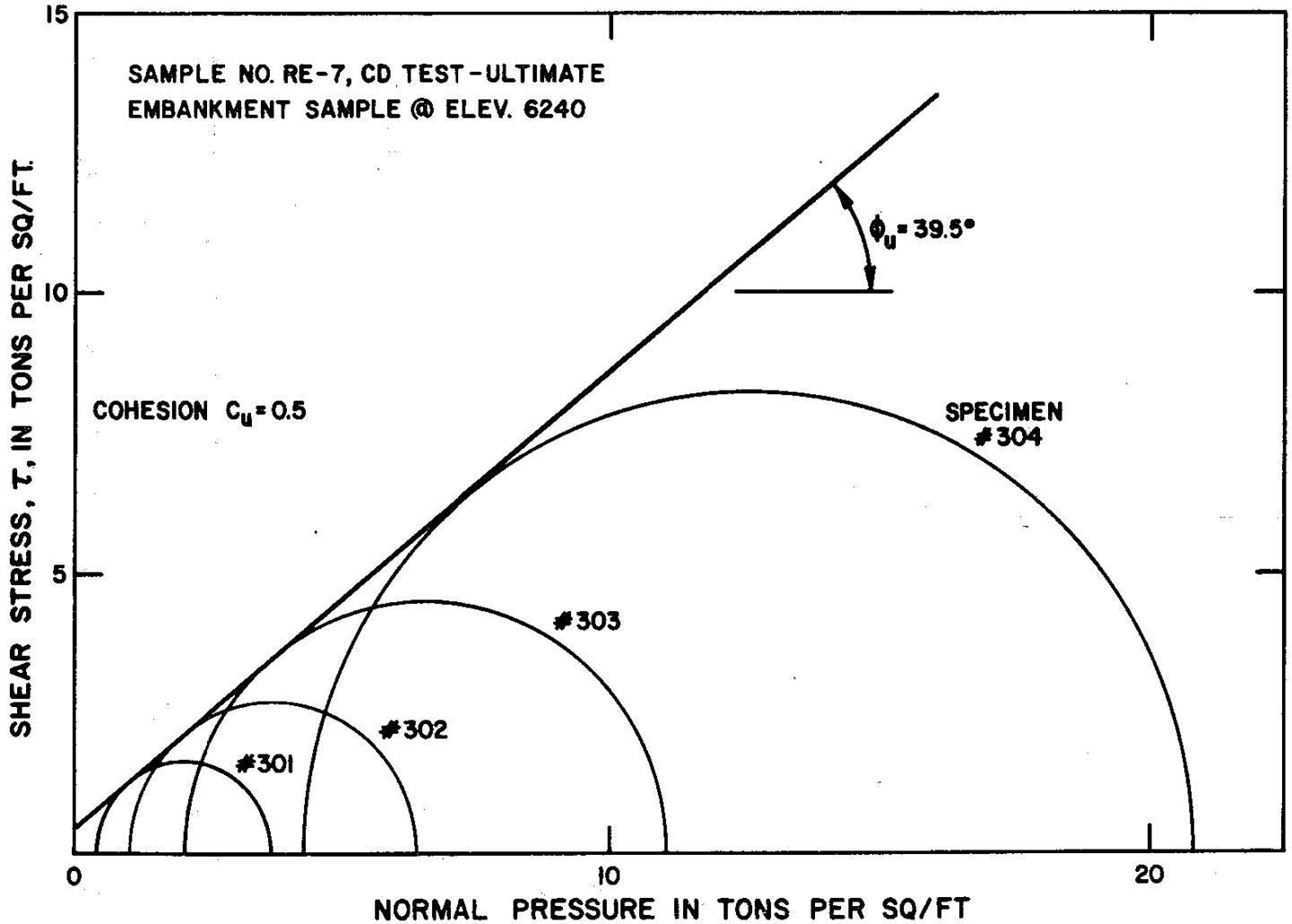



Figure 48: TYPICAL MOHR CIRCLES

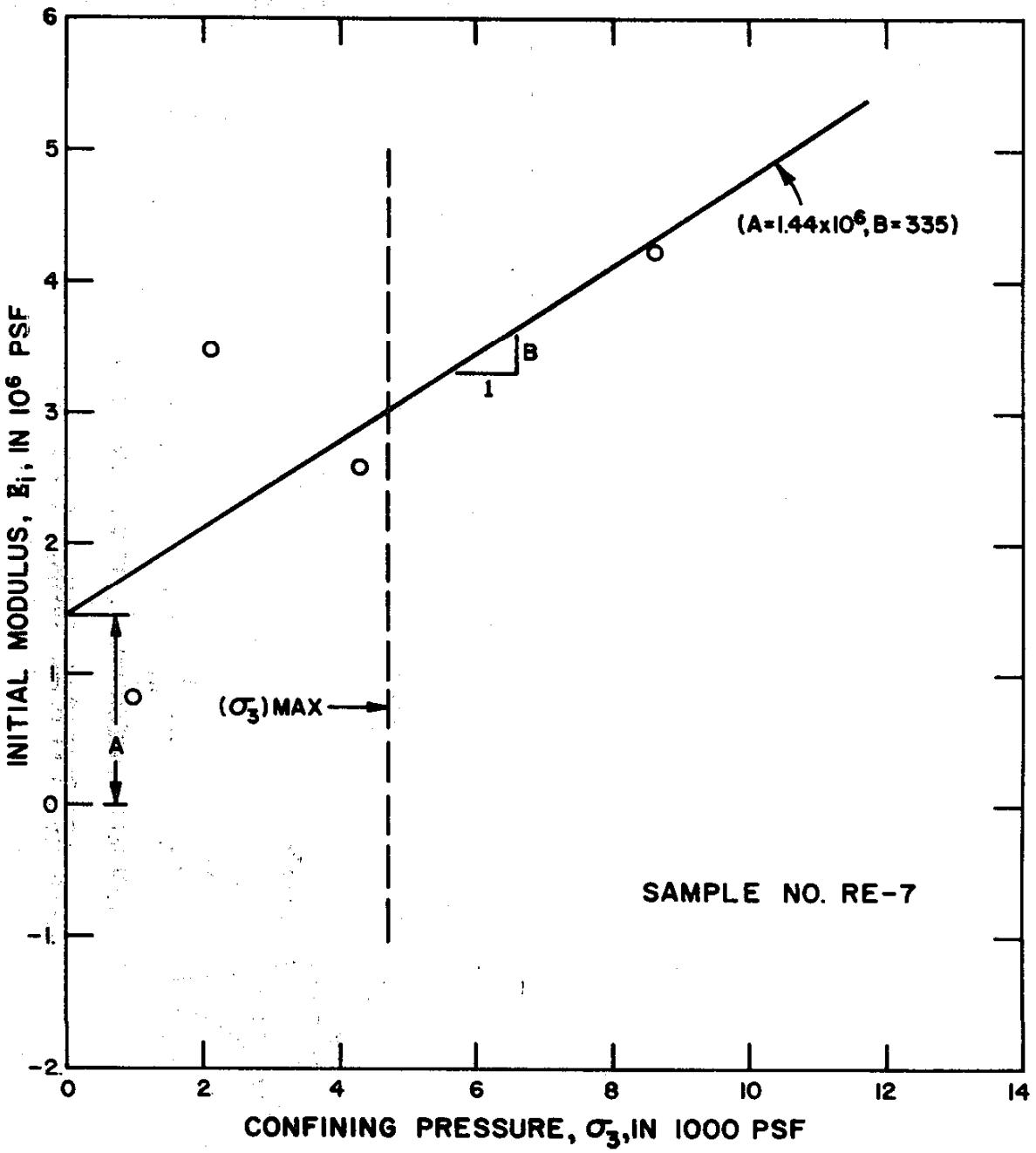



Figure 49: VARIATION OF INITIAL TANGENT MODULUS WITH CONFINING PRESSURE

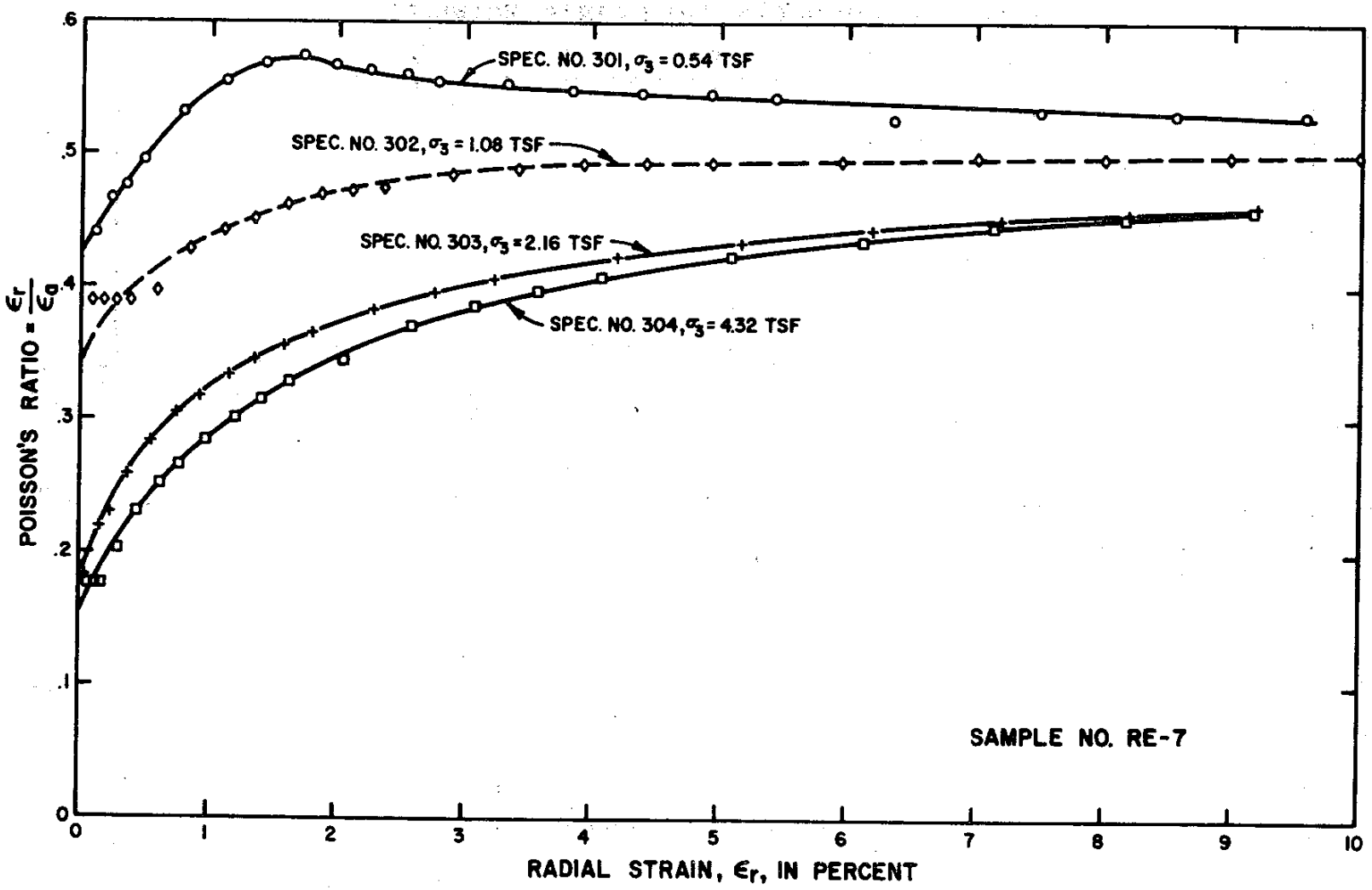



Figure 50: POISSON'S RATIO VS RADIAL STRAIN CURVES

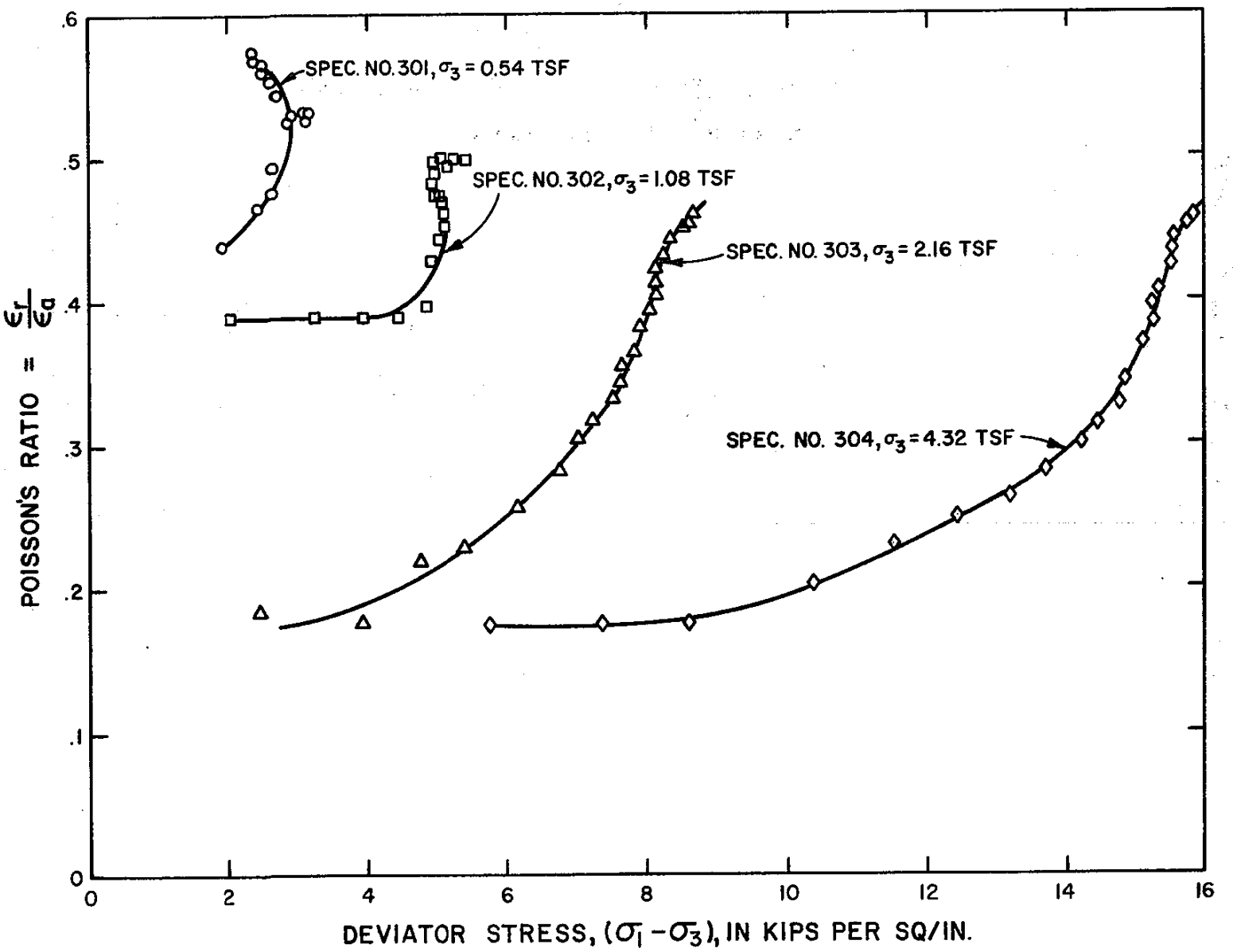



Figure 51: POISSON'S RATIO VS DEVIATOR STRESS

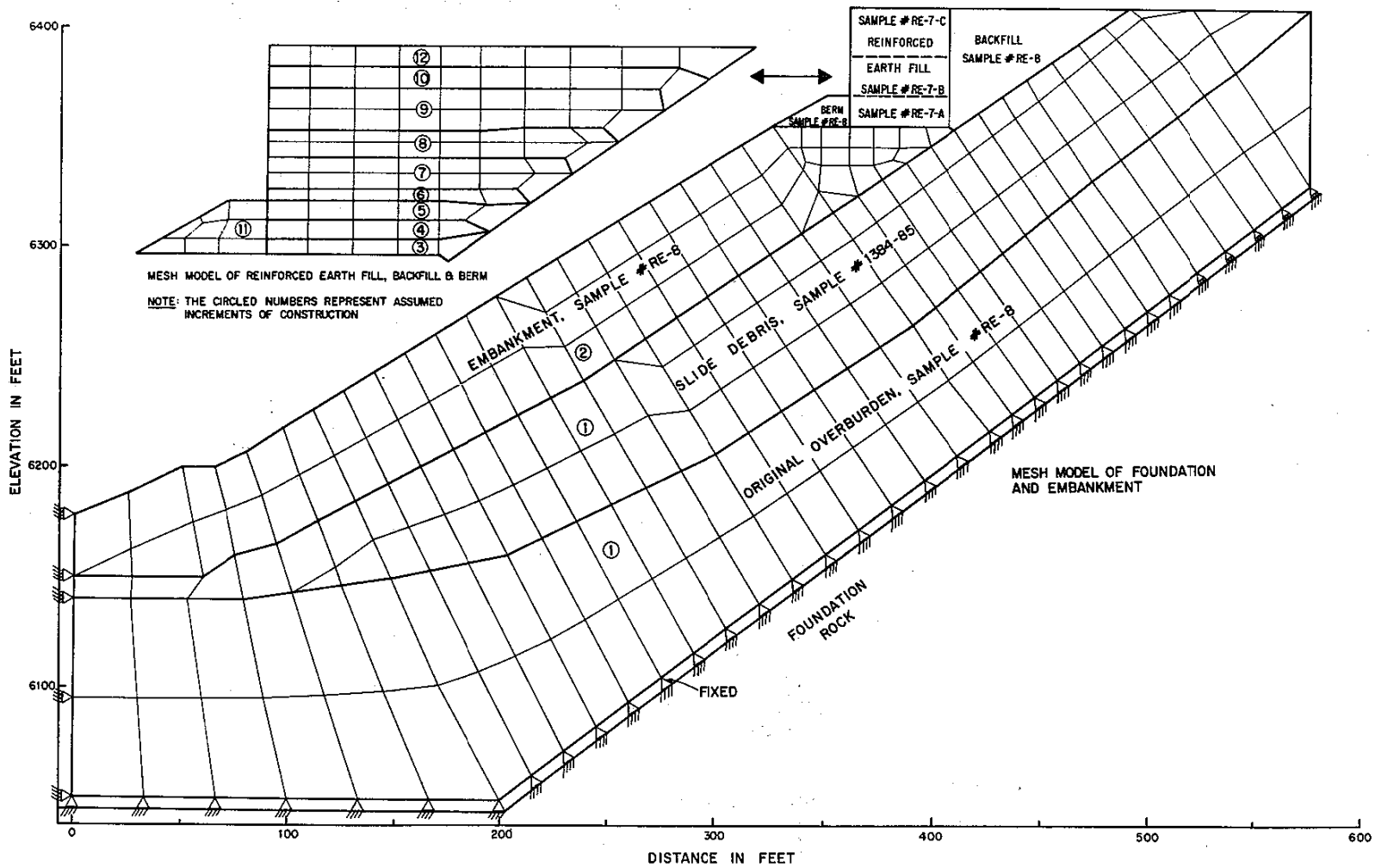
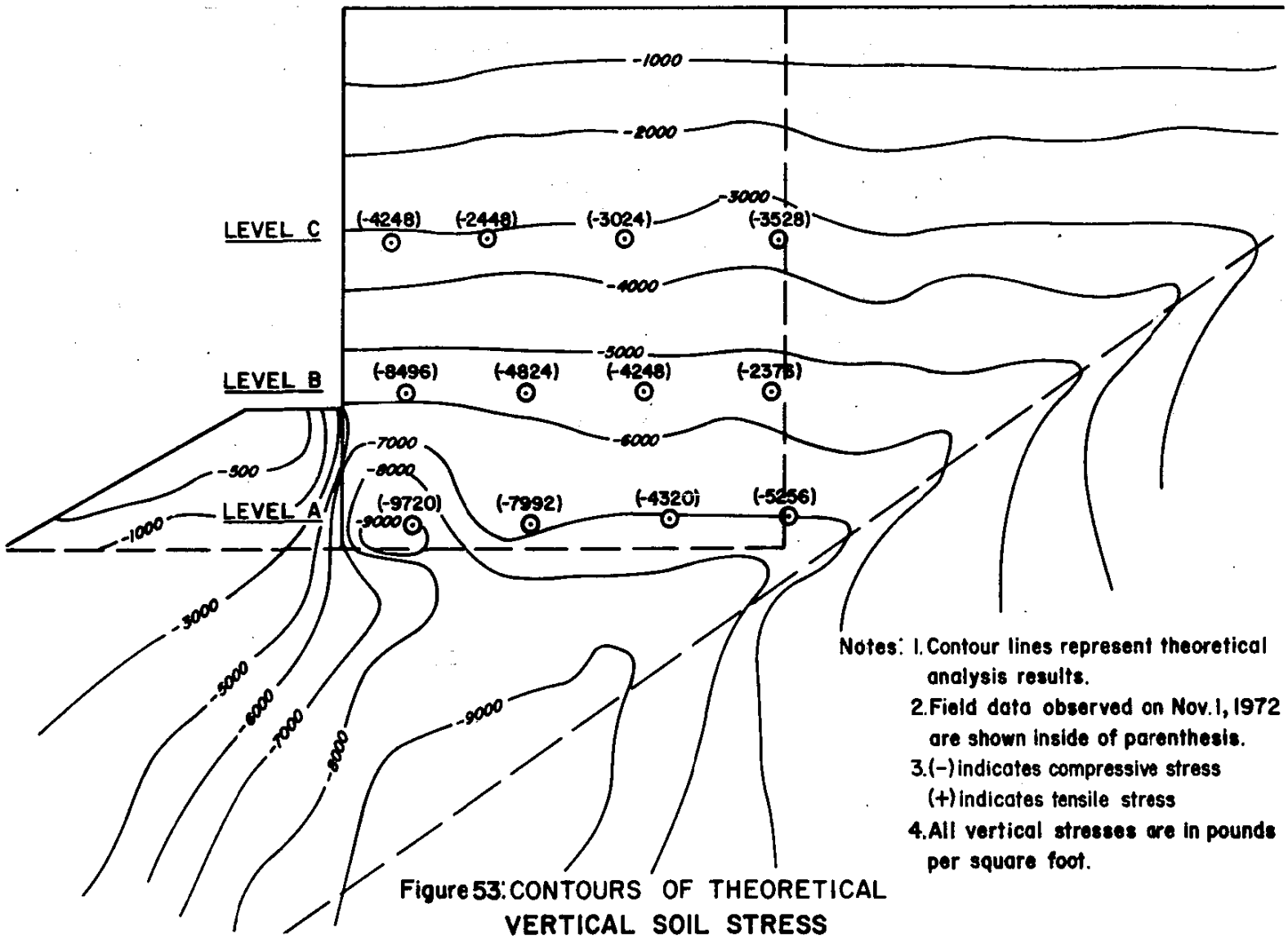



FIGURE 52: TYPICAL SECTION FOR FINITE ELEMENT ANALYSIS, STATION 551+75




Notes: 1. Contour lines represent theoretical analysis results.
2. Field data observed on Nov. 1, 1972 are shown inside of parenthesis.
3. (−) indicates compressive stress
(+) indicates tensile stress
4. All vertical stresses are in pounds per square foot.

Figure 53: CONTOURS OF THEORETICAL VERTICAL SOIL STRESS

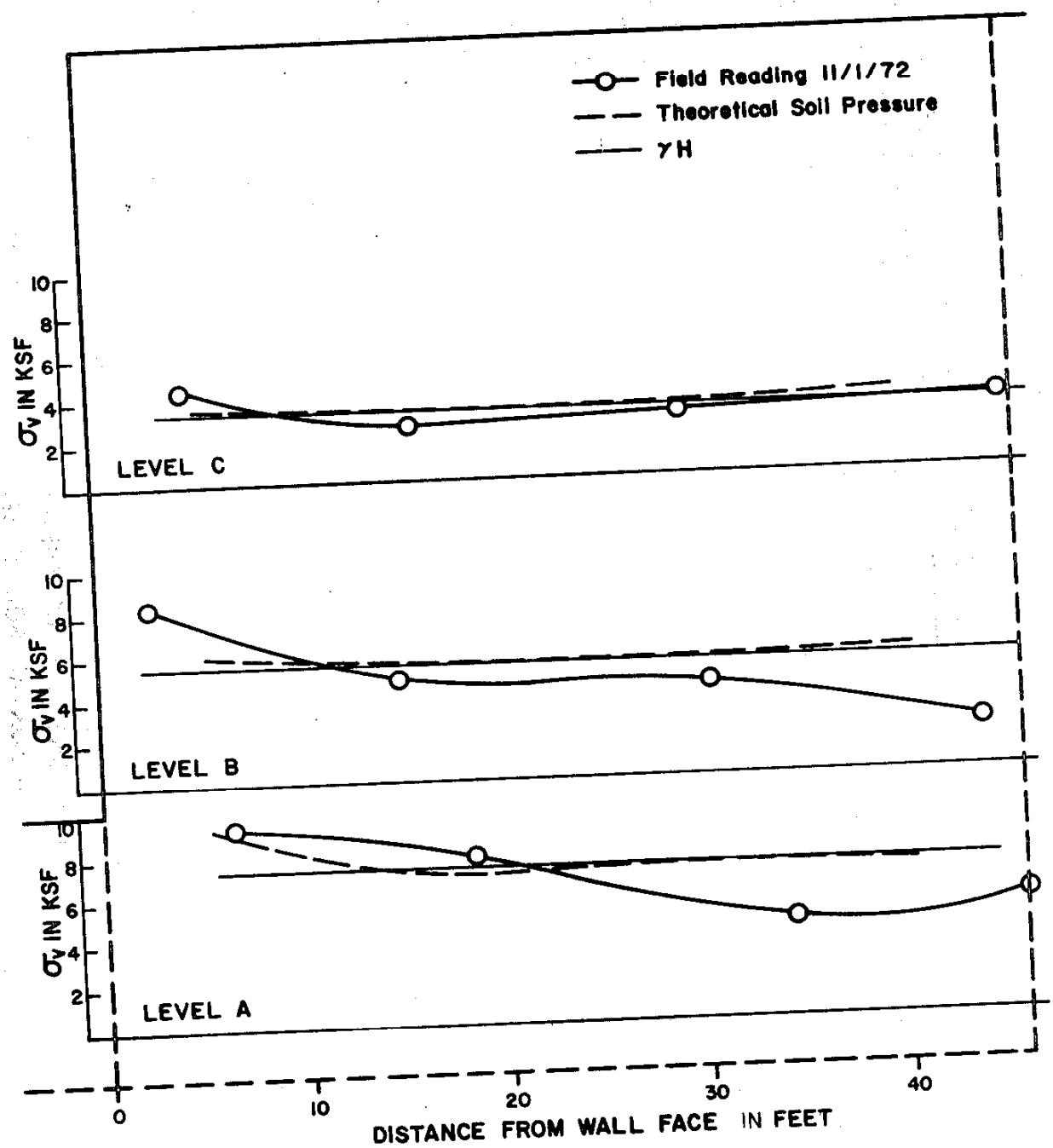
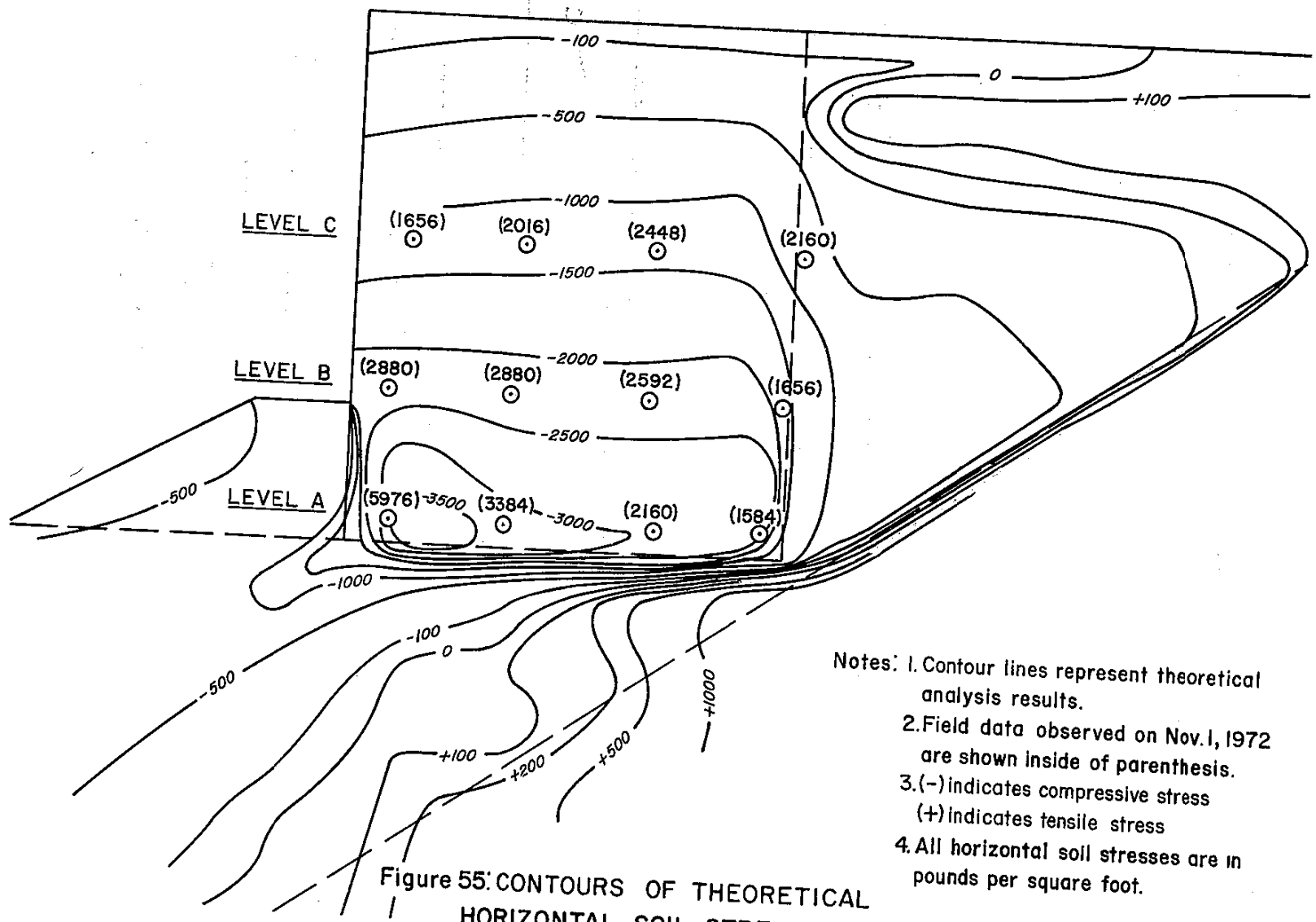



Figure 54: COMPRESSIVE VERTICAL SOIL STRESS DISTRIBUTION, STA. 551+75




Notes: 1. Contour lines represent theoretical analysis results.
2. Field data observed on Nov. 1, 1972 are shown inside of parenthesis.
3. (−) indicates compressive stress
(+) indicates tensile stress
4. All horizontal soil stresses are in pounds per square foot.

Figure 55: CONTOURS OF THEORETICAL HORIZONTAL SOIL STRESS

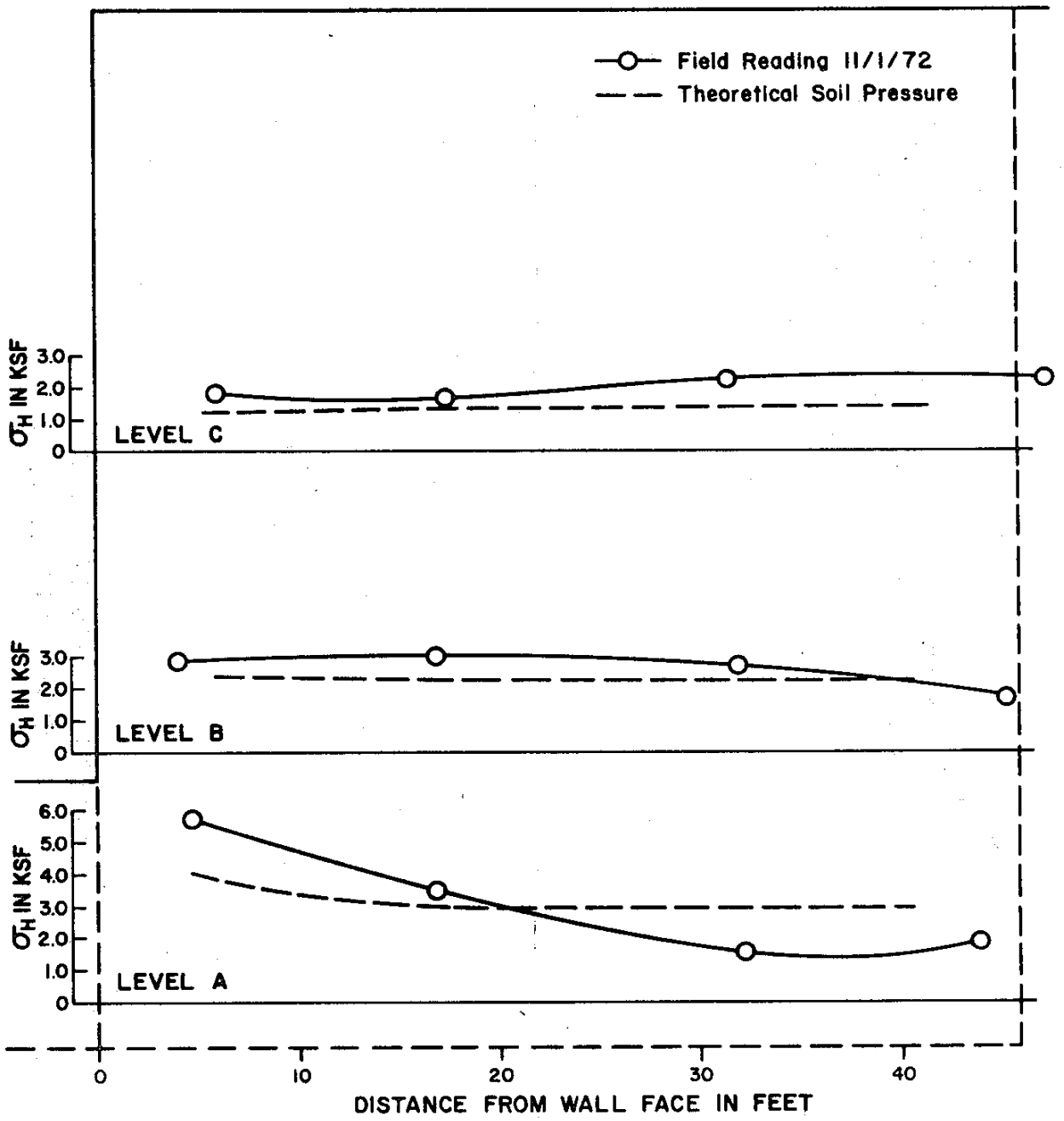
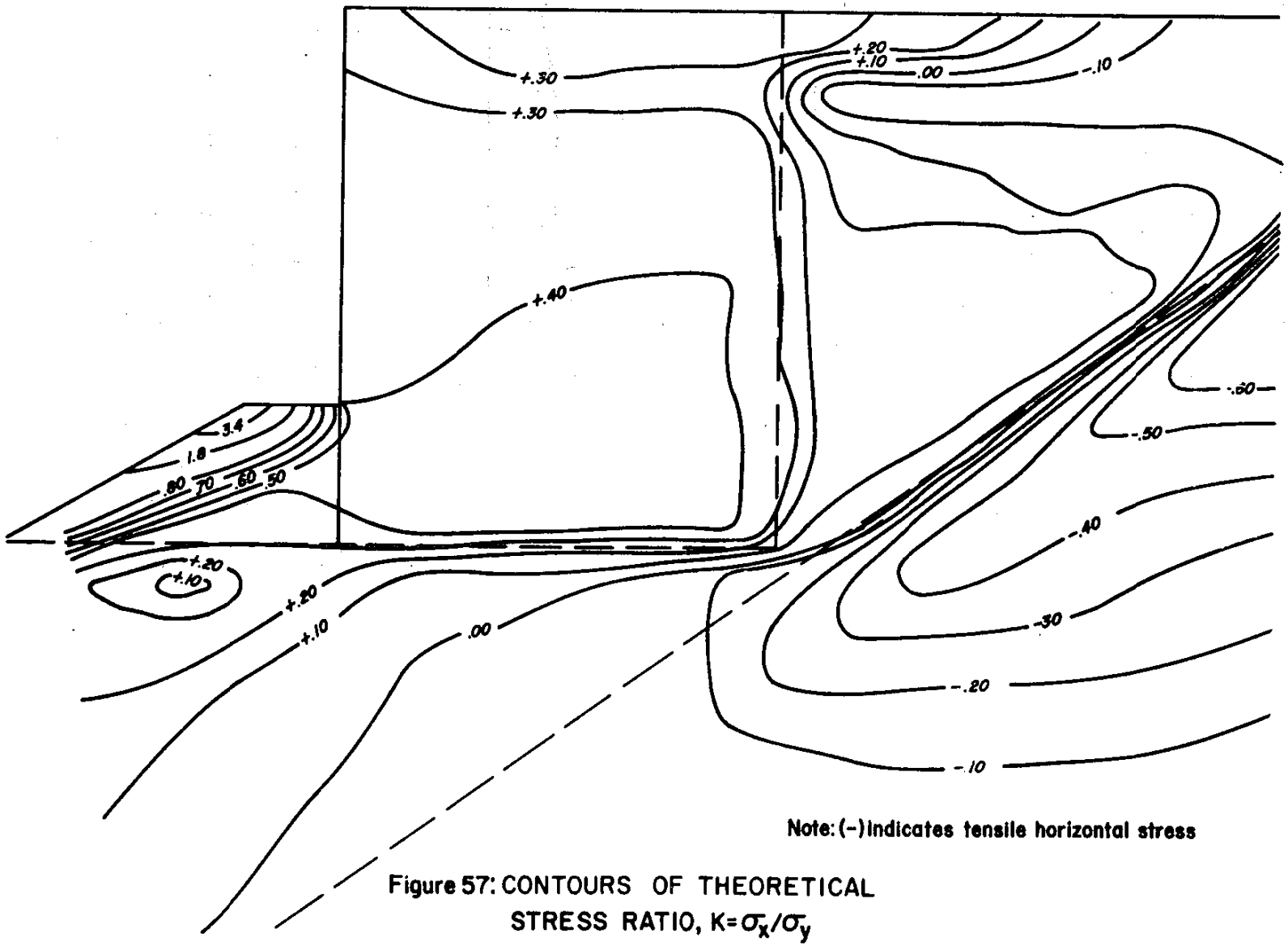
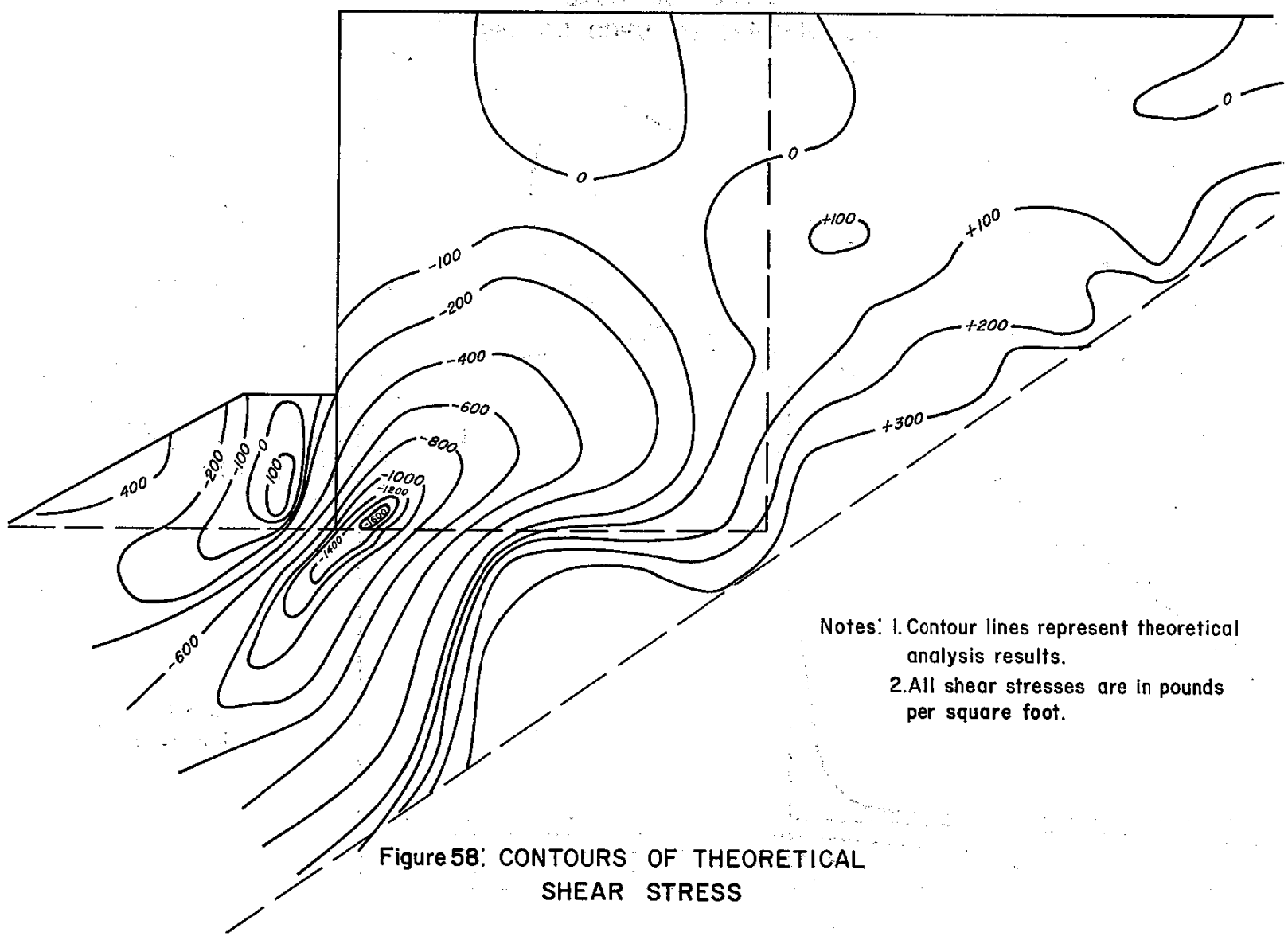



**Figure 56 COMPRESSIVE HORIZONTAL SOIL STRESS DISTRIBUTION, STATION 551+75**



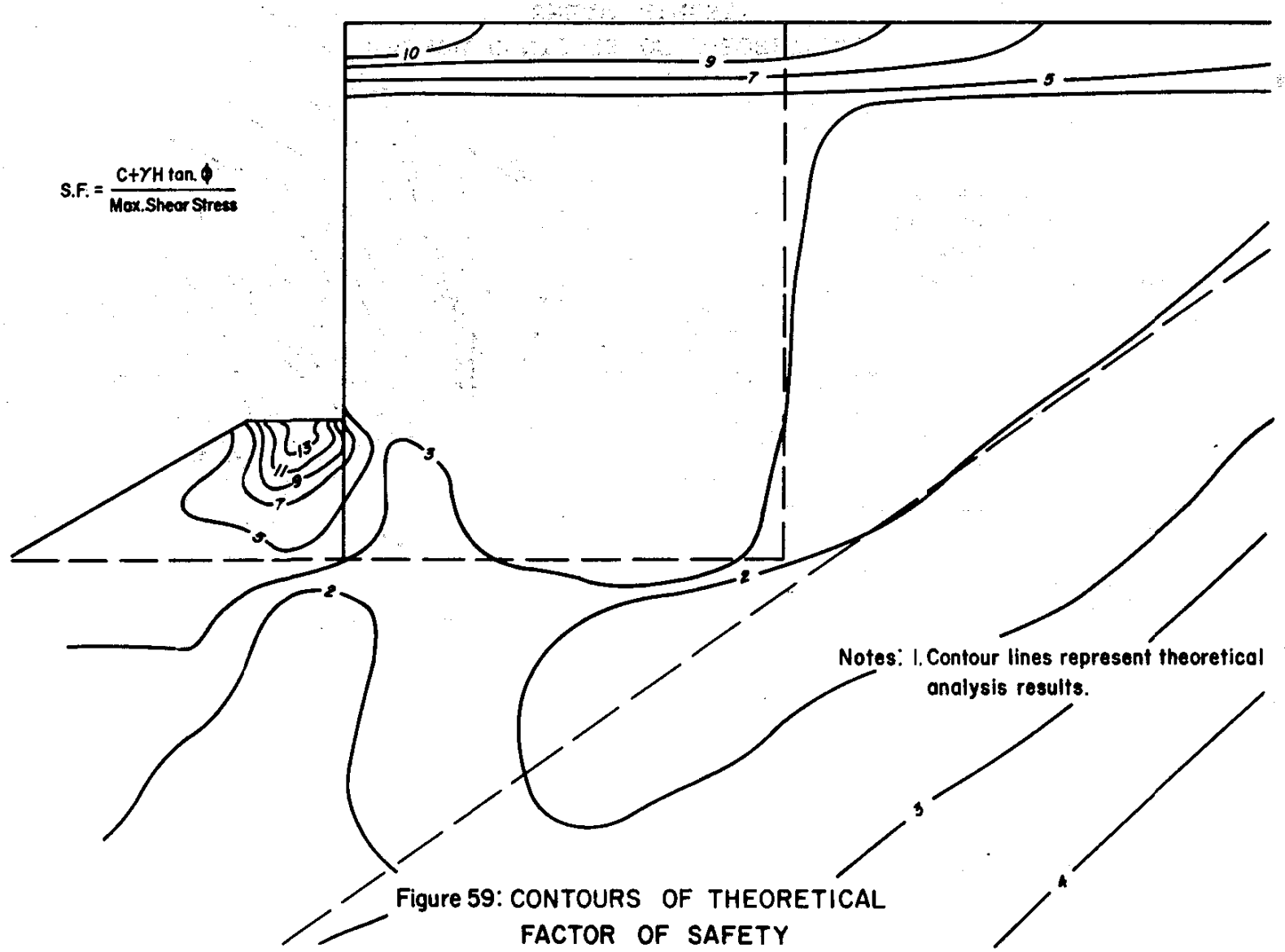

Note: (-) indicates tensile horizontal stress

Figure 57: CONTOURS OF THEORETICAL STRESS RATIO, $K = \sigma_x / \sigma_y$



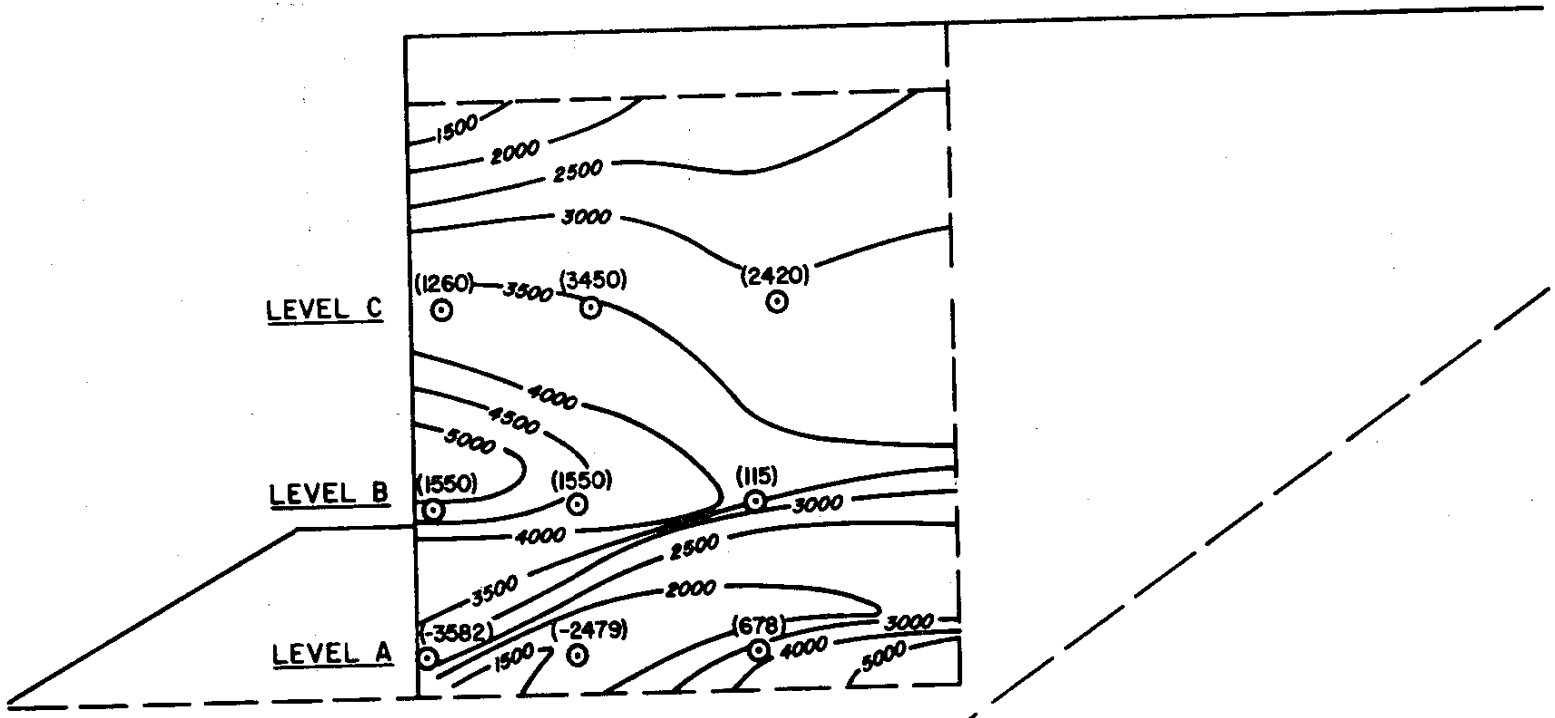

Notes: 1. Contour lines represent theoretical analysis results.
2. All shear stresses are in pounds per square foot.

Figure 58: CONTOURS OF THEORETICAL SHEAR STRESS




Notes: 1. Contour lines represent theoretical analysis results.

Figure 59: CONTOURS OF THEORETICAL FACTOR OF SAFETY




Notes: 1. Contour lines represent theoretical analysis results.
2. Field data observed on Nov. 1, 1972 are shown inside of parenthesis.
3. (−) indicates compressive stress
(+) indicates tensile stress
4. All steel forces are in pounds

Figure 60: CONTOURS OF THEORETICAL STEEL STRIP FORCES

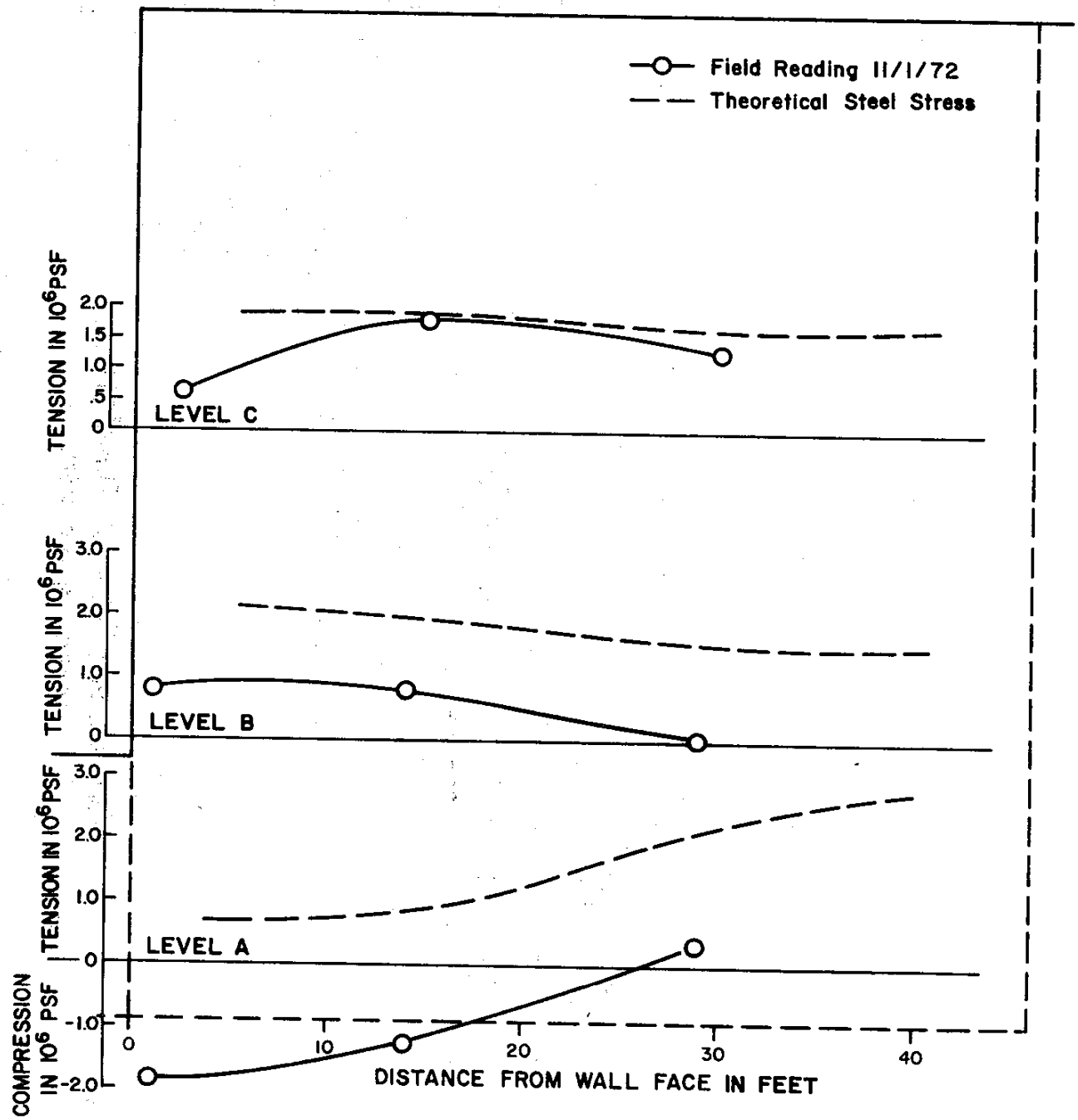



Figure 61: DISTRIBUTION OF STEEL STRIP STRESS, STATION 551 + 75

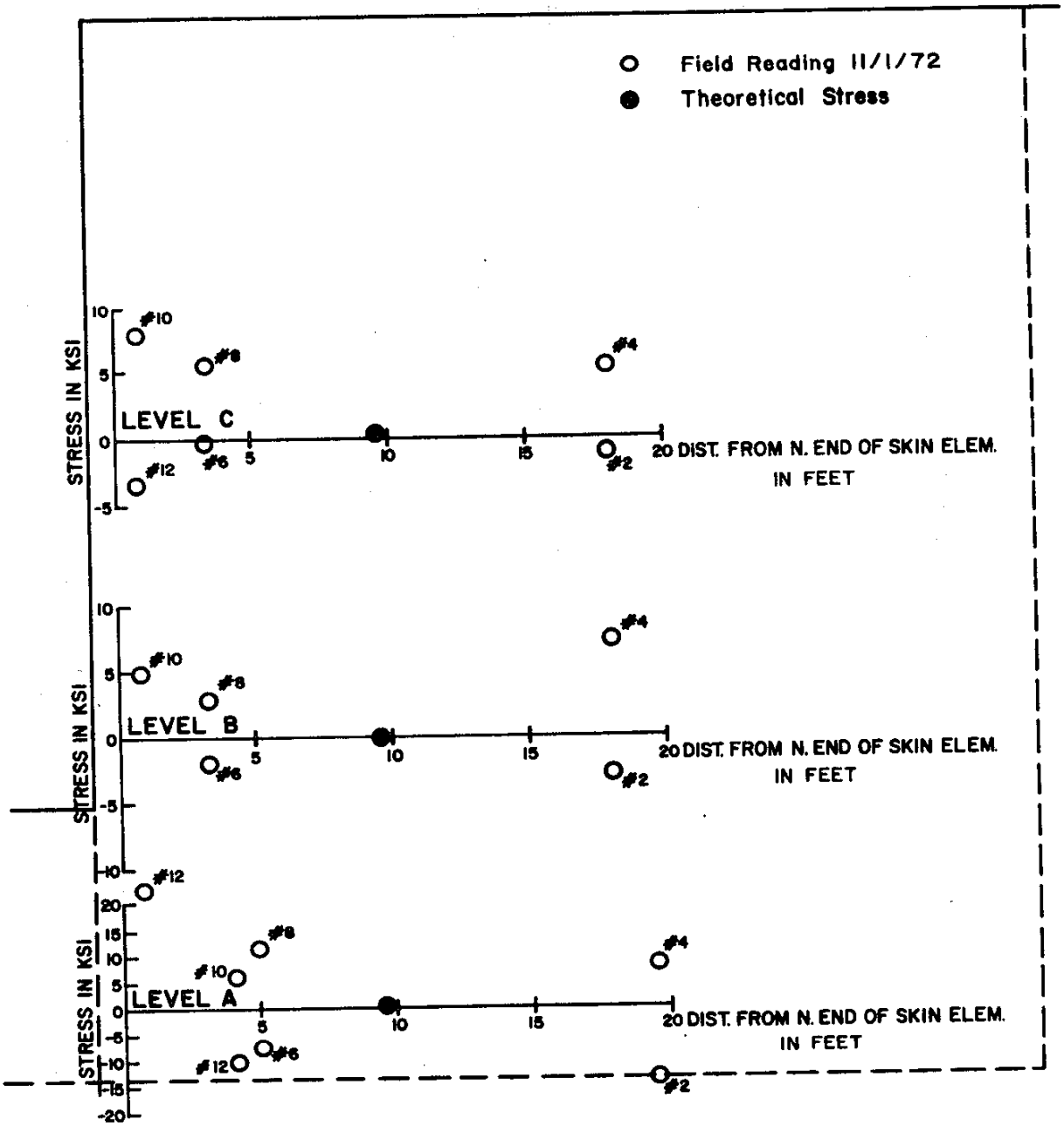



Figure 62: COMPARISON OF THEORETICAL AND FIELD STRESS IN SKIN PLATE

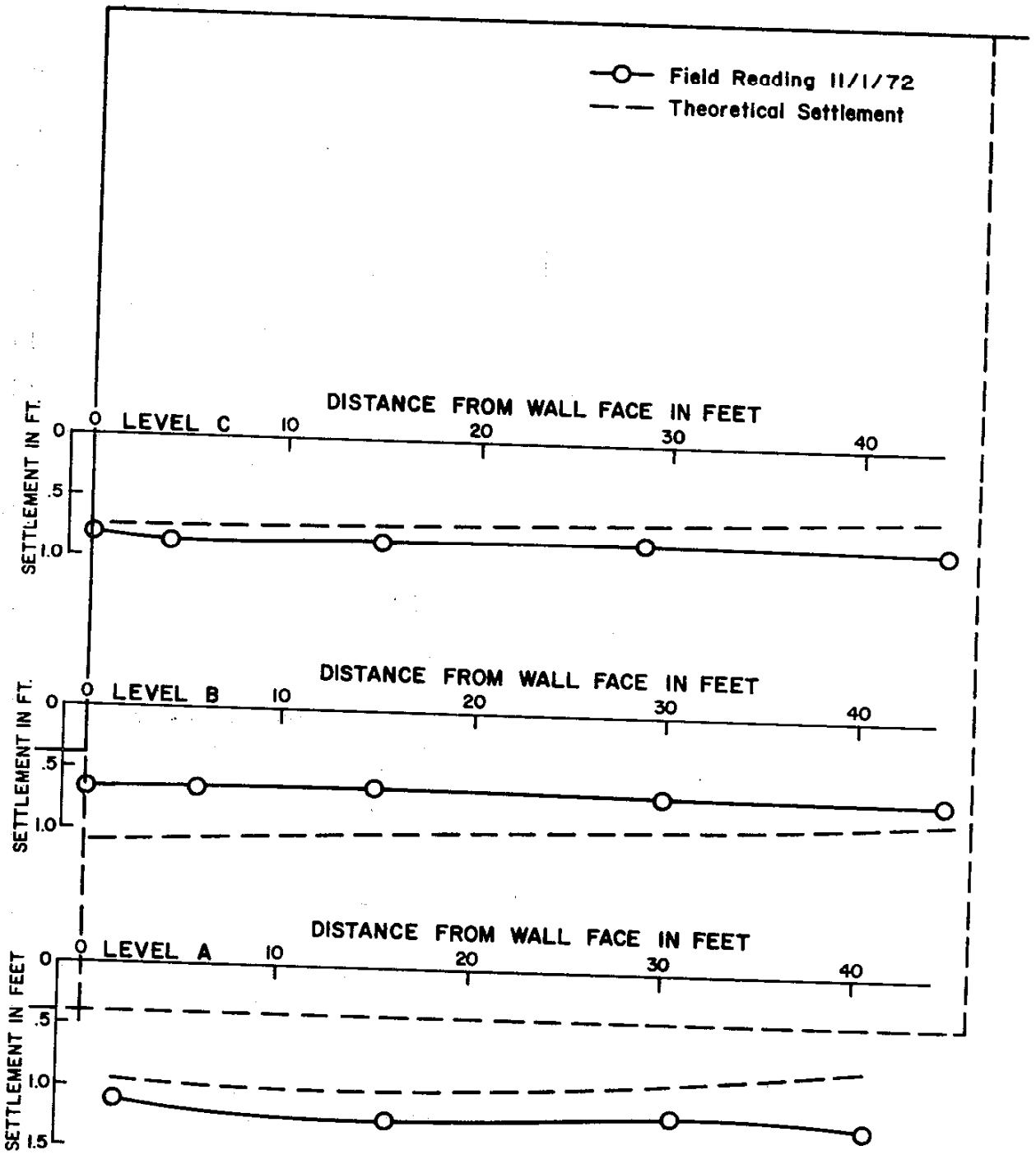



Figure 63: SETTLEMENT WITH RESPECT TO BERM READOUT POINT, STA. 551+75

# APPENDIX A

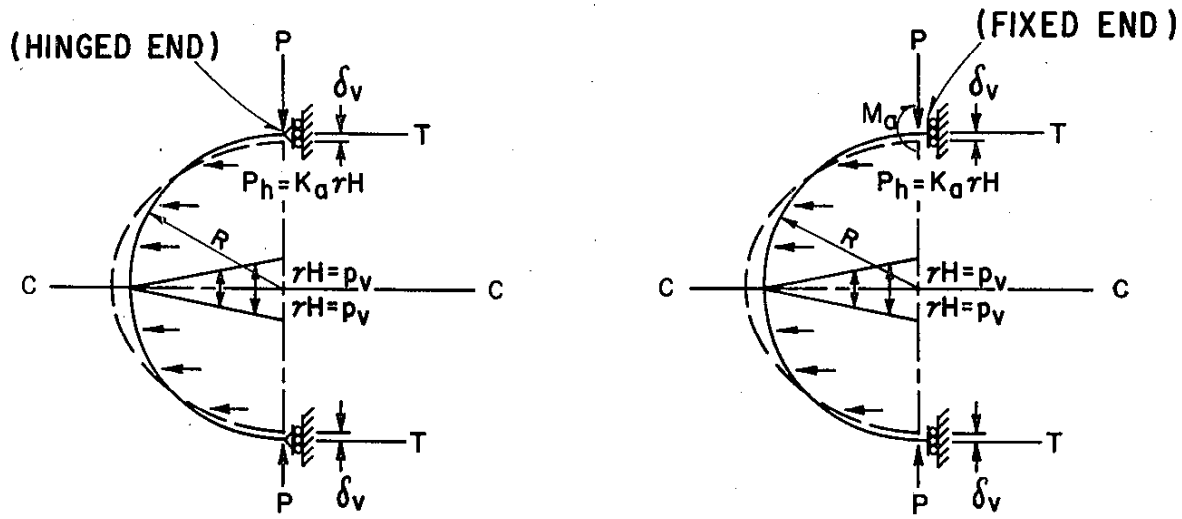
## DERIVATION OF EQUATIONS FOR ANALYSIS OF STRESSES IN SKIN PLATE

by

JERRY C. CHANG

DERIVATION OF EQUATIONS FOR ANALYSIS
OF STRESSES IN SKIN PLATE

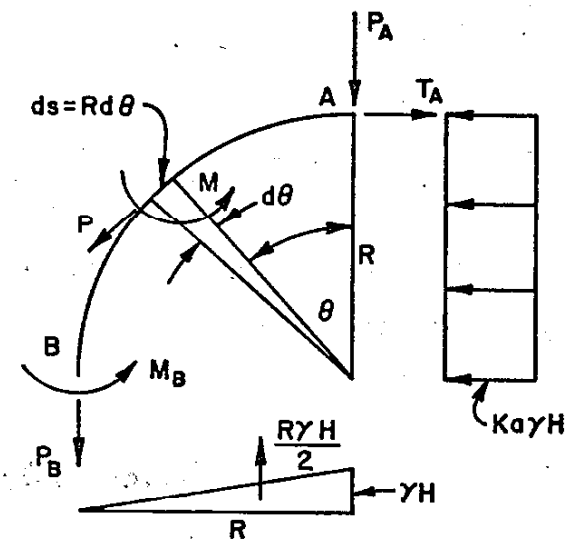
In order to analyze the stress in the skin plate, the redundant force, P, for the hinged end condition and additional redundant moment, $M_a$, for the fixed end condition must be solved (Figure A-1). The solutions of these two unknown are derived as follows:




LOADING DIAGRAM ON SKIN PLATE

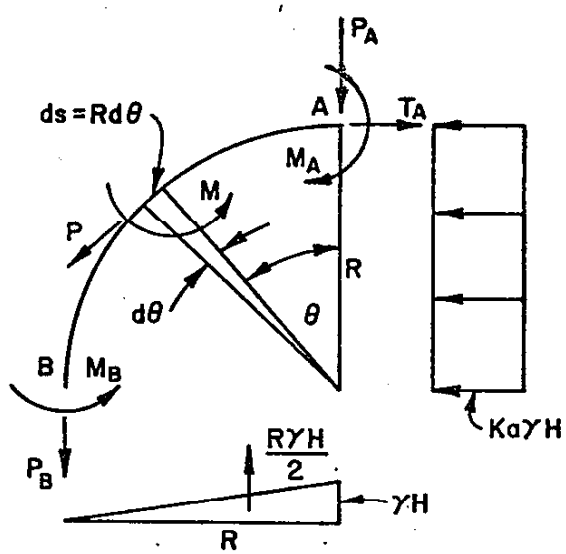
FIGURE A-1

A free body is cut through Section C-C (Figure A-1) and is shown in Figure A-2 for the hinged end condition and Figure A-3 for the fixed end condition. Due to symmetry, only one-half of the semi-circle needs to be analyzed.




HINGED END

FIGURE A-2




FIXED END

FIGURE A-3

Using the strain energy principles described by any text book of structural theory, for example, Seely and Smith (27)* strain energy, U, is equal to

$$U = \int \frac{M^2 R d\theta}{2EI}, \qquad (1)$$

and the deflection $\delta$ is equal to

$$\delta v = \int \frac{M}{EI} \frac{\partial M}{\partial P_A} ds. \qquad (2)$$

For the hinged end condition, using the notation and loading shown in Figure A-2, it can be shown that the moment, M, at any where in the quadrant is equal to

*Reference of the main body of this report.

$$M = P_A \; R \; \sin\theta + T_A \; R(1-\cos\theta) - \frac{K_a \gamma H R^2}{2}(1-\cos\theta)^2$$

$$-\gamma H(1-\sin\theta)\frac{R^2 \sin^2\theta}{2}$$

$$-\frac{R\sin\theta}{2}\gamma H \; \sin\theta \, \frac{2}{3} R \sin\theta \quad . \qquad \text{-----} \quad (3)$$

Substituting ds = R dθ into equation 2, yields

$$\delta v_A = \frac{R}{EI}\int_0^{\pi/2} M \frac{\partial M}{\partial P_A} d\theta \quad . \qquad \text{----------} \quad (4)$$

Substituting Equation 3 into Equation 4 and integrating over the quadrant, Equation 4 yields

$$\delta v_A = \frac{P_A \pi R^3}{4EI} + \frac{K_a \gamma H R^4}{3EI} + \frac{\gamma H R^4}{96EI}(3\pi - 32) \quad . \qquad \text{----------} \quad (5)$$

Solving Equation 5 in terms of $P_A$, then

$$P_A = \frac{4EI\,\delta v_A}{\pi R^3} - \frac{4K_a \gamma H R}{3\pi} - \frac{\gamma H R}{24\pi}(3\pi - 32) \quad . \qquad \text{----------} \quad (6)$$

For the fixed end condition, using the notation and loading shown in Figure A-3, the moment, M, at any where in the quadrant is

$$M = P_A \; R \; \sin\theta + T_A \; R(1-\cos\theta) + M_A$$

$$-\frac{K_a \gamma H R^2}{2}(1 - 2\cos\theta + \cos^2\theta)$$

$$-\frac{R^2 \gamma H}{2}(\sin^2\theta - \sin^3\theta) - \frac{\gamma H R^2}{3}\sin^3\theta \quad . \qquad \text{----------} \quad (7)$$

Substituting Equation 7 into Equation 4 and integrating over the quadrant, then

$$\delta v_A = \frac{M_A R^2}{EI} + \frac{R^3}{4EI}(P_A \pi + 2\,T_A) + \frac{R^4 \gamma H}{96EI}(3\pi - 16Ka - 32) \quad \text{-------} \quad (8)$$

At the fixed end, A, the angle of rotation, $\theta_A$, is expressed as

$$\theta_A = \int_0^{\pi/2} \frac{M}{EI}\,\frac{\partial M}{\partial M_A}\,ds = \frac{R}{EI}\int_0^{\pi/2} M\,d\theta = 0 \quad \text{----------} \quad (9)$$

Substituting Equation 7 into Equation 9 and integrating over the quadrant, then

$$\theta_A = \frac{P_A R^2}{EI} + \frac{T_A R^2}{EI}\left(\frac{\pi}{2} - 1\right) + \frac{\pi M_A R}{2EI} + \frac{Ka\gamma HR^3}{8EI}(8 - 3\pi)$$

$$- \frac{\gamma HR^3}{24EI}(3\pi - 8) - \frac{2\gamma HR^3}{9EI} = 0 \quad \text{----------} \quad (10)$$

Solve Equation 8 and 10 simultaneously for $P_A$ and $M_A$, then

$$P_A = \frac{\delta v_A\, EI}{\pi R^3}\left(4 - \frac{32}{8 - \pi^2}\right) + \gamma HR\left(\frac{4 - 4Ka}{3\pi} - \frac{1}{8}\right)$$

$$- \frac{8\gamma HR}{8 - \pi^2}\left(\frac{4 - 4Ka}{3\pi} - \frac{(1 + \pi - \pi Ka)}{8} + \frac{1}{9}\right), \quad \text{----------} \quad (11)$$

and

$$M_A = \frac{8\,\delta v_A\,EI}{R^2(8-\pi^2)} + \frac{2\pi\gamma HR^2}{(8-\pi^2)}\left(\frac{4-4Ka}{3\pi} - \frac{(1+\pi-\pi Ka)}{8} + \frac{1}{9}\right). \quad \text{---------} \quad (12)$$

In summary:

For hinged end conditions,

$$P_A = \frac{4EI\,\delta v_A}{\pi R^3} - \frac{4Ka\gamma HR}{3\pi} - \frac{\gamma HR}{24\pi}(3\pi-32) \quad ;$$

and for fixed end conditions,

$$P_A = \frac{\delta v_A\,EI}{\pi R^3}\left(4-\frac{32}{8-\pi^2}\right) + \gamma HR\left(\frac{4-4Ka}{3\pi} - \frac{1}{8}\right)$$

$$- \frac{8\gamma HR}{8-\pi^2}\left(\frac{4-4Ka}{3\pi} - \frac{(1+\pi-\pi Ka)}{8} + \frac{1}{9}\right) \quad ;$$

and

$$M_A = \frac{8\,\delta v_A\,EI}{R^2(8-\pi^2)} + \frac{2\pi\gamma HR^2}{(8-\pi^2)}\left(\frac{4-4Ka}{3\pi} - \frac{(1+\pi-\pi Ka)}{8} + \frac{1}{9}\right) .$$

# APPENDIX B

# MATERIAL PROPERTIES OF REINFORCED EARTH

By

K. M. ROMSTAD

L. R. HERRMANN

# INTRODUCTION

In order to be able to quickly and economically evaluate the structural reliability of proposed reinforced earth structures it is necessary that analysis procedures applicable to such structures be available. There are two obvious approaches to the analysis of such reinforced structures: One possible approach is to attempt to analyze the structure in such a way that each and every reinforcing element is considered in detail. Due to projected excessive computer costs and the high probability of numerical difficulties such detailed analyses appear not to be feasible for real structures. The second approach involves the consideration of the reinforced earth as a "composite material" with associated "composite properties" which represent the overall structural response of the material. This latter approach may be applied with relative ease to very complicated structures and is the one pursued herein.

The use of composite materials for Civil Engineering applications is ages old, e.g., plain concrete (i.e., mortar reinforced with aggregate) and reinforced concrete. Correspondingly "strength of materials" theories have long been available for the analysis of structures made of such materials. During the past 15 years the use of new and exotic composite materials has become commonplace for aerospace applications and extensive theories have been developed for explaining their behaviors. Although on the surface

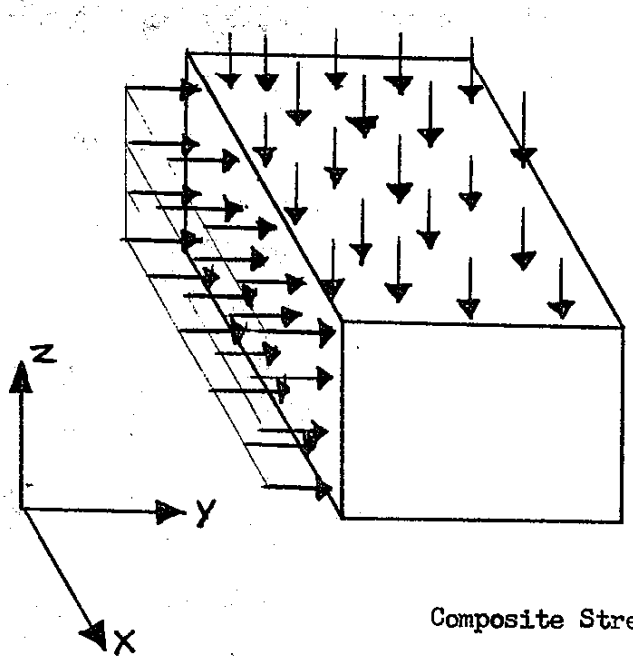
the bases for these theories may appear to differ from those used for the strength of materials theories for concrete structures, in reality they do not. The work reported herein follows directly from that reported in reference (1); an introduction to some of the extensive literature in this field may be found in reference(2).

The theory of composite material behavior may be derived from several different points of view (all leading to substantially the same result). The approach followed herein is to recognize that if the reinforcing pattern is repeated a sufficiently large number of times the material can be considered homogeneous at the phenomenological level (or as an inhomogeneous material in which the changing properties reflect only changes in the reinforcing pattern). The consideration of the reinforced material as homogeneous at the phenomenological level is analogous to the consideration of a microscopically crystalline material as macroscopically homogeneous (e.g., the treatment of steel as a homogeneous isotropic material) or to the accounting for the reinforcement in a concrete beam by the use of transformed section properties, etc. The reinforced material when viewed at the composite level will, in general, exhibit anisotropic behavior. Once the appropriate composite properties are determined standard analysis procedures (e.g., finite element procedures) may be used to analyze reinforced earth structures.

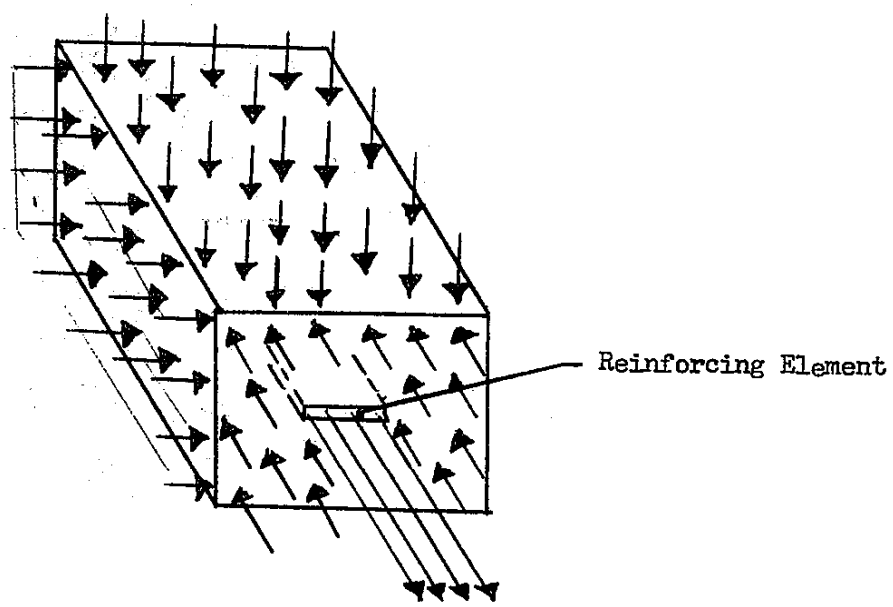
## REINFORCED EARTH UNIT CELL

The experimental determination of the complete array of composite properties is often very difficult and expensive, fortunately a well developed theory exists for the relating of these properties to the known properties of the individual component materials (soil and steel in this case) and to the geometric arrangement of the reinforcement.

For a material that has a regular reinforcing pattern one can, in general, find a small unit of the material which when repeated in all directions results in the actual configuration of the composite material; in this report this fundamental building block is called the "unit cell". The average values of the stresses distributed over the cell faces are equal to the stresses in the equivalent composite material and thus the average response of the unit cell to a state of stress or strain is the same as the composite response of the material. Hence, the desired composite properties may be calculated from a consideration of the behavior of the unit cell and once the composite stress state is determined at a particular point in a reinforced earth structure the corresponding constituent stress state may be determined by returning to the unit cell. Figure B-1 illustrates a particular composite stress state and the corresponding stress state at the constituent level of the reinforced material.




Composite Stress State ($\sigma_x = 0$)




Corresponding Local Stress State

Figure B-1 Illustration of Composite Stress Concept

The unit cell for the reinforced earth structures under consideration is shown in Figure B-2. The composite material considered consists of a soil with thin steel strips parallel to each other at chosen spacings and extending deep into the soil mass. The 1 axis in Figure B-2 is chosen parallel to the strips and the 2 and 3 axes form a plane perpendicular to the longitudinal axis of the strips and are aligned with the principle axes of the strips. For a given reinforcing pattern all strips in a given 1-3 plane are assumed to be equally spaced, b, and the 1-3 planes containing the strips in the reinforced earth are present in parallel layers of spacing, d, (where b and d may vary from layer to layer). When the composite material is subjected to a homogeneous stress or strain state, those cells which are sufficiently far removed from the surface of the material to avoid surface effects must satisfy the conditions, (1) all unit cells will exhibit identical deformation and stress states, (2) the averages of the unit cell stresses and strains are equal to the phenomenological stresses and strains of the composite and (3) there must be continuity of the displacement and traction vectors across all cell interfaces.

## COMPOSITE STRESS-STRAIN RELATIONSHIP FOR REINFORCED EARTH

The anisotropic phenomological behavior of the composite material (i.e., reinforced earth) may be described by the equations:

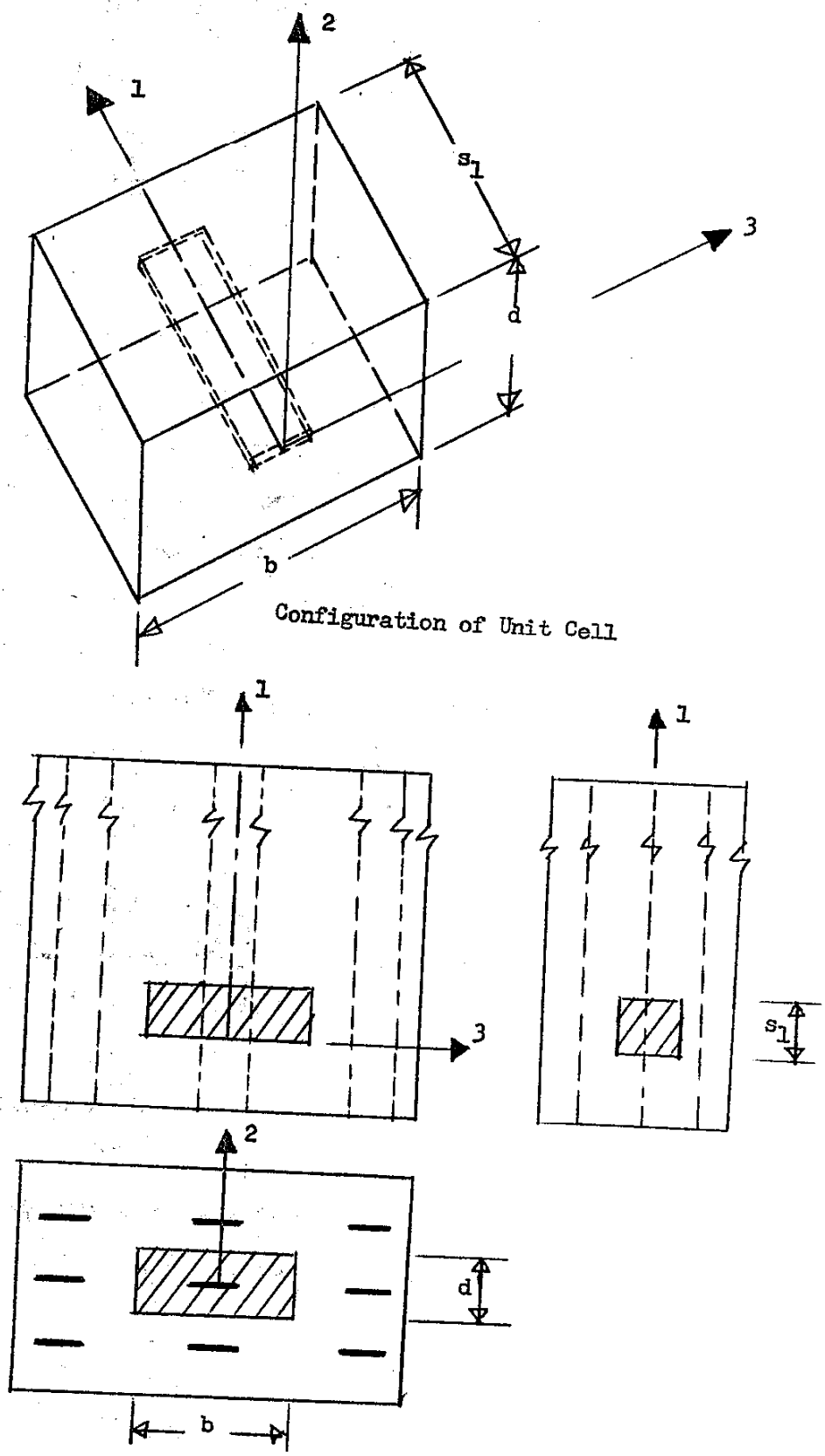



Figure B-2 Unit Cell Representation of Reinforced Earth

## Strain - Stress Relationship

$$\begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \epsilon_3 \\ \gamma_{12} \\ \gamma_{13} \\ \gamma_{23} \end{bmatrix} = \begin{bmatrix} c_{11} & c_{12} & c_{13} & & & \\ c_{12} & c_{22} & c_{23} & & & \\ c_{13} & c_{23} & c_{33} & & & \\ & & & c_{44} & & \\ & & & & c_{55} & \\ & & & & & c_{66} \end{bmatrix} \begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_{12} \\ \sigma_{13} \\ \sigma_{23} \end{bmatrix} \quad (1)$$

The composite properties may be theoretically predicted by determining the average response of the unit cell to various applied homogeneous composite stress or strain states. The most accurate solution to this problem would require a detailed solution of a complicated three-dimensional boundary value problems, possibly by the finite element method. Fortunately however, the characteristics of the reinforced earth unit cell make some approximations possible which greatly simplify the problem. The most significant characteristic is that the percentage of reinforcement is extremely small (much less than 1% by volume). This characteristic leads to the assumption of the strains in the composite being equal to the strains in the soil.

The composite properties were predicted by considering the response of the unit cell to an arbitrary composite stress state and predicting the resulting composite strain state. The most significant considerations utilized in developing the properties were

the assumptions that the composite stress-strain state in the 2 and 3 directions equaled the soil stress-strain state and the displacements of all points in any 2-3 plane are equal for both soil and strip.

Any arbitrary composite stress state may be expressed as the sum of a series of simple stress states, i.e.,

$$\begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_{12} \\ \sigma_{13} \\ \sigma_{23} \end{bmatrix}_{\text{arbitrary}} = \begin{bmatrix} \sigma_1 \\ \sigma_0 \\ \sigma_0 \\ \sigma_0 \\ \sigma_0 \\ \sigma_0 \end{bmatrix} + \begin{bmatrix} \sigma_0 \\ \sigma_2 \\ \sigma_0 \\ \sigma_0 \\ \sigma_0 \\ \sigma_0 \end{bmatrix} + \cdots \begin{bmatrix} \sigma_0 \\ \sigma_0 \\ \sigma_0 \\ \sigma_0 \\ \sigma_0 \\ \sigma_{12} \end{bmatrix}$$

Consider the first of these simple stress states, i.e.,

$$\sigma_1 = \sigma; \quad \sigma_2 = \sigma_3 = \sigma_{12} = \sigma_{13} = \sigma_{23} = 0 \qquad (2)$$

Equation (1) then yields

$$c_{11} = \epsilon_1 / \sigma \qquad (3)$$

$$c_{12} = \epsilon_2 / \sigma \qquad (4)$$

$$c_{13} = \epsilon_3 / \sigma \qquad (5)$$

The applied composite stress $\sigma$ acting over the composite area bd must equal the sum of the strip stress, $\sigma^{st}$, acting over the strip area, $A^{st}$, and the soil stress, $\sigma^{so}$ acting over the soil area, $A^{so}$

(Fig.B-1). Note that the soil area and the composite area are essentially equal for the reinforced earth systems under consideration ($bd = A^c = A^{so}$)

$$\sigma A^c = \sigma_1^{so} A^c + \sigma_1^{st} A^{st} \quad (6)$$

$$\sigma_2 = \sigma_2^{so} = 0 \quad (7)$$

$$\sigma_3 = \sigma_3^{so} = 0 \quad (8)$$

The superscripts c, so, and st refer to composite, soil and strip respectively.

It follows from the strain displacement relationships and the previous assumptions that

$$\epsilon_1 = \epsilon_1^{so} = \epsilon_1^{st} \quad (9)$$

$$\epsilon_2 = \epsilon_2^{so} \quad (10)$$

$$\epsilon_3 = \epsilon_3^{so} \quad (11)$$

The constitutive equations for the soil and strip must be satisfied which, consistent with the assumptions made, become

$$\epsilon_1^{so} = (1/E^{so})\, \sigma_1^{so} \quad (12)$$

$$\epsilon_1^{st} = (1/E^{st})\, \sigma_1^{st} \quad (13)$$

Substitute the strain-stress Equations 12 and 13 into Equation 9 to obtain the relationship

$$\sigma_1^{so} = \frac{E^{so}}{E^{st}} \sigma_1^{st} \tag{14}$$

which may then be substituted into Equation 6 to yield the relationships

$$\sigma_1^{st} = \frac{A^c E^{st}}{A^c E^{so} + A^{st} E^{st}} \tag{15}$$

$$\sigma_1^{so} = \frac{A^c E^{so}}{A^c E^{so} + A^{st} E^{st}} \tag{16}$$

Using Equations (3), (4) and (5) the composite material properties $C_{11}$, $C_{12}$, and $C_{13}$ may then be solved for from the relationships

$$c_{11} = \frac{\epsilon_1}{\sigma} = \frac{\epsilon_1^{so}}{\sigma} = \frac{\sigma_1^{so}}{\sigma E^{so}} = \frac{A^c}{A^c E^{so} + A^{st} E^{st}} \tag{17}$$

$$c_{12} = \frac{\epsilon_2}{\sigma} = \frac{\epsilon_2^{so}}{\sigma} = \frac{-\nu^{so} \sigma_1^{so}}{\sigma E^{so}} = \frac{-\nu^{so} A^c}{A^c E^{so} + A^{st} E^{st}} \tag{18}$$

$$c_{13} = \frac{\epsilon_3}{\sigma} = \frac{\epsilon_3^{st}}{\sigma} = \frac{-\nu^{so} \sigma_1^{so}}{\sigma E^{so}} = \frac{-\nu^{so} A^c}{A^c E^{so} + A^{st} E^{st}} \tag{19}$$

Considering in a similar manner the other five simple stress states into which the arbitrary composite stress state was decomposed yields the values of the other composite properties, i.e., $C_{22}$, $C_{23}$, $C_{33}$, $C_{44}$, $C_{55}$, and $C_{66}$. The final results are:

$$\begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \epsilon_3 \end{bmatrix} = \frac{1}{E^{SO}(1+\alpha)} \begin{bmatrix} 1 & -\nu^{SO} & -\nu^{SO} \\ -\nu^{SO} & 1+\alpha(1-\nu^{SO^2}) & -\nu^{SO}\left[1+\alpha(1+\nu^{SO})\right] \\ -\nu^{SO} & -\nu^{SO}\left[1+\alpha(1+\nu^{SO})\right] & 1+\alpha(1-\nu^{SO^2}) \end{bmatrix} \begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \end{bmatrix}$$

$$\begin{bmatrix} \gamma_{12} \\ \gamma_{13} \\ \gamma_{23} \end{bmatrix} = \begin{bmatrix} G^{SO} & & \\ & G^{SO} & \\ & & G^{SO} \end{bmatrix} \begin{bmatrix} \sigma_{12} \\ \sigma_{13} \\ \sigma_{23} \end{bmatrix} \quad ; \quad \alpha = \frac{A^{st}\ E^{st}}{A^{c}\ E^{SO}} \tag{20}$$

This matrix is inverted to obtain the stress-strain coefficients in a form suitable for use in a finite element displacement formulation.

Reinforced earth structures will generally exhibit behavior assumed in elasticity as plain strain response where the strains $\epsilon_3$, $\gamma_{13}$, and $\gamma_{23}$ are taken to be zero. In the accompanying computer program these strains are assumed to be zero and the resulting stress-strain matrix utilized is of the form,

$$\begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_{12} \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & 0 \\ a_{12} & a_{22} & 0 \\ 0 & 0 & a_{44} \end{bmatrix} \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \gamma_{12} \end{bmatrix} \tag{21}$$

where the $a_{ij}$ coefficients are directly obtained from the inversion of the (C) matrix.

For a given problem if the 1-2 axes do not coincide with the x-y axes the $a_{ij}$ coefficients are appropriately transformed by the program.

## STRESS-STRAIN STATE IN SOIL, STRIP, AND SKIN PLATE

The finite element program utilizes Equation (21) in performing analyses for the composite stresses and strains in a reinforced earth structure. The corresponding strains and stresses in the component materials are obtained in the following manner. The x-y composite stress and strain components are transformed into 1-2 components. Since the composite strain in the 1 direction equals the axial strain in the strip (Equation 9), the force in the strip may be obtained from

$$F^{st} = A^{st} E^{st} \epsilon_1 \qquad (22)$$

When the axial force in the strip has been determined, the stress in the soil in the 1 direction may be obtained from the equilibrium relationship (Equation 6) as

$$\sigma_1^{so} = \sigma_1 - F^{st}/A^c \qquad (23)$$

The normal soil stresses in the 2 and 3 directions and the soil shear stress are assumed to be equal to the composite stresses and all soil strains are assumed to equal the composite strains.

The results from a detailed finite element analysis of the soil, reinforcing strip and skin plate for a small zone of reinforced earth indicated that the bending induced in the skin plate is negligible, and that the only significant stress in the skin plate is the membrane stress. Accordingly, in the accompanying computer program the membrane stress in the skin plate is estimated by approximating it as a circular membrane subjected to the pressure calculated to be acting in the soil at the point in question. If for a particular situation it should be desired to estimate the moment in the skin plate this may be done by a simple subsidiary calculation based on the predicted relative displacements of the membrane edges.

The calculation of moments in the strips is discussed in the following section.

## HIGHER ORDER EFFECTS

The developments of the previous sections are all in the realm of conventional elasticity theory. There exist, however, higher order elasticity theories which in addition to the usual effects account for the so-called "couple-stresses" (e.g., see reference (3)).

That is, not only normal and shear stresses are admitted on an infinitesimal element but also stress couples; beam theory may in fact in some sense be interpreted as a special case of these theories. Experience has shown that for structures of practical interest made of isotropic materials, any effects due to "couple-stresses" are completely unimportant (this is indeed fortuitous as the application of the theory is considerably more complicated than the application of the conventional theory). It appears that this may not be the case for certain composite materials; fortunately reinforced earth does not appear to be one of the composite materials for which the "couple-stress" effects are significant.

The purpose of the steel reinforcing strips in reinforced earth is to develop tensile axial forces and thus to provide tensile strength for the material. However, it is possible, that in addition to the anticipated axial forces, shears and moments may also be developed in the strips. The accounting for the additional stiffness of the reinforced earth which results from the development of these moments and shears would apparently require the use of a "couple-stress" elasticity theory, however, because of the low percentage of reinforcement and because of the strip's small bending rigidity these effects appear to be negligible.

Even though the effects of the moments and shears in the reinforcement are not accounted for in the calculations of the stiffness

of the composite a knowledge of their values is of interest. Using the results of a conventional analysis (based on the use of the appropriate composite properties) of a reinforced earth structure it is possible to estimate their values. These calculations require only the predicted deformed shape of a reinforcing strip and the bending properties of the strip. In the accompanying finite element computer program quadratic displacement elements (linear strain elements) are used, thus, the curvatures of the reinforcing strips may be simply estimated and hence the resulting moments in the strips are determined. The use of a quadratic displacement element does not make it possible to directly compute the third derivatives of the strip deflections and hence estimates of the strip shears are not obtained. It would appear that they would be rather insignificant.

A second higher order effect which appears to be significant for certain composite materials is the so-called edge effect (it appears that this effect could also be accounted for by the use of a "couple-stress" theory). The edge effect arises because disturbances on the edges of the structure, due to self equilibrating stress distributions, may propagate far into the interior of the structure. For most structures made of isotropic homogeneous materials such disturbances quickly dampen out (St. Venant's principle), however, apparently this is not the case for certain composite materials (it appears that these effects are particularly pronounced when the modulus of the reinforcing element is orders

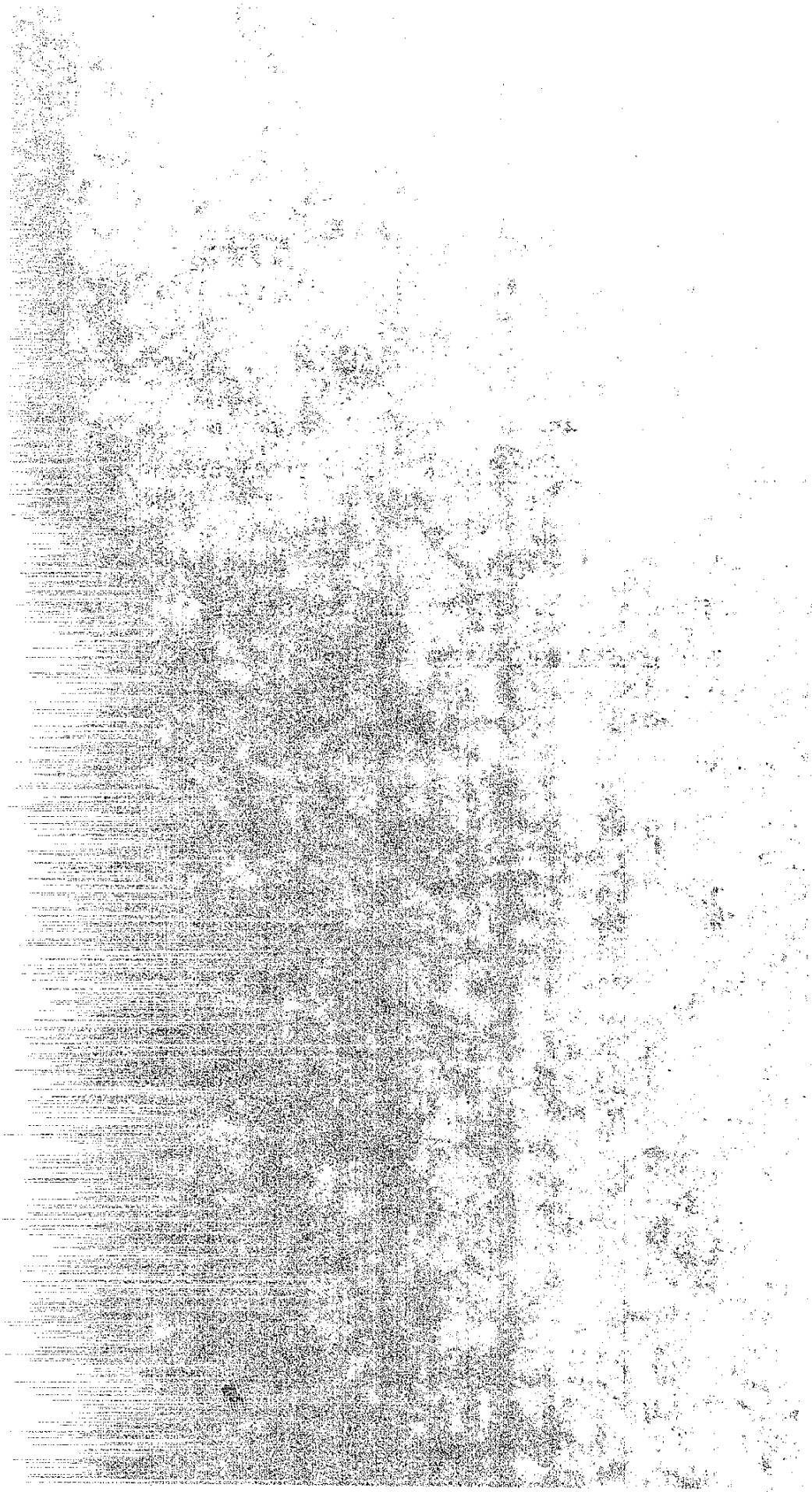
of magnitude greater than for the matrix material). In reinforced earth the presence of the skin plate would appear to essentially negate the edge effects that would otherwise be present and thus it was not necessary to consider these effects.

## REFERENCES


(1) Herrmann, L. R. and K. S. Pister, "Composite Properties of Filament-Resin Systems", ASME Paper No. 63-WA-239, pp. 1-8, Nov. 1963.

(2) Pagano, N. J., S. W. Tsai, "Micromechanics of Composite Media", Composite Materials Workshop, Technomic Publications, Stamfer, Conn., 1966.

(3) Mindlin, R. D., "Influence of Couple-Stresses on Stress Concentrations", Experimental Mechanics, 3, 1963.



APPENDIX C

USER'S MANUAL FOR

# PLANE STRAIN FINITE ELEMENT INCREMENTAL CONSTRUCTION PROGRAM FOR EMBANKMENT AND/OR REINFORCED EARTH ANALYSIS WITH BEAM ELEMENT AND MATERIAL PROPERTY OPTIONS

by

L. R. Herrmann

University of California
Davis, California

July 1972
Revised April 1974

I. CAPABILITIES OF PROGRAM: A brief discussion of the program is given in Commentary B.

II. INPUT*: The input data is entered by means of the following groups of cards.

A1. Title Card (12A6) - Columns 1 to 72 - Any information that is to be printed as a title for the problem.

A2. Control Card (I5, E10.3, 2I5, A4, 2A8) 3

| | |
|---|---|
| Columns 1 - 5 | Number of construction increments |
| Columns 6 - 15 | Plot width (max. 30) |
| Columns 6 - 20 | Output desired<br>0 = complete analysis<br>1 = node point coordinates only |
| Columns 21 - 25 | Change number of construction increments |
| Columns 26 - 29 | Labor cost code |
| Columns 30 - 37 | Name of user |
| Columns 38 - 45 | User's phone number |

A3. Material Cards - For each material type the following information must be supplied: 2,4

1st card (1X, I4, I2, I3, 6E10.5)

Columns 2 - 5 Material Number**

Col. 7 ITYP = 0 - Isotropic Material 4
2 - Orthotropic Material
3 - Reinforced Earth Material
4 - Strip Plate (beam) 17

*The numbers in the right-hand column refer to explanatory comments listed in Commentary A. The input and results for a sample problem are given in Commentary C and the program listing in Commentary D.

**If excavation is to be included in the analysis, see comment number 19 in Commentary A.

| | ITYP = 0 | | | ITYP = 2 | ITYP = 3 | | ITYP = 4 |
|---|---|---|---|---|---|---|---|
| 10** | - | 1 | NP | - | - | 1 | - |
| 11 - 20 | Unit weight ($\gamma$) | | | Unit weight | Unit weight | | A |
| 21 - 30 | - | B | $h_1$ | $C_{11}$ | - | B | I |
| 31 - 40 | E | A | $E_1$ | $C_{12}$ | $E_{soil}$ | A | E |
| 41 - 50 | $\nu$ | $\nu$ | $\nu_1$ | $C_{22}$ | $\nu_{soil}$ | $\nu$ | $\nu$ |
| 51 - 60 | - | $\phi$ | - | $C_{33}$ | - | $\phi$ | $n_{max}$ |
| 61 - 70 | - | c | - | TH($\theta$) | - | c | $n_{min}$ |
| 71 - 80 | - | - | - | - | - | - | $Tau_r$ |

<u>If ITYP = 3</u> then the above card is immediately followed by a card giving the properties of the reinforcing strips. Whenever any of the strip properties change a new material must be defined.

<u>REINFORCED EARTH DEFINITION</u> (7E10.5)

Columns 1 - 10 EB = Young's modulus of strip

11 - 20 AB = Width of strip

21 - 30 XIB = Thickness of strip

31 - 40 BE = Horizontal spacing of strips

41 - 50 DE = Vertical spacing of strips

51 - 60 TE = Angle (in degrees) the strip makes with x-axis

61 - 70 TK = Thickness of skin plate

**Overburden code, i.e., 1 - indicates overburden properties description A; NP > 1 - indicates overburden properties description B (see note 4).

If NP > 1 then the previous card is immediately followed by M = (NP-1) cards which describe the plots of properties vs. overburden, i.e., Type B description. These M cards successively contain the values of $h_n$ (columns 1-10), $E_n$ (columns 11-20), and $\nu_n$ (columns 21-30) ($n = 2 \rightarrow NP$) which define the modulus and Poisson's ratio curves vs. overburden $h = \gamma H$. If the value of Poisson's ratio is ommitted from a card, the value is taken to be equal to the last specified value. The value of NP may not exceed 10.

B1. A card with 1 punched in column 1, followed by:

NODE POINT ARRAY - (1X, I4, 2E10.5, I5, 2E10.5, I5, E10.5) 1,2

As many cards as are necessary to specify the locations of all nodes in the system. 6,8

| | | | |
|---|---|---|---|
| Columns | 2 - 5 | N - Node point number | 5 |
| | 6 - 15 | x - coordinate | |
| | 16 - 25 | y - coordinate | |
| | 26 - 30 | N'- final point in st. line sequence | quantities associated with straight line generation option 6 |
| | 31 - 40 | x' | |
| | 41 - 50 | y' | |
| | 51 - 55 | INC-Numbering Increment | |
| | 56 - 65 | D - Spacing Ratio | 7 |

B2. A card with 2 punched in column 1, followed by:

ELEMENT ARRAY - (1X, I4, 10I5) As many cards as necessary to define all elements in the system. 1,2

Columns 2 - 5
6 - 10
11 - 15
16 - 20

The numbers of the four node points which describe the element (reading counter clockwise around the element). For a triangular element the fourth number is left blank. For a bending element the third and fourth numbers are left blank.

21 - 25 MN - Material number (corresponding to the material description in Section A3) 9

26 - 30 IN - Construction increment number (i.e., the number of the construction increment when the element becomes part of the structure) 9

31 - 35 NMIS - Number of additional elements in the sequence

36 - 40 INC - Numbering Increment

41 - 45 NMISP - Number of additional layers
46 - 50 INCP - Numbering Increment for the layers

quantities associated with the data generation option 10

55 IPRNT = 0 Element does not have skin plate
1 Element includes skin plate 15

56 - 60 IOUT = Excavation increment number 19

The order of the element cards need bear no relationship to the locations of the elements in the body.

B3. A card with 3 punched in column 1, followed by:

<u>BOUNDARY ARRAY</u> - (1X, I4, I5, E10.5, I5, 2E10.5, 3I5, 2E10.3) 2,18

As many cards as necessary to specify displacement or non-zero stress boundary conditions. Pressure specification cards must precede all other cards in the Boundary Array.

Columns

2 - 5 N - Node point number

10 $IF_1 = \begin{Bmatrix} 0 \\ 1 \end{Bmatrix}$ indicates $\begin{Bmatrix} \text{force} \\ \text{displacement} \end{Bmatrix}$ specified in 1 direction 11 12

11 - 20 $V_1$ = value of $\begin{Bmatrix} \text{force} \\ \text{displacement} \end{Bmatrix}$ specified in 1 direction

25 $IF_2 = \begin{Bmatrix} 0 \\ 1 \end{Bmatrix}$ indicates $\begin{Bmatrix} \text{force} \\ \text{displacement} \end{Bmatrix}$ specified in 2 direction

26 - 35 $V_2$ = value of $\begin{Bmatrix} \text{force} \\ \text{displacement} \end{Bmatrix}$ specified in 2 direction

36 - 45 $\theta$ - angle (in degrees) between $x_1$-axis and x-axis (see Figure 1) 12

46 - 50 IN - Construction increment in which the non-zero boundary conditions are to be applied 11

51 - 55 N' - final point in sequence
56 - 60 INC - Numbering Increment
} quantities associated with boundary condition generation option 13

61 - 70 $P_N$
71 - 80 $P_{N'}$
} Pressure magnitudes at points N and N' respectively 14

B4. <u>END CARD</u> - Card with 4 punched in column 1

The above sequence of cards is repeated for the next analysis, etc.

III. OUTPUT:

The items appearing in the output are listed below:

A. The input data is printed

B. For each construction increment the following items are printed (Note: All of the following items are total values, i.e., values accumulated during all the previous and present construction increments; incremental values can of course be found by subtracting values printed for successive increments.)

1. For each element, the following items are printed: (Note: The units are determined by the units employed in the input.)

Element No. = The element numbers are defined by the order of printing of the element input information.

a) For continuum Elements:

X, Y = Coordinates of the point in the element for which stresses and strains are printed

EPSILON-X = Soil strain in x direction

EPSILON-Y = Soil strain in y direction

GAMA-XY = Shear strain in soil

SIGMA-X = Soil stress in x direction

SIGMA-Y = Soil stress in y direction

TAU-XY = Shear stress in soil

SIGMA-1 = Max. Principal stress in soil

SIGMA-2 = Min. Principal stress in soil

ANG = Angle (in degress) between direction of maximum principal stress and x axis

In addition if the element is reinforced earth the following items are printed:

STRIP AXIAL FORCE = Force in reinforcing strip

MOMENT = Moment in reinforcing strip

In addition if the reinforced earth element has a skin plate and is on the edge of the structure

SKIN MEMBRANE STRESS = Membrane stress in skin plate

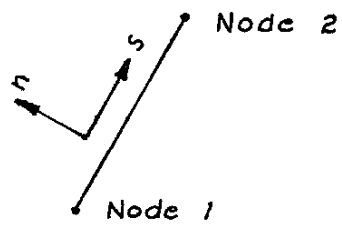
b) For beam elements (for plane strain these quantities are per unit of width)

P = Axial force at the center of element

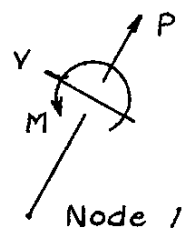
V = Shear force at the center of element

M = Moment at the center of element

The sign convention used for the bending element is:




Line Element




Sign Convention

The stress calculation for the beam element requires values for $n_{max}$ (distance from N.A. to extreme fiber, for positive n), $n_{min}$ (distance from N.A. to extreme fiber, for negative n) and $Tau_r$ (ratio of maximum shear stress to average value). If $n_{max}$ is left blank it is assumed that the section is rectangular and the program sets $n_{max} = h/2$, $n_{min} = -h/2$ and $Tau_r = 1.5$, where $\frac{h}{2} = \sqrt{\frac{3I}{A}}$. The normal stresses and strains are denoted by the symbols S and E respectively; the shear stress by the symbol TAU.

2. For each node in the system the x-y displacement components are printed.

# COMMENTARY A

## Explanatory Comments Concerning the Input

1. The cross-section of the body is assumed to lie in the x-y plane with the gravity loading acting in the negative y-direction, see Figure C-1. In the application of the analysis the cross-section of the body is described by a series of quadrilateral and/or triangular continuum elements and line (bending) elements. The quadrilateral elements may have arbitrary shapes. Because the triangular elements are of lower order than the quadrilateral elements they should be used sparingly. The numbering of the nodes for a simple element representation is shown in Figure C-2.

Considering any two of the two or three or four nodes which describe an element (line or triangle or quadrilateral) denote the bandwidth span between them as $N_i$. The value of $N_i$ is equal to 2 plus twice the difference in their node numbers plus the number of nodes in this "range" which have bending elements associated with them minus twice the number of nodes in this "range" which are not part of the structure (see note 5). If the two nodes under consideration are 17 and 45, the "range" of nodes referred to is 17 → 45. For a given element denote the maximum value of $N_i$ as $NE_j$. Considering all elements in the system denote the maximum value of $NE_j$ as $NE_{max}$ ("bandwidth" of simultaneous equations). For a minimization of computational cost, for a given analysis, it is important that the node points be numbered so as to minimize the value of $NE_{max}$ (the numbering used in Figure C-2 gives a value of $NE_{max} = 12$; if the numbering had instead proceeded from left to right a value of $NE_{max} = 22$ would have been obtained).

The program checks the area of each element, if any one of these values should be non-positive, an error message ("data error in element n") is printed. This error is normally a result of one of the following causes: i) the nodes describing the element were entered in a clockwise manner instead of counter clockwise; ii) one of the node numbers describing the element was entered incorrectly or; iii) the coordinates of one of the nodes describing the element was entered incorrectly.

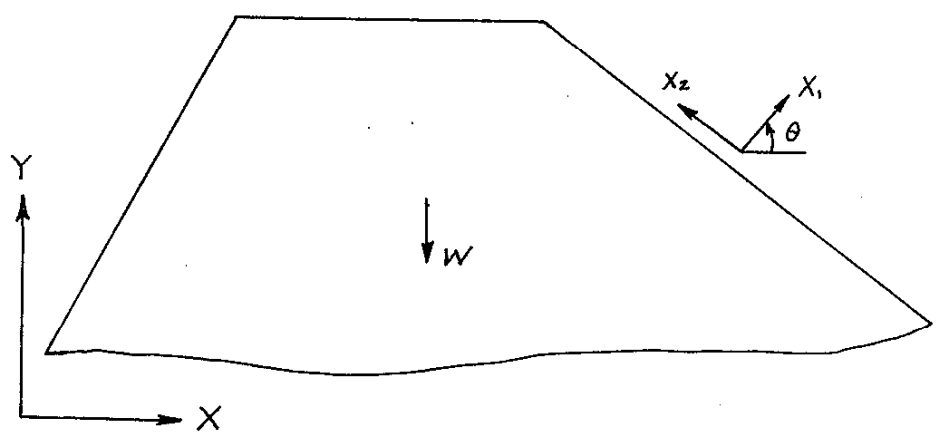



Figure C-1 - Sketch of typical body

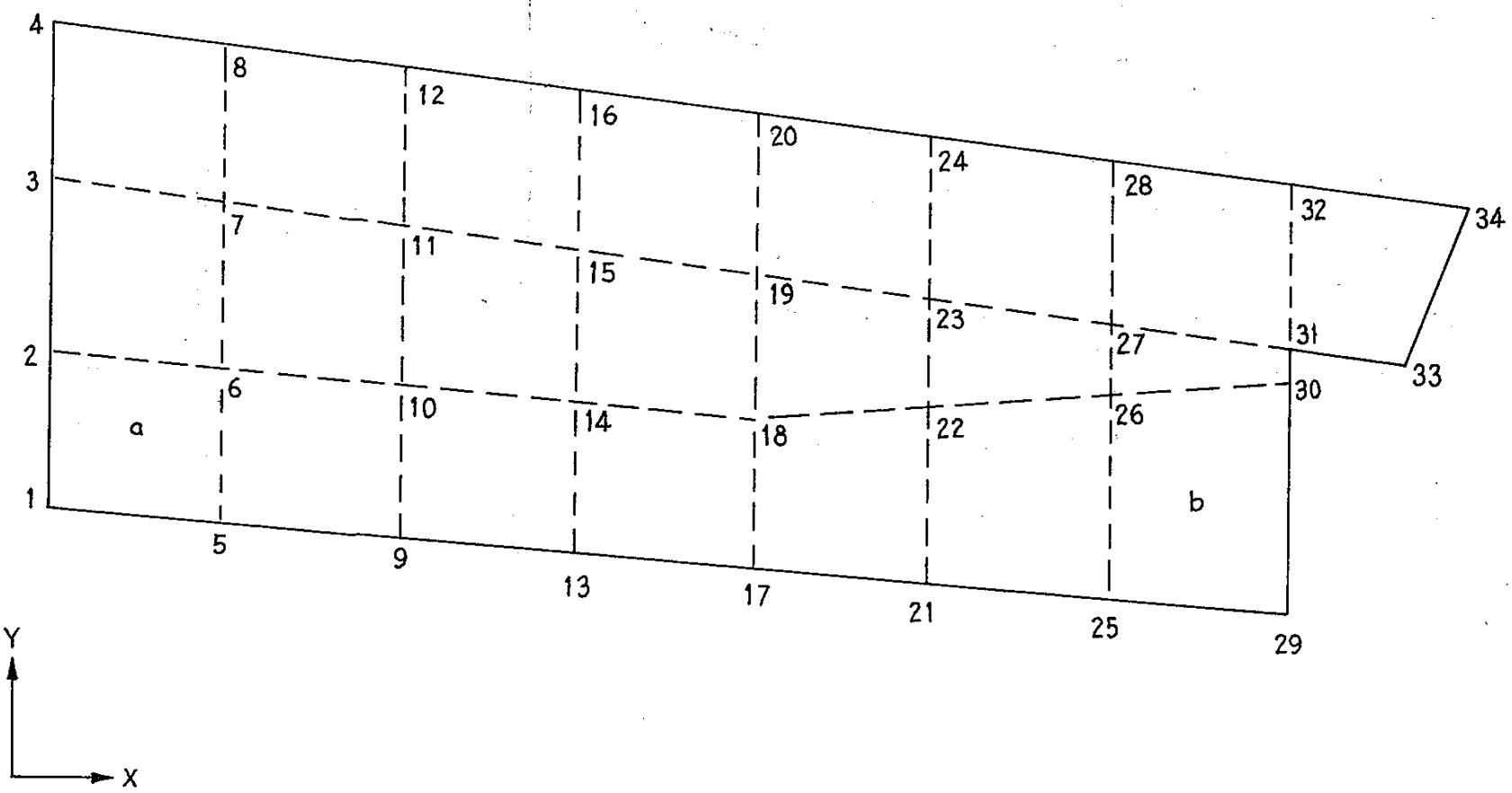



Figure C-2 - Representation by quadrilateral elements.

2. As the program is now dimensioned the value of $NE_{max}$ (see comment 1) may not exceed 56, the maximum node number (NPT) may not exceed 700, the number of elements (NELEM) may not exceed 599, the number of boundary condition specifications (NBPTC) may not exceed 199, the number of different materials (NMAT) may not exceed 10, and the number of points used to specify overburden properties may not exceed 10. These limitations may be modified by changing the dimensions of the program. If any one of these restrictions is violated, an error message is printed and the program proceeds to the consideration of the next problem.

When changing the dimensions of the program three areas must be considered:

i) Common blocks (see Table C-1)

ii) The value of NEQ = N4 specified at the beginning of the program

iii) The dimension checks at the end of the subroutine PREP

The dimensions in the program which are related to the size of the problem are indicated below:

$X(N_1)$, $Y(N_1)$, $NQ(N_1+1)$, $U(N_1)$, $V(N_1)$

$NOD(N_2,4)$, $MNO(N_2)$, $ST(N_2,17)$, $INCOUT(N_2)$

$NODB(N_3)$, $BIV(N_3, 3)$

$SL(2*N_4)$, $S(2*N_4, N_4)$

$DEN(N_5)$, $NON(N_5)$, $GNU(N_5,N_6)$, $E(N_5,N_6)$, $H(N_5,N_6)$

$AB(N_5)$, $EB(N_5)$, $XIB(N_5)$, $BE(N_5)$, $DE(N_5)$, $TE(N_5)$, $TK(N_5)$

where

$N_1$ = maximum node number

$N_2 - 1$ = maximum number of elements

$N_3 - 1$ = maximum number of boundary conditions

| SUBROUTINE \ COMMON BLOCK | 1 | 2 | 3 | 4 | 5 | 6 |
|---|---|---|---|---|---|---|
| MAIN | X | X | X | X | X | X |
| STRESS | X | X | X | X | X | X |
| PREP | X | X | | | X | X |
| CONVT | | | | | X | |
| ANISP | | | | | X | |
| INTPI | X | | | | X | |
| STIFNS | X | X | X | X | X | |
| GEOM | | | X | | | |
| STFSUB | X | | X | | X | |
| REDUCI | | | | X | | |
| BAKSUB | | | | X | | |
| PRINC | | | | | | |
| ESTAB | | | X | | | |
| REINF | | | | | | X |
| STREH | | | X | | | X |

Table C-1 - Common Blocks - Subroutine Association

$N_4 \geq 2*(NE_{max}+1)$

$N_5$ = maximum number of different materials

$N_6$ = maximum number of points describing a Type B material

3. The program may be utilized for a non-incremental construction analysis by specifying the number of construction increments to be one.

4. The length units used to describe the material properties must be consistent with the units used to describe the geometry of the body.

The overburden dependence of a soil's modulus may be accounted for by one of two different means. "Type A" description is specified by punching a 1 in Col. 10 of the appropriate "material card." The overburden dependence of the modulus is modeled by using the relationship reported in Equ. (27) of the Highway Research Report by Travis Smith, et. al.*, i.e.,

$$E_t = [A + B(1-\sin\phi)\gamma H] \quad [1 - \frac{\gamma H\ (1-\sin\phi)\ \sin\phi}{2c\ \cos\phi + 2\ \sin\phi\ (\frac{\gamma H}{N_\phi} - \frac{2c}{(N_\phi)^{\frac{1}{2}}})}]^2$$

where

$N_\phi = \tan^2\ (45° + \frac{\phi}{2})$

$E_i = A + B\sigma_3$

$\gamma$ = Density

c = Cohesion

$\phi$ = Friction angle (degrees)

H = Overburden depth

---

*"Stresses and Deformations in Jail Gulch Embankment," Interim report prepared by the Materials and Research Department, California Division of Highways, February 1972.

For a given construction increment, the program takes the overburden depth to be the vertical distance between the center of the element and the surface of the soil directly above this point. The value of $\gamma$ that is used in the above and following equations is determined as follows: The average of all specified values of $\gamma$, for the several materials in the problem, which are non-zero are used; if no non-zero values are specified, a value of 130 pcf is assumed.

The "Type B" description interpolates plots of E and $\nu$ vs. overburden pressure ($h = H\gamma$), see Figure C-2a. This description is specified by assigning propriate values for $h_1$, $E_1$, $\nu_1$; $h_2$, $E_2$, $\nu_2$; etc.

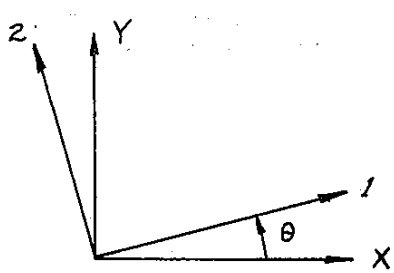
If the program is to be used for a plane stress analysis the "equivalent" plane stress properties are used, i.e., for isotropic materials the values of $\bar{E}$ and $\bar{\nu}$ are used for E and $\nu$.

$$\bar{E} = E \frac{(1 + 2\nu)}{(1 + \nu)^2}$$

$$\bar{\nu} = \frac{\nu}{1 + \nu}$$

Linear orthotropic material are described by the following stress-strain law:

$$\begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \tau_{12} \end{bmatrix} = \begin{bmatrix} C_{11} & C_{12} & \\ C_{12} & C_{22} & \\ & & C_{33} \end{bmatrix} \begin{bmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \gamma_{12} \end{bmatrix}$$



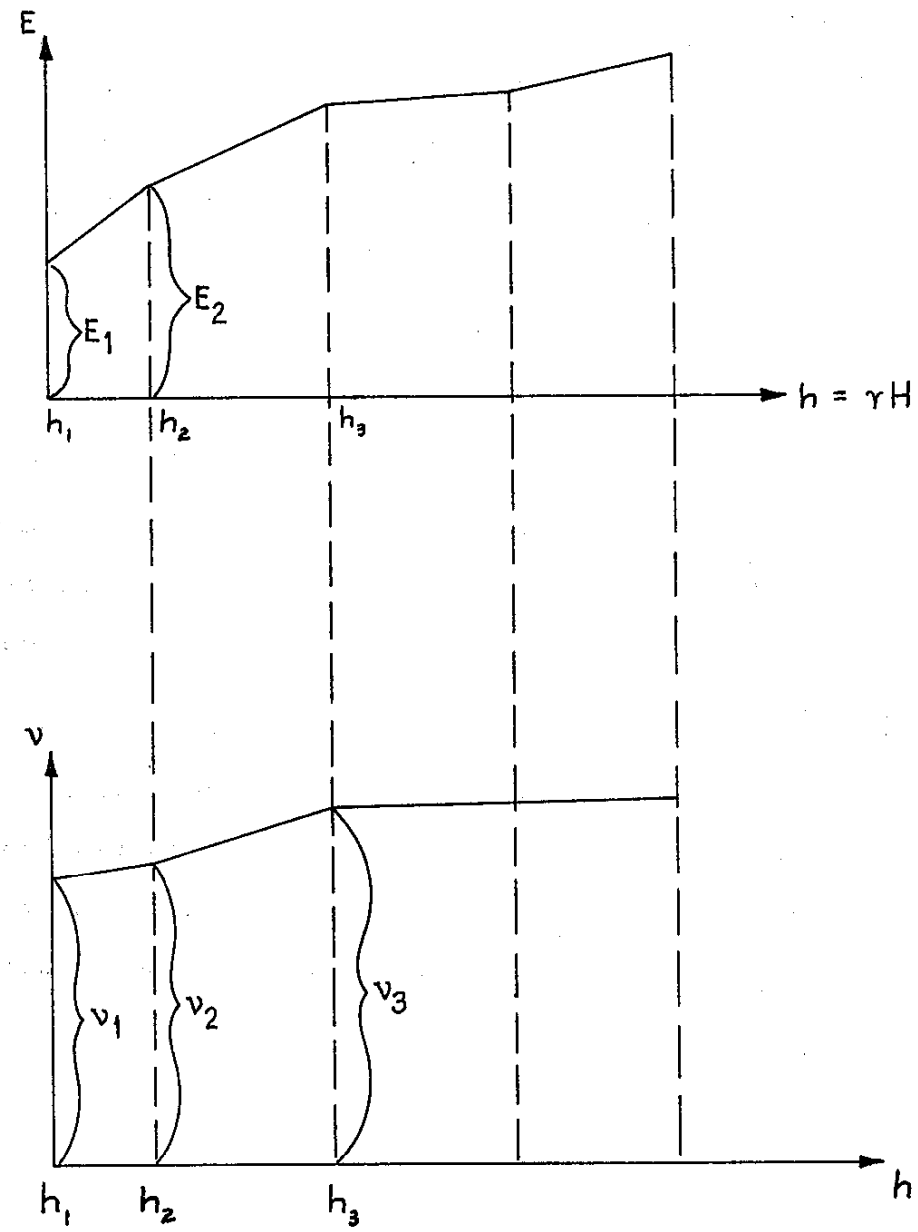



Figure C-2a - Typical plots of E and ν - Overburden

Reinforced earth materials are described by: a) specifying the appropriate properties for the soil and b) specifying the size, spacing and elastic properties of the reinforcing strips. The quantities which define the reinforcing strips are illustrated in Figure C-3.

5. Not all numbers between 1 and the maximum node number need correspond to actual nodes in the body, e.g, the grid shown in Figure C-4 is permissible; coordinates may or may not be specified for the nonexistent nodes 15 and 21. This feature facilitates the use of the various data generation options (e.g., see "Comment 7").

6. The program has available two generation procedures to assist the User in describing the location of the node points. These generation options are described in the following two "comments." The use of these options can, for instance, permit one to describe the location of the nodes for an arbitrarily large grid by as few as four cards.

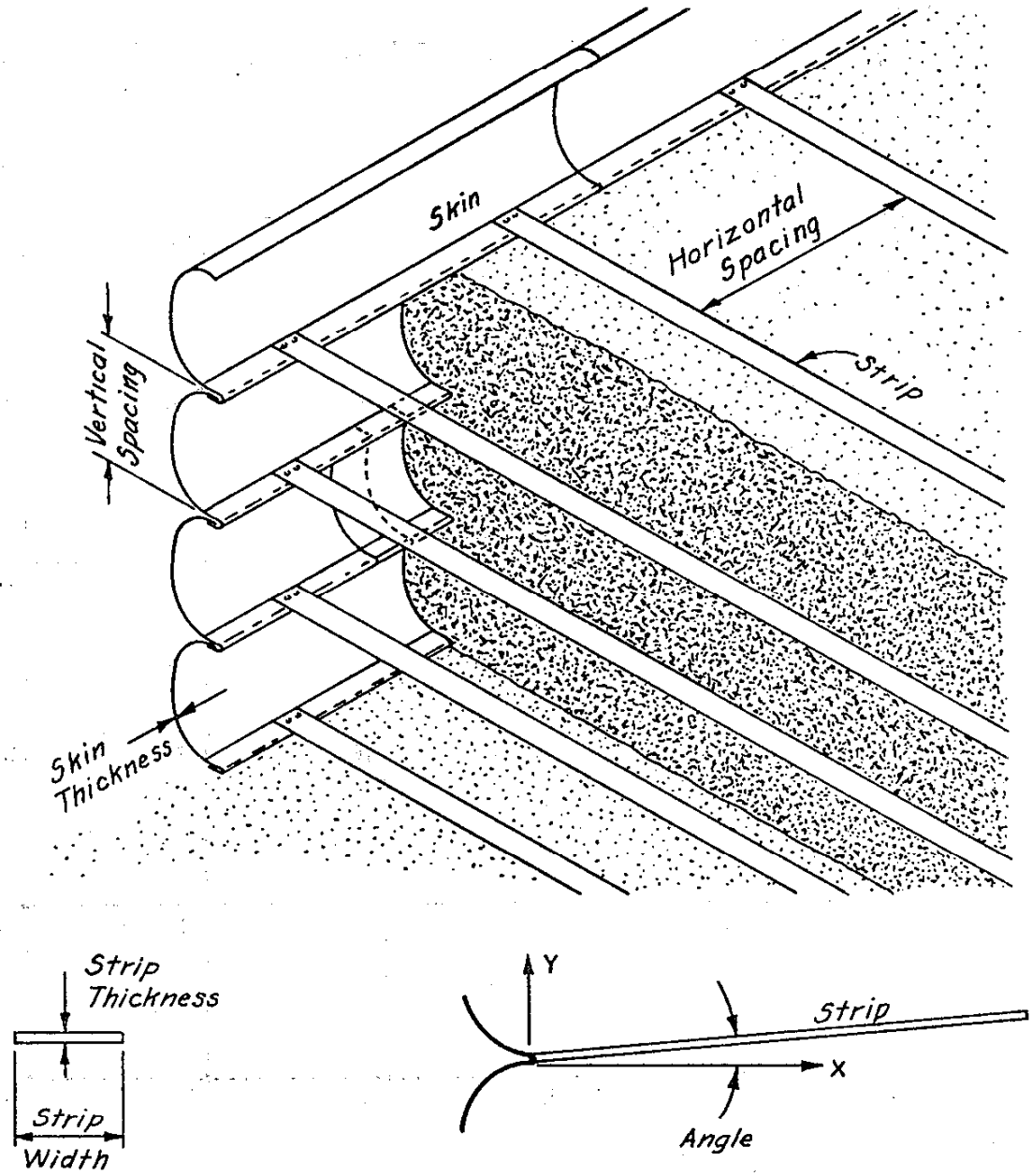



Figure C-3 - Reinforced Earth Input Properties

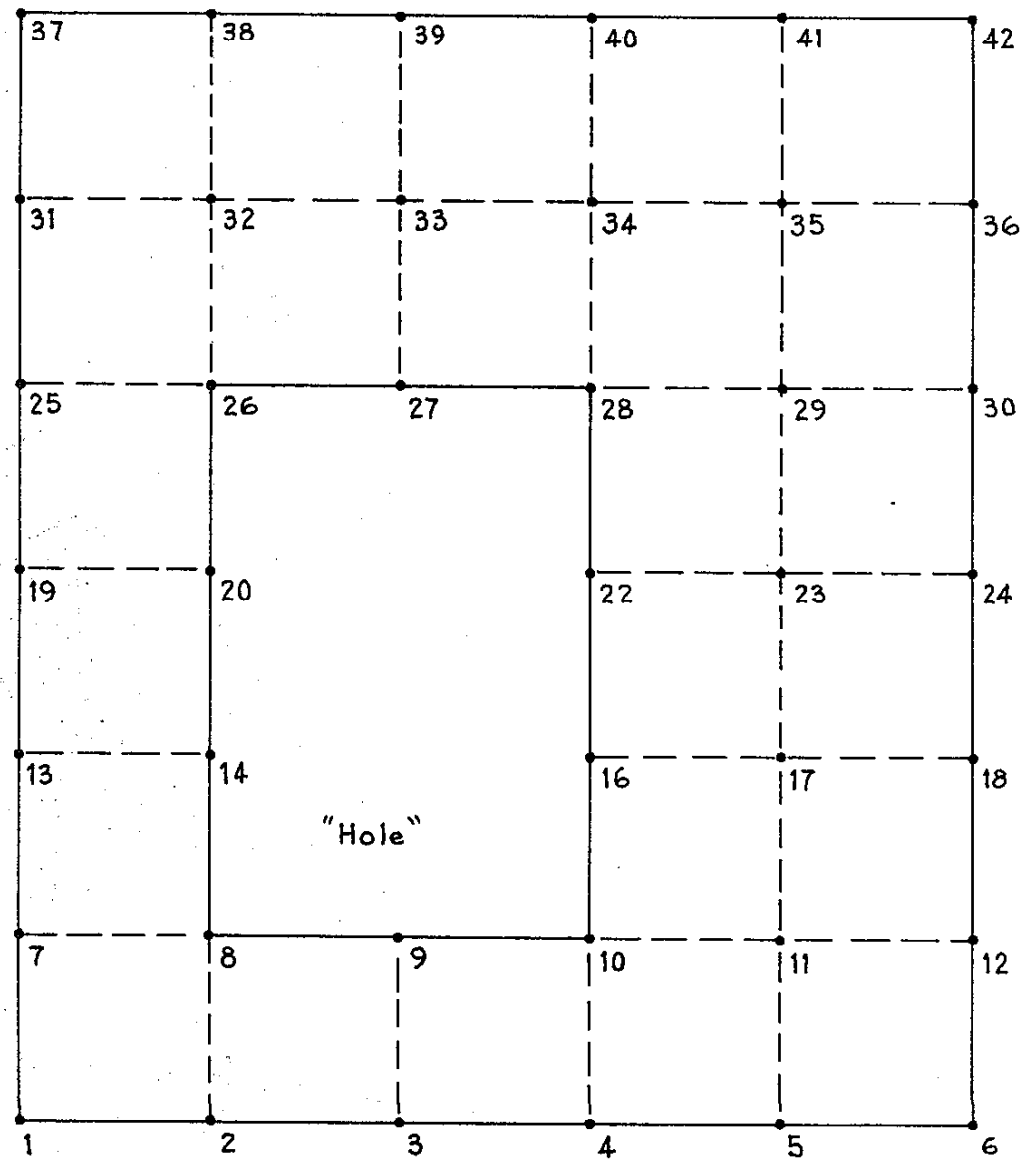



Figure C-4 - Example of grid with missing node numbers.

7. The "straight line coordinate generation option" may be used whenever several sequential points lie along a straight line. For such points it is only necessary to enter data for the end points (denoted as N and N') of the sequence and values for INC and D. INC is the difference between two successive node numbers in the sequence and D is the ratio of the distances between successive pairs of points. The end points of the segment may be entered in any order, i.e. the line segment shown in Figure C-5 may be defined by specifying the end-points in order 7 → 22 or 22 → 7. The spacing of the intermediate points is controlled by the value of the spacing ratio D. D is equal to the ratio of the lengths of the successive segments defined by the intermediate points. A value of D = 1.0 gives equally spaced points. The locations of the intermediate points 12 and 17 (see Figure C-5) could be generated by either specifying points 7 → 22 and D = 2.0 (Note: D = 2.0/1.0 = 4.0/2.0), or 22 → 7 and D = 0.5 (Note: D = 2.0/4.0 = 1.0/2.0); the value of INC would be 5.

For the grid shown in Figure C-2 the coordinates could be generated for the points lying between 1-4, 5-8, 9-12, etc., or between 1-29, 2-18, 18-30, 3-31 etc. Note that the line 3-31 cannot be extended to point 33 as the value of INC changes at point 31, however, if nodes 33 and 34 had been instead numbered 35 and 36 (there would then have been no nodes numbered 33 and 34, see "comment 5") it would be possible to generate all the nodes along the line with a single card.

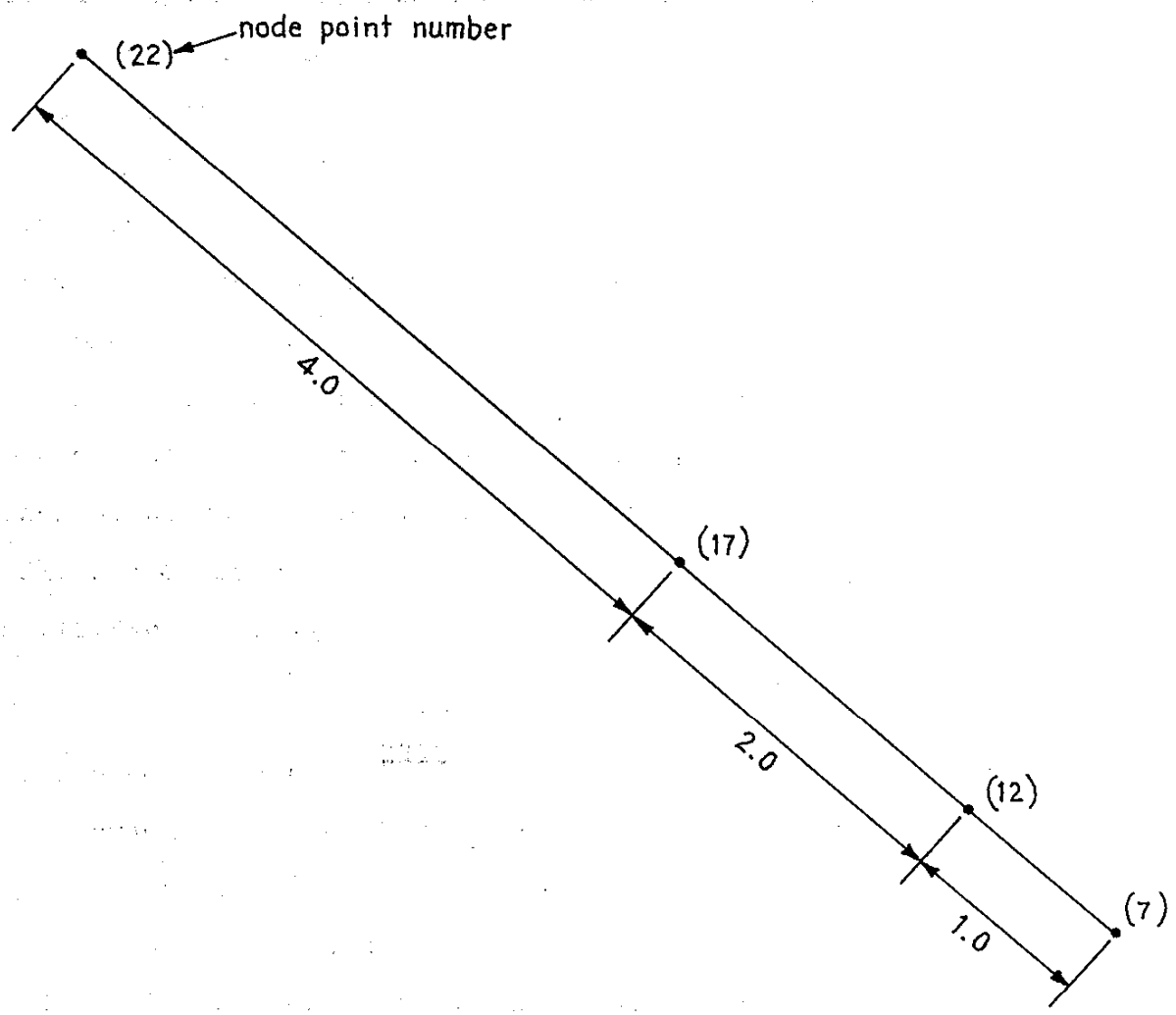
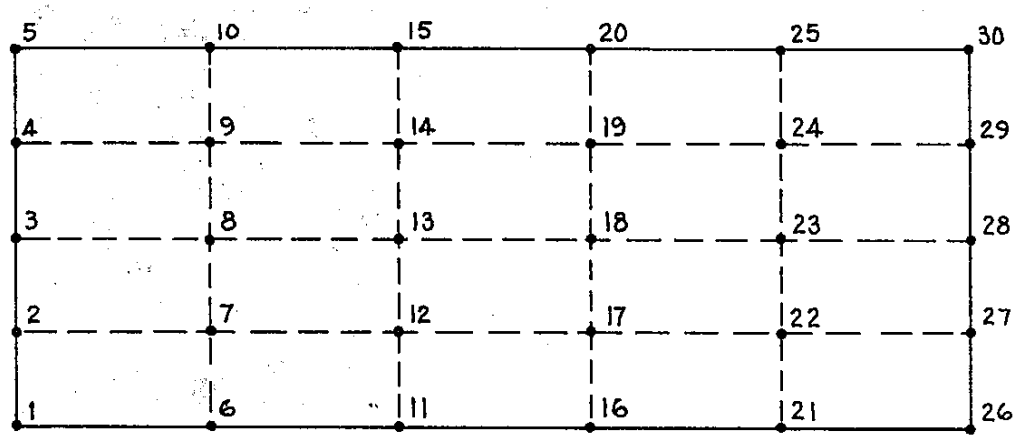



Figure C-5 - Node points lying on straight line.

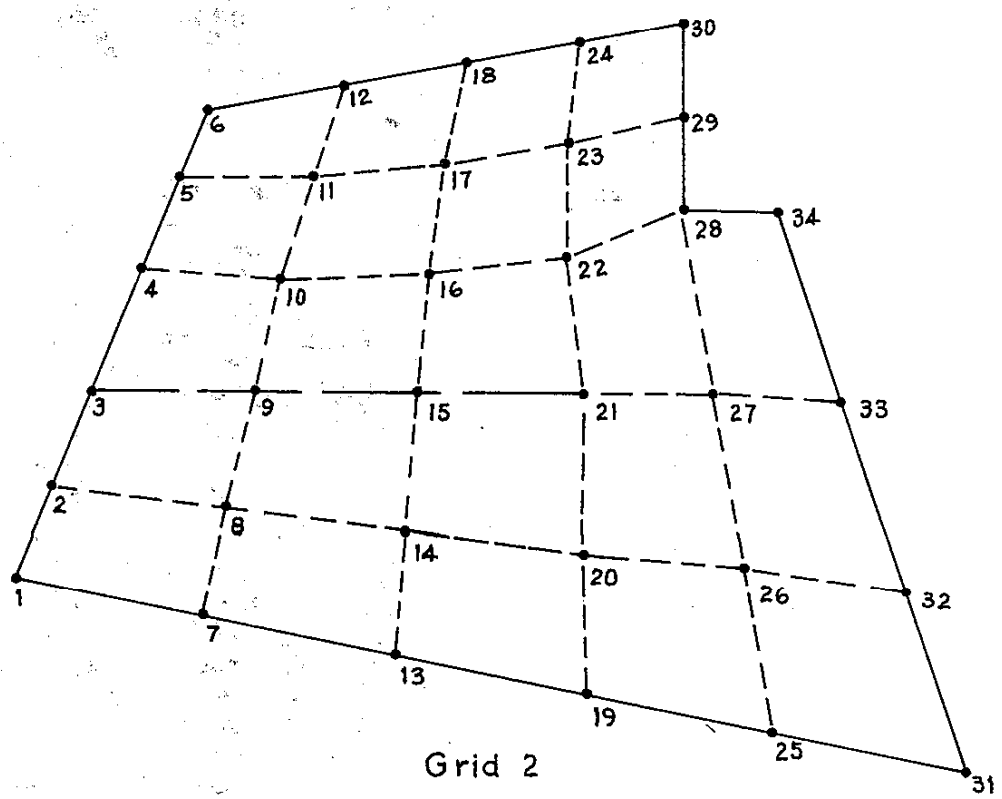
8. The "interior node point generation option" locates all nodes interior to the body whose coordinates have not been specifically specified by the user (i.e. all points not specifically treated in Section B1). The location of the interior nodes is accomplished by the so called "Laplacian generation scheme", i.e., the coordinates of an interior node point are selected so that they are equal to the average of the coordinates of the neighboring nodes. Note that all nodes on the boundaries of the body must be either directly specified or generated by means of the straight line generation scheme (described in "comment 7"). Figure C-6 illustrates two grids which have been prepared with the aid of this generation scheme. Grid 1 was prepared by specifying the locations of the exterior nodes by means of the straight line generation scheme; the interior nodes were left unspecified and hence were "generated" as described above. Grid 2 was prepared in a similiar way with the exception that the interior sequence of nodes lying on the line 3-21 were generated with the "straight line generation scheme".

9. When the values of MN, and/or IN remain constant for a number of sequential element cards, it is only necessary to specify MN and/or IN for the first card in the group (the appropriate columns are left blank for the remainder of the cards in the group).

10. If the body is divided into layers of elements, and the quantities MN and IN remain the same for a number of elements within a layer (and possibly the same for a number of layers), the node numbers for these elements may be simply specified by




Grid 1




Grid 2

Figure C-6 - Grids prepared with the aid of the generation options.

using the "element data generation option". To use the generation option for the elements in a single layer the data is supplied for the first element in the layer and the appropriate values are specified for NMIS and INC. The quantity NMIS indicates the number of additional elements in the sequence. The quantity INC indicates the amount by which the node numbers of successive elements differ.

For example the bottom row of elements in Figure C-2 could be specified by giving the node numbers for element "a" and the values NMIS = 6 and INC = 4 or the information for element "b" and the values NMIS = 6 and INC = -4 (in order to use this option all the elements from a → b must, however, have the same values of MN and IN). Alternatively if one wished to generate the element information for the elements in the left hand column (all these elements would need to have the same values of MN and IN), one could do this by giving the node numbers for element "a" and the values NMIS = 2 and INC = 1, etc.

In addition, if the values of MN and IN remain unchanged for a number of layers the data information for all the elements in these layers may be generated with a single card by supplying, in addition to the values of NMIS and INC (for the first layer), the values of NMISP and INCP. NMISP denotes the number of additional layers for which the element data is to be generated and INCP indicates the difference between the node numbers of the successive layers. For example, if the bottom two layers of elements in Figure C-2 all had identical values of MN and IN the data for <u>all</u> these elements could be generated by giving the appropriate data for element "a" and the values

```
NMIS = 6
INC = 4
NMISP = 1
INCP = 1
```

or alternatively

```
NMIS = 1
INC = 1
NMISP = 6
INCP = 4
```

As a second example if the elements of Grid 1 of Figure C-6 all had identical values of MN and IN they all could be described by giving the appropriate data for the lower left element and

```
NMIS = 3
INC = 1
NMISP = 4
INCP = 5
```

11. For each of the two directions (see "comment 12") one either specifies the displacement by setting "IF" equal to one and "V" equal to the specified displacement or adds in the "boundary load" by leaving "IF" blank and setting "V" equal to the boundary load (i.e. resultant of specified boundary stress). Boundary displacements and forces are positive when they have the same sense as the positive coordinate direction. If a boundary point is not constrained and has no load applied to it, it is not necessary and is in fact economically not desirable to include the point in the boundary array.

A point load may be applied at any node point within the structure by treating it as a boundary point.

Specified loads are applied to the structure during construction increment IN. A specified displacement is applied during construction increment IN, during all other increments, the incremental displacement for that point is taken to be zero. If at a given point, loads are applied during more than one of the construction increments, this may be achieved by specifying the point more than once in the boundary array.

12. If $\theta = 0$ the subscripts 1 and 2 refer to x and y, if $\theta \neq 0$ (see Figure C-1) they refer to $X_1$ and $X_2$, (i.e. $IF_1 = IF_{X_1}$, etc.).

13. If several sequential points have identical boundary conditions, they may all be considerated with a single card by supplying the proper values for the quantities N' and INC. The quantity N' denotes the number of the last point in the sequence. The quantity INC specifies the difference between the node numbers of successive points.

If for example the points $1 \rightarrow 21$ on the bottom boundary of the structure shown in Figure C-2 all had the same boundary condition specifications, this could be accomplished by specifying the appropriate boundary conditions and N = 1, N' = 21, INC = 4.

14. Uniform or linearly varying pressure may be applied to a straight or curved boundary by using the boundary condition generation option (see "comment 13" - leaving the spaces for $IF_1$, $IF_2$, $V_1$, $V_2$ and TH blank) for the points involved and specifying appropriate values for $P_N$ and $P_{N'}$ (if the pressure is uniform $P_N = P_{N'}$). For example, for the boundary shown in Figure C-7 one would specify:

$N = 11$
$N' = 2$
$INC = -3$
$P_N = 100$
$P_{N'} = 50$

The points $N \rightarrow N'$ must be specified in a counterclockwise order as one proceeds along an external boundary and clockwise along internal boundaries (i.e., inside holes in the body). Pressure specification cards <u>must</u> precede all others in the "Boundary Condition Array".

15. Those reinforced earth elements which are on the edge of the earth structure where a "skin plate" is present are flaged by setting IPRNT = 1.

16. A bending (and stretching) element (strip plate element for plane strain, beam element for plane stress) may be placed between any two nodes in the system. If two or more bending elements intersect at a node the connection between them is treated as rigid. Curved members may be approximated by a series of straight elements. In the element array bending elements are designated by leaving their 3rd and 4th node numbers blank.

17. The section properties of a bending element are described by specifying values of area (A) and moment of inertia (I). For plane stress analyses A and I are the appropriate values for a unit width of the bending element. The Young's modulus of the material is denoted by E. For plane strain the values of Poisson's ratio is supplied for $\nu$ while the plane stress $\bar{\nu}$ is assigned a value of zero. The quantities $n_{max}$, $n_{min}$ and $Tau_r$ are described in Section III-B-1-b (i.e., description of output for beam element).

18. Slope boundary conditions for bending elements are specified automatically by the program as follows: If no displacement boundary conditions are specified for a node at the end of a bending member the moment at the end of the bending member is taken to be zero; if one or both of the displacements are specified the slope of the bending element is set equal to zero.

19. The "Element Excavation Increment Number" specifies the increment during which the material in the element is to be excavated. If the material is <u>not</u> to be excavated the number is <u>left blank</u> (the program then sets it equal to 99).

For a given analysis if there is to be excavation <u>all</u> "Type B" materials (see note 4 and Figure C-2a) <u>require</u> additional input. For excavation problems "Type B" materials require that two plots of "E and $\nu \sim$ overburden" be specified.

The first (loading behavior) is used in all increments prior to the first excavation increment for the problem. The second description (unloading behavior) is used for <u>all</u> subsequent increments. Both descriptions <u>must</u> have the same number of points in the specifications of the "E & $\nu \sim h$" curves. For example, for an excavation problem if material number 3 is of type B with 6 points defining the E & $\nu$ curves, then material 4 must be a dummy material that is used to record the unloading behavior for material 3 (6 points must also be used to describe the unloading curves). All elements made of this material are given material number 3.

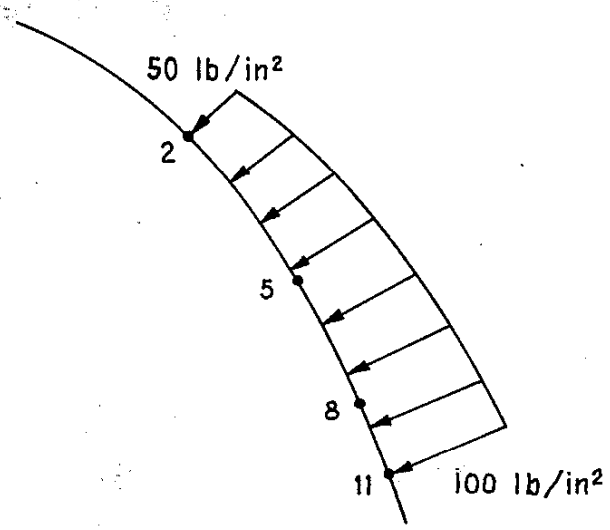



Figure C-7 - Pressurized boundary.

COMMENTARY B

## Discussion of Program

In this appendix very brief descriptions of the uses and special features of the program are given. The theory of the finite element procedure is, however, not discussed; instead the reader is referred to standard works on the subject such as the book by Zienkiewicz*.

This finite element program may be applied to a wide range of problems in structural engineering and mechanics. The program may be directly, or with only minor modification, applied to any elasticity problem that may be characterized as plane stress or plane strain. The program is specifically set up for plane strain problems; the use of the program for plane stress problems is described in comment 4 of Commentary A. In addition the program has certain unique features which make it particularly suitable for the analysis of ordinary and reinforced earth structures (e.g., embankments) situated on soil or rock foundations. These special features include provisions for the consideration of:

1. The incremental construction sequence
2. Overburden dependent material properties
3. Orthotropic material behavior
4. Reinforced earth construction
5. Bending members

The basic theory underlying an incremental construction analysis may be found in the paper by Clough and Woodward**. Basically such

*The Finite Element Method in Engineering Science, McGraw-Hill, London, 1971.

**"Analysis of Embankment Stresses and Deformations," J. of the Soil Mech. and Foundations Div. of the ASCE, Vol. 93. No. SM4, July 1967, pp. 529-549.

analyses permit account to be taken of the fact that an earth embankment is not formed in one operation but is instead placed as a sequence of layers. Thus the program may be used to predict the stresses and deformations developed in all existing layers as each new layer is placed.

For soils whose properties are functions of the overburden their properties may be modeled by utilizing (see comment 4 in Commentary A) the special provision in the program for the description of this dependence.

The inclusion of the option of prescribing an orthotropic stress-strain law permits the characterization of layers which exhibit directionally dependent material properties.

The program is specially designed for the analysis of reinforced earth structures. The user supplies to the program a description of the spacing, size and elastic properties of the reinforcing strips and the properties of the soil. Utilizing these properties the program calculates "composite properties" for the reinforced earth (these calculations are based upon the model developed by Romstad and Herrmann*). Utilizing these "composite properties" for the reinforced earth a finite element analysis of the structure subjected to the loads prescribed by the user is performed. From the finite element analysis the composite stresses and strains developed in the reinforced earth are obtained. The program then uses the composite stresses and strains in calculations which yield the corresponding stresses and strains in the soil and the axial forces and moments developed in the reinforcing strips (these calculations follow from the above mentioned model*).

*"Material Properties of Reinforced Earth," Consulting Report to California Division of Highways, July 1972.

The bending (and stretching) element may be used, for example, to model cross-sections of culverts or bridges which pass through the embankment.

The finite element analysis utilizes a recently developed element that is considerably more accurate than previously available simple elements. The derivation and characteristics of this element are described in detail in a paper by Herrmann*.

The "Input" procedures used in the program represent an attempt to minimize the effort required by the user for data preparation and represents a combination of numerous suggestions made to the authors by users of related finite element programs over the past years.

*"Efficiency Evaluation of a Two-Dimensional Incompatible Finite Element," J. of Computers and Structures, June 1972.

# COMMENTARY C

## Sample Problem

In this commentary the input and output for a sample problem are given. The problem is intended to serve as an example of the input and output formats, and a check-problem that may be used to determine if the program is functioning properly. For the sake of simplicity a very much coarser grid is used for this sample problem than would be used in an actual analysis.

The configuration of the problem is shown in Figure C-8. The first number contained within parentheses within an element indicates the material type, the second, the incremental construction number. The number in parentheses next to the external load, indicates the construction increment during which this load is applied. Material 1 is taken to have been in place prior to construction, hence, its weight is not a new factor and thus its density is set equal to zero.

The input data and the output from the program follow (Note: Units of lbs. and ft. were used in this example, e.g., moduli and stress are expressed in psf):

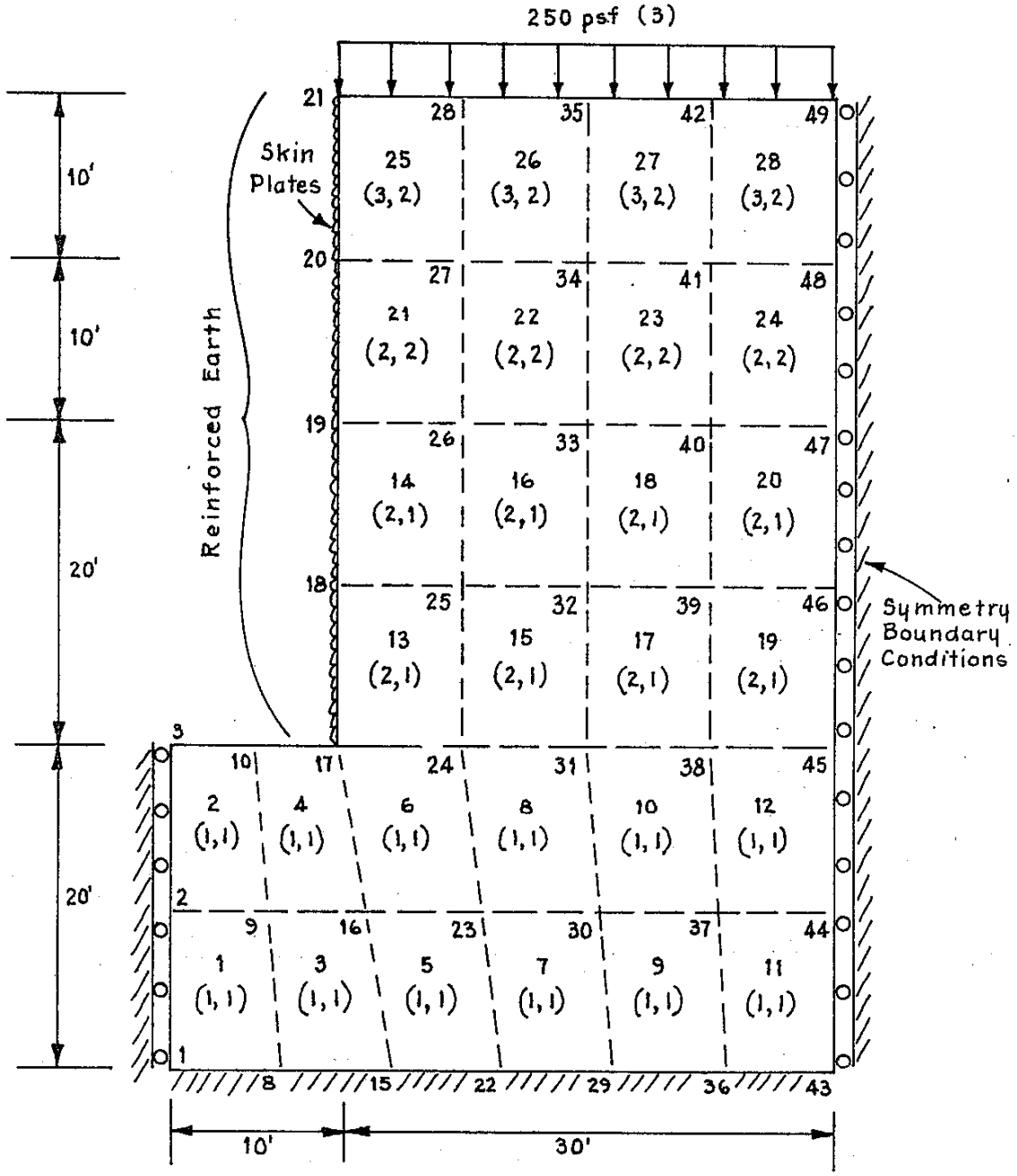



Figure C-8 - Sample problem.

INPUT FOR SAMPLE PROBLEM - COMMENTARY C - FIGURE C-8

1/2

```
REINFØRCED EARTH EXAMPLE--VERY COARSE GRID
   3    6.15          0     0E132 CLETUS 6964
   1                                15000000.    .3
   2 3  4   130.                    3000000.     .4
 4.32E+09   .131      .00985        3.28         .833                .0104
 2000.    4200000.      .4
 4000.    5200000.      .4
10000.    6700000.      .4
   3 3  4 130.                      3000000.     .4
 4.32E+09   .131      .00985        4.92         .833                .0104
 2000.    4200000.      .4
 4000.    5200000.      .4
10000.    6700000.      .4
1
   1                          43    40.                        7
   2                  10.
  44     40.          10.
   3                  20.      17    10.        20.          7
  17     10.          20.      45    40.        20.          7
```

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| | 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 | 56–60 | 61–65 | 66–70 | 71–75 | 76–80 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 2 | 17 | 10. | | 20. | | 20 | 10. | | 50. | | 1 | | | | | |
| | 45 | 40. | | 20. | | 48 | 40. | | 50. | | 1 | | | | | |
| | 20 | 10. | | 50. | | 48 | 40. | | 50. | | 7 | | | | | |
| | 21 | 10. | | 60. | | 49 | 40. | | 60. | | 7 | | | | | |
| 3 | 1 | 8 | 9 | 2 | 1 | 1 | 5 | 7 | 1 | 1 | | | | | | |
| | 17 | 24 | 25 | 18 | 2 | 1 | 1 | 1 | | | 1 | | | | | |
| | 24 | 31 | 32 | 25 | 2 | 1 | 2 | 7 | 1 | 1 | | | | | | |
| | 19 | 26 | 27 | 20 | 2 | 2 | | | | | 1 | | | | | |
| | 26 | 33 | 34 | 27 | 2 | 2 | 2 | 7 | | | | | | | | |
| 4 | 20 | 27 | 28 | 21 | 3 | 2 | | | | | 1 | | | | | |
| | 27 | 34 | 35 | 28 | 3 | 2 | 2 | 7 | | | | | | | | |
| | 49 | | | | | | | | | 3 | 21 | -7 | 250. | | 250. | |
| | 1 | 1 | | | | | | | | | 3 | | | | | |
| | 1 | 1 | | | 1 | | | | | | 43 | 7 | | | | |
| | 43 | 1 | | | | | | | | | 49 | 1 | | | | |

C35

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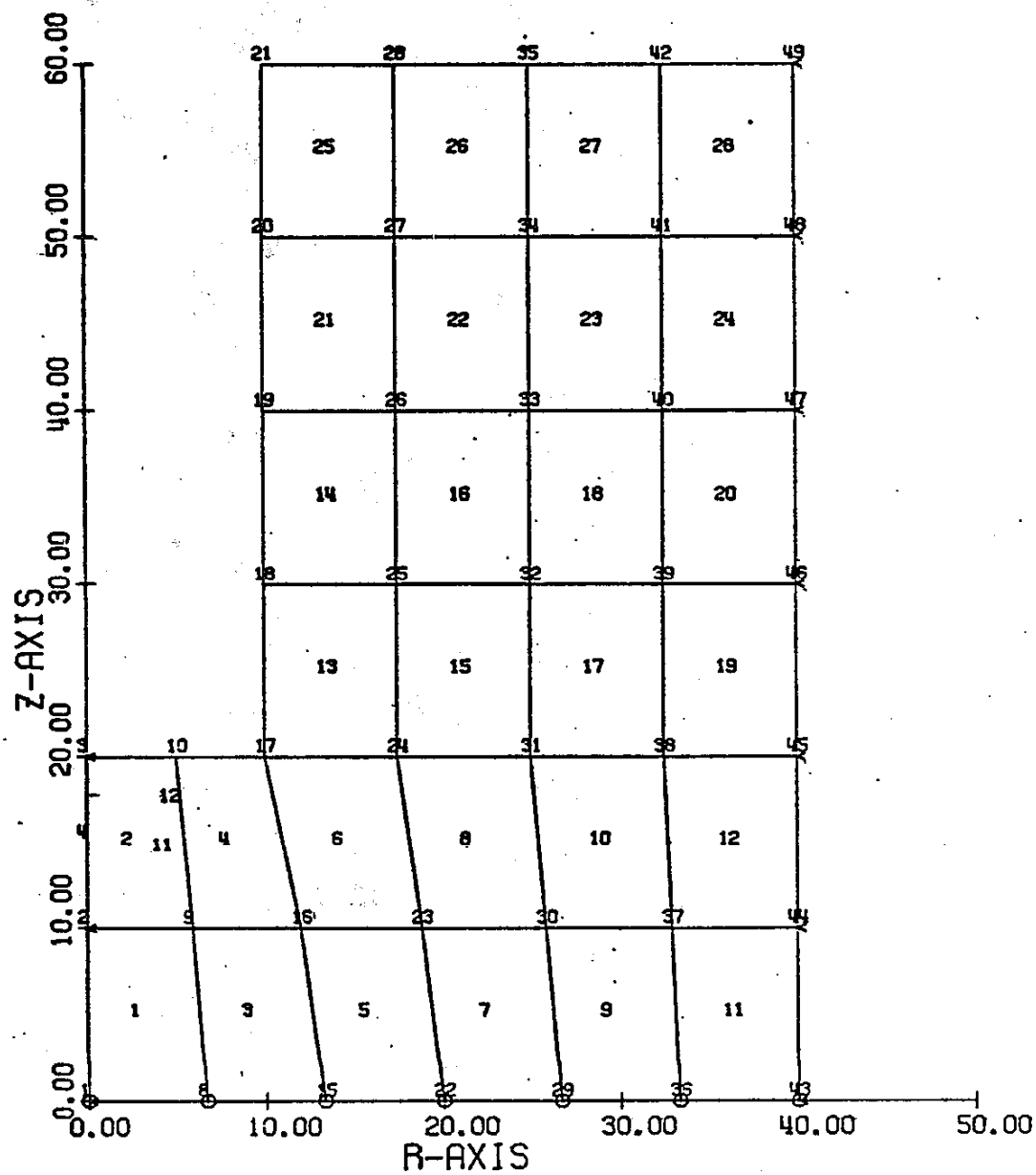


END OF PLOT TAPE011549 DATED 02/23/73

REINFORCED EARTH EXAMPLE--VERY COARSE GRID

```
INPUT DATA CARD IMAGE ****

  REINFORCED EARTH EXAMPLE--VERY COARSE GRID
    3   6.15        0    0E132 CLETUS 6964
    1                          15000000.    .3
    2 3  4  130.               3000000.     .4
  4.32E+09  .131      .00985    3.28        .833                  .0104
  2000.    4200000.      .4
  4000.    5200000.      .4
 10000.    6700000.      .4
    3 3  4 130.                3000000.     .4
  4.32E+09  .131      .00985    4.92        .833                  .0104
  2000.    4200000.      .4
  4000.    5200000.      .4
 10000.    6700000.      .4
1
    1                        43   40.                    7
    2                10.
   44  40.        10.
    3                20.      17   10.        20.        7
   17    10.        20.      45   40.        20.        7
   17    10.        20.      20   10.        50.        1
   45    40.        20.      48   40.        50.        1
   20    10.        50.      48    40.       50.        7
   21    10.        60.      49    40.       60.        7
2
    1    8    9    2    1    1    5    7    1    1
   17   24   25   18    2    1    1    1                1
   24   31   32   25    2    1    2    7    1    1
   19   26   27   20    2    2                          1
   26   33   34   27    2    2    2    7
   20   27   28   21    3    2                          1
   27   34   35   28    3    2    2    7
3
   49                                          3   21   -7  250.    250
    1    1                                            3
    1    1              1                            43    7
   43    1                                           49    1
4
```

```
REINFORCED EARTH EXAMPLE--VERY COARSE GRID

NUMBER OF CONSTRUCTION INCREMENTS =   3

PROPERTIES FOR MATERIAL  1   ********

     DENSITY =    0.0

      YOUNGS MODULUS= 0.1500E 08
      POISSONS RATIO= 0.3000E 00

PROPERTIES FOR MATERIAL  2   ********

     DENSITY =    1.30000E 02

 REINFORCED EARTH

     STRIP YOUNGS MODULUS= 0.4320E 10
     STRIP WIDTH= 0.1310E 00
     STRIP THICKNESS= 0.9850E-02
     HORIZONTAL SPACING= 0.3280E 01
     VERTICAL SPACING= 0.8330E 00
     ANGLE= 0.0
     SKIN THICKNESS IF BOUNDARY ELEMENT= 0.1040E-01
   SOIL PROPERTIES
```

ELASTIC PROPERTIES - OVERBURDEN

| OVERBURDEN | YOUNGS MODULUS | POISSONS RATIO |
|---|---|---|
| 0.0 | 3.00E 06 | 4.00E-01 |
| 2.00E 03 | 4.20E 06 | 4.00E-01 |
| 4.00E 03 | 5.20E 06 | 4.00E-01 |
| 1.00E 04 | 6.70E 06 | 4.00E-01 |

PROPERTIES FOR MATERIAL 3 ********

DENSITY = 1.30000E 02

REINFORCED EARTH

STRIP YOUNGS MODULUS= 0.4320E 10
STRIP WIDTH= 0.1310E 00
STRIP THICKNESS= 0.9850E-02
HORIZONTAL SPACING= 0.4920E 01
VERTICAL SPACING= 0.8330E 00
ANGLE= 0.0
SKIN THICKNESS IF BOUNDARY ELEMENT= 0.1040E-01

SOIL PROPERTIES

ELASTIC PROPERTIES - OVERBURDEN

| OVERBURDEN | YOUNGS MODULUS | POISSONS RATIO |
|---|---|---|
| 0.0 | 3.00E 06 | 4.00E-01 |
| 2.00E 03 | 4.20E 06 | 4.00E-01 |
| 4.00E 03 | 5.20E 06 | 4.00E-01 |
| 1.00E 04 | 6.70E 06 | 4.00E-01 |

| NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|
| 1 | 0.0 | 0.0 |
| 2 | 0.0 | 10.00 |
| 3 | 0.0 | 20.00 |
| 4 | 0.0 | 15.00 |
| 5 | 0.0 | 17.50 |
| 6 | 0.0 | 16.25 |
| 7 | 0.0 | 16.88 |
| 8 | 6.67 | 0.0 |
| 9 | 5.92 | 10.00 |
| 10 | 5.00 | 20.00 |
| 11 | 4.17 | 14.22 |
| 12 | 4.58 | 17.11 |
| 13 | 4.37 | 15.66 |
| 14 | 4.48 | 16.39 |
| 15 | 13.33 | 0.0 |
| 16 | 12.03 | 10.00 |
| 33 | 25.00 | 40.00 |
| 34 | 25.00 | 50.00 |
| 35 | 25.00 | 60.00 |
| 36 | 33.33 | 0.0 |
| 37 | 32.92 | 10.00 |
| 38 | 32.50 | 20.00 |
| 39 | 32.50 | 30.00 |
| 40 | 32.50 | 40.00 |
| 41 | 32.50 | 50.00 |
| 42 | 32.50 | 60.00 |
| 43 | 40.00 | 0.0 |
| 44 | 40.00 | 10.00 |
| 45 | 40.00 | 20.00 |
| 46 | 40.00 | 30.00 |
| 47 | 40.00 | 40.00 |
| 48 | 40.00 | 50.00 |
| 49 | 40.00 | 60.00 |

| NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|
| 17 | 10.00 | 20.00 |
| 18 | 10.00 | 30.00 |
| 19 | 10.00 | 40.00 |
| 20 | 10.00 | 50.00 |
| 21 | 10.00 | 60.00 |
| 22 | 20.00 | 0.0 |
| 23 | 18.85 | 10.00 |
| 24 | 17.50 | 20.00 |
| 25 | 17.50 | 30.00 |
| 26 | 17.50 | 40.00 |
| 27 | 17.50 | 50.00 |
| 28 | 17.50 | 60.00 |
| 29 | 26.67 | 0.0 |
| 30 | 25.86 | 10.00 |
| 31 | 25.00 | 20.00 |
| 32 | 25.00 | 30.00 |

| ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. |
|---|---|---|---|---|---|---|
| 1 | 1 | 8 | 9 | 2 | 1 | 1 |
| 2 | 2 | 9 | 10 | 3 | 1 | 1 |
| 3 | 8 | 15 | 16 | 9 | 1 | 1 |
| 4 | 16 | 17 | 10 | 9 | 1 | 1 |
| 5 | 15 | 22 | 23 | 16 | 1 | 1 |
| 6 | 16 | 23 | 24 | 17 | 1 | 1 |
| 7 | 29 | 30 | 23 | 22 | 1 | 1 |
| 8 | 23 | 30 | 31 | 24 | 1 | 1 |
| 9 | 36 | 37 | 30 | 29 | 1 | 1 |
| 10 | 37 | 38 | 31 | 30 | 1 | 1 |
| 11 | 43 | 44 | 37 | 36 | 1 | 1 |
| 12 | 37 | 44 | 45 | 38 | 1 | 1 |
| 13 | 17 | 24 | 25 | 18 | 2 | 1 |
| 14 | 18 | 25 | 26 | 19 | 2 | 1 |
| 15 | 24 | 31 | 32 | 25 | 2 | 1 |
| 16 | 32 | 33 | 26 | 25 | 2 | 1 |
| 17 | 31 | 38 | 39 | 32 | 2 | 1 |
| 18 | 32 | 39 | 40 | 33 | 2 | 1 |

| ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. |
|---|---|---|---|---|---|---|
| 19 | 38 | 45 | 46 | 39 | 2 | 1 |
| 20 | 39 | 46 | 47 | 40 | 2 | 1 |
| 21 | 19 | 26 | 27 | 20 | 2 | 2 |
| 22 | 26 | 33 | 34 | 27 | 2 | 2 |
| 23 | 33 | 40 | 41 | 34 | 2 | 2 |
| 24 | 47 | 48 | 41 | 40 | 2 | 2 |
| 25 | 20 | 27 | 28 | 21 | 3 | 2 |
| 26 | 27 | 34 | 35 | 28 | 3 | 2 |
| 27 | 34 | 41 | 42 | 35 | 3 | 2 |
| 28 | 41 | 48 | 49 | 42 | 3 | 2 |

*****BOUNDARY CONDITIONS****

| BOUNDARY NODE | | | | INCREMENT NO. |
|---|---|---|---|---|
| 49 | P-X= 0.0 | P-Y= -9.38E 02 | ANG= 0.0 | 3 |
| 42 | P-X= 0.0 | P-Y= -1.88E 03 | ANG= 0.0 | 3 |
| 35 | P-X= 0.0 | P-Y= -1.88E 03 | ANG= 0.0 | 3 |
| 28 | P-X= 0.0 | P-Y= -1.88E 03 | ANG= 0.0 | 3 |
| 21 | P-X= 0.0 | P-Y= -9.38E 02 | ANG= 0.0 | 3 |
| 1 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 2 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 3 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 1 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 8 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 15 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 22 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 29 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 36 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 43 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 44 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 45 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 46 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 47 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 48 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |
| 49 | U-X= 0.0 | P-Y= 0.0 | ANG= 0.0 | 1 |

CONSTRUCTION INCREMENT 1

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 1 | 3.33E 00 | 5.00E 00 | -2.60E-05 | -4.57E-05 | -4.00E-05 |
| 2 | 2.96E 00 | 1.50E 01 | -5.00E-05 | 5.17E-06 | -3.16E-05 |
| 3 | 9.63E 00 | 5.00E 00 | -5.30E-06 | -7.17E-05 | -5.63E-05 |
| 4 | 7.96E 00 | 1.50E 01 | -3.85E-05 | -4.54E-05 | -1.30E-04 |
| 5 | 1.60E 01 | 5.00E 00 | 3.01E-06 | -9.64E-05 | -5.72E-05 |
| 6 | 1.44E 01 | 1.50E 01 | 1.03E-05 | -1.08E-04 | -8.07E-05 |
| 7 | 2.29E 01 | 5.00E 00 | 9.35E-06 | -1.15E-04 | -3.87E-05 |
| 8 | 2.17E 01 | 1.50E 01 | 1.67E-05 | -1.27E-04 | -2.95E-05 |
| 9 | 2.98E 01 | 5.00E 00 | 8.85E-06 | -1.22E-04 | -1.94E-05 |
| 10 | 2.92E 01 | 1.50E 01 | 1.93E-05 | -1.31E-04 | -1.39E-05 |
| 11 | 3.67E 01 | 5.00E 00 | 8.53E-06 | -1.24E-04 | -6.36E-06 |
| 12 | 3.63E 01 | 1.50E 01 | 1.97E-05 | -1.33E-04 | -3.71E-06 |
| 13 | 1.38E 01 | 2.50E 01 | 9.88E-05 | -3.31E-04 | -2.45E-04 |
| | STRIP AXIAL FORCE= 5.510E 02 | | MOMENT= 5.548E-03 | | |
| | SKIN MEMBRANE STRESS= 0.374E 05 | | | | |
| 14 | 1.37E 01 | 3.50E 01 | 7.07E-05 | -1.32E-04 | 8.80E-05 |
| | STRIP AXIAL FORCE= 3.942E 02 | | MOMENT= 8.052E-03 | | |
| | SKIN MEMBRANE STRESS= 0.470E 04 | | | | |
| 15 | 2.12E 01 | 2.50E 01 | 6.07E-05 | -2.89E-04 | -1.27E-04 |
| | STRIP AXIAL FORCE= 3.385E 02 | | MOMENT= 5.894E-03 | | |
| 16 | 2.12E 01 | 3.50E 01 | 7.64E-05 | -1.56E-04 | 2.98E-05 |
| | STRIP AXIAL FORCE= 4.259E 02 | | MOMENT= 7.309E-03 | | |
| 17 | 2.87E 01 | 2.50E 01 | 4.73E-05 | -2.83E-04 | -5.28E-05 |
| | STRIP AXIAL FORCE= 2.635E 02 | | MOMENT= 6.068E-03 | | |
| 18 | 2.87E 01 | 3.50E 01 | 6.59E-05 | -1.39E-04 | 3.74E-06 |
| | STRIP AXIAL FORCE= 3.675E 02 | | MOMENT= 7.107E-03 | | |
| 19 | 3.62E 01 | 2.50E 01 | 4.23E-05 | -2.78E-04 | -1.59E-05 |
| | STRIP AXIAL FORCE= 2.357E 02 | | MOMENT= 6.126E-03 | | |
| 20 | 3.62E 01 | 3.50E 01 | 6.37E-05 | -1.38E-04 | -2.45E-07 |
| | STRIP AXIAL FORCE= 3.554E 02 | | MOMENT= 7.024E-03 | | |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 1 | -9.21E 02 | -1.15E 03 | -2.31E 02 | -7.77E 02 | -1.29E 03 | -3.19E 01 |
| 2 | -9.65E 02 | -3.28E 02 | -1.82E 02 | -2.80E 02 | -1.01E 03 | 1.05E 02 |
| 3 | -7.28E 02 | -1.49E 03 | -3.25E 02 | -6.09E 02 | -1.61E 03 | -2.02E 01 |
| 4 | -1.17E 03 | -1.25E 03 | -7.47E 02 | -4.62E 02 | -1.96E 03 | -4.35E 01 |
| 5 | -7.73E 02 | -1.92E 03 | -3.30E 02 | -6.85E 02 | -2.01E 03 | -1.50E 01 |
| 6 | -7.29E 02 | -2.09E 03 | -4.66E 02 | -5.85E 02 | -2.24E 03 | -1.71E 01 |
| 7 | -8.04E 02 | -2.24E 03 | -2.23E 02 | -7.70E 02 | -2.27E 03 | -8.67E 00 |
| 8 | -7.66E 02 | -2.43E 03 | -1.70E 02 | -7.49E 02 | -2.45E 03 | -5.77E 00 |
| 9 | -8.78E 02 | -2.39E 03 | -1.12E 02 | -8.70E 02 | -2.40E 03 | -4.21E 00 |
| 10 | -7.45E 02 | -2.48E 03 | -8.01E 01 | -7.41E 02 | -2.48E 03 | -2.64E 00 |
| 11 | -9.01E 02 | -2.43E 03 | -3.67E 01 | -9.01E 02 | -2.43E 03 | -1.37E 00 |
| 12 | -7.53E 02 | -2.52E 03 | -2.14E 01 | -7.53E 02 | -2.52E 03 | -6.96E-01 |
| 13 | -9.33E 02 | -2.03E 03 | -3.14E 02 | -8.50E 02 | -2.12E 03 | -1.49E 01 |
| 14 | -1.17E 02 | -5.79E 02 | 1.00E 02 | -9.65E 01 | -6.00E 02 | 1.17E 01 |
| 15 | -1.01E 03 | -1.91E 03 | -1.63E 02 | -9.85E 02 | -1.94E 03 | -9.99E 00 |
| 16 | -1.89E 02 | -7.19E 02 | 3.40E 01 | -1.86E 02 | -7.21E 02 | 3.65E 00 |
| 17 | -1.09E 03 | -1.94E 03 | -6.76E 01 | -1.08E 03 | -1.94E 03 | -4.54E 00 |
| 18 | -1.82E 02 | -6.49E 02 | 4.27E 00 | -1.82E 02 | -6.49E 02 | 5.23E-01 |
| 19 | -1.10E 03 | -1.92E 03 | -2.04E 01 | -1.10E 03 | -1.92E 03 | -1.42E 00 |
| 20 | -1.93E 02 | -6.52E 02 | -2.80E-01 | -1.93E 02 | -6.52E 02 | -3.49E-02 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 1 | 0.0 | 0.0 | 17 | -5.61E-04 | -1.53E-03 |
| 2 | 0.0 | -3.06E-04 | 18 | -3.18E-03 | -5.25E-03 |
| 3 | 0.0 | -3.15E-04 | 19 | -9.75E-04 | -6.14E-03 |
| 4 | 0.0 | 0.0 | 20 | 0.0 | 0.0 |
| 5 | 0.0 | 0.0 | 21 | 0.0 | 0.0 |
| 6 | 0.0 | 0.0 | 22 | 0.0 | 0.0 |
| 7 | 0.0 | 0.0 | 23 | -3.65E-04 | -1.07E-03 |
| 8 | 0.0 | 0.0 | 24 | -4.47E-04 | -2.29E-03 |
| 9 | -3.35E-04 | -5.77E-04 | 25 | -1.81E-03 | -5.19E-03 |
| 10 | -2.09E-04 | -4.38E-04 | 26 | -1.28E-03 | -6.92E-03 |
| 11 | 0.0 | 0.0 | 27 | 0.0 | 0.0 |
| 12 | 0.0 | 0.0 | 28 | 0.0 | 0.0 |
| 13 | 0.0 | 0.0 | 29 | 0.0 | 0.0 |
| 14 | 0.0 | 0.0 | 30 | -2.37E-04 | -1.20E-03 |
| 15 | 0.0 | 0.0 | 31 | -3.31E-04 | -2.48E-03 |
| 16 | -4.06E-04 | -8.12E-04 | 32 | -1.01E-03 | -5.37E-03 |
| 33 | -9.33E-04 | -6.75E-03 | | | |
| 34 | 0.0 | 0.0 | | | |
| 35 | 0.0 | 0.0 | | | |
| 36 | 0.0 | 0.0 | | | |
| 37 | -1.17E-04 | -1.23E-03 | | | |
| 38 | -1.71E-04 | -2.57E-03 | | | |
| 39 | -4.63E-04 | -5.35E-03 | | | |
| 40 | -4.93E-04 | -6.75E-03 | | | |
| 41 | 0.0 | 0.0 | | | |
| 42 | 0.0 | 0.0 | | | |
| 43 | 0.0 | 0.0 | | | |
| 44 | 0.0 | -1.25E-03 | | | |
| 45 | 0.0 | -2.58E-03 | | | |
| 46 | 0.0 | -5.36E-03 | | | |
| 47 | 0.0 | -6.72E-03 | | | |
| 48 | 0.0 | 0.0 | | | |
| 49 | 0.0 | 0.0 | | | |

CONSTRUCTION INCREMENT 2

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 1 | 3.33E 00 | 5.00E 00 | -5.40E-05 | -1.02E-04 | -8.54E-05 |
| 2 | 2.96E 00 | 1.50E 01 | -1.09E-04 | 1.10E-05 | -7.05E-05 |
| 3 | 9.63E 00 | 5.00E 00 | -7.96E-06 | -1.52E-04 | -1.09E-04 |
| 4 | 7.96E 00 | 1.50E 01 | -8.36E-05 | -1.02E-04 | -2.86E-04 |
| 5 | 1.60E 01 | 5.00E 00 | 6.87E-06 | -1.96E-04 | -1.09E-04 |
| 6 | 1.44E 01 | 1.50E 01 | 1.77E-05 | -2.22E-04 | -1.60E-04 |
| 7 | 2.29E 01 | 5.00E 00 | 1.75E-05 | -2.26E-04 | -7.07E-05 |
| 8 | 2.17E 01 | 1.50E 01 | 3.19E-05 | -2.49E-04 | -7.10E-05 |
| 9 | 2.98E 01 | 5.00E 00 | 1.68E-05 | -2.36E-04 | -3.70E-05 |
| 10 | 2.92E 01 | 1.50E 01 | 4.52E-05 | -2.57E-04 | -4.49E-05 |
| 11 | 3.67E 01 | 5.00E 00 | 1.77E-05 | -2.39E-04 | -1.31E-05 |
| 12 | 3.62E 01 | 1.50E 01 | 4.96E-05 | -2.64E-04 | -1.40E-05 |
| 13 | 1.37E 01 | 2.50E 01 | 2.31E-04 | -6.95E-04 | -5.94E-04 |
| | STRIP AXIAL FORCE= 1.285E 03 | | MOMENT= 4.430E-03 | | |
| | SKIN MEMBRANE STRESS= 0.840E 05 | | | | |
| 14 | 1.37E 01 | 3.50E 01 | 3.05E-04 | -5.45E-04 | 4.77E-05 |
| | STRIP AXIAL FORCE= 1.699E 03 | | MOMENT= 8.246E-03 | | |
| | SKIN MEMBRANE STRESS= 0.194E 05 | | | | |
| 15 | 2.12E 01 | 2.50E 01 | 1.59E-04 | -5.89E-04 | -3.89E-04 |
| | STRIP AXIAL FORCE= 8.868E 02 | | MOMENT= 5.140E-03 | | |
| 16 | 2.12E 01 | 3.50E 01 | 2.90E-04 | -6.03E-04 | -8.68E-05 |
| | STRIP AXIAL FORCE= 1.619E 03 | | MOMENT= 7.021E-03 | | |
| 17 | 2.87E 01 | 2.50E 01 | 1.44E-04 | -5.94E-04 | -1.89E-04 |
| | STRIP AXIAL FORCE= 8.032E 02 | | MOMENT= 5.516E-03 | | |
| 18 | 2.87E 01 | 3.50E 01 | 2.51E-04 | -5.62E-04 | -6.05E-05 |
| | STRIP AXIAL FORCE= 1.401E 03 | | MOMENT= 6.860E-03 | | |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 1 | -1.97E 03 | -2.52E 03 | -4.93E 02 | -1.68E 03 | -2.81E 03 | -3.04E 01 |
| 2 | -2.11E 03 | -7.24E 02 | -4.07E 02 | -6.14E 02 | -2.23E 03 | 1.05E 02 |
| 3 | -1.48E 03 | -3.15E 03 | -6.27E 02 | -1.27E 03 | -3.36E 03 | -1.85E 01 |
| 4 | -2.57E 03 | -2.78E 03 | -1.65E 03 | -1.02E 03 | -4.33E 03 | -4.32E 01 |
| 5 | -1.56E 03 | -3.90E 03 | -6.27E 02 | -1.40E 03 | -4.06E 03 | -1.41E 01 |
| 6 | -1.57E 03 | -4.34E 03 | -9.22E 02 | -1.29E 03 | -4.62E 03 | -1.68E 01 |
| 7 | -1.60E 03 | -4.42E 03 | -4.08E 02 | -1.55E 03 | -4.47E 03 | -8.09E 00 |
| 8 | -1.51E 03 | -4.75E 03 | -4.10E 02 | -1.46E 03 | -4.80E 03 | -7.09E 00 |
| 9 | -1.70E 03 | -4.62E 03 | -2.14E 02 | -1.69E 03 | -4.64E 03 | -4.16E 00 |
| 10 | -1.32E 03 | -4.81E 03 | -2.59E 02 | -1.30E 03 | -4.83E 03 | -4.22E 00 |
| 11 | -1.71E 03 | -4.67E 03 | -7.53E 01 | -1.71E 03 | -4.67E 03 | -1.46E 00 |
| 12 | -1.28E 03 | -4.89E 03 | -8.08E 01 | -1.28E 03 | -4.89E 03 | -1.26E 00 |
| 13 | -2.10E 03 | -4.92E 03 | -9.21E 02 | -1.82E 03 | -5.20E 03 | -1.65E 01 |
| 14 | -4.84E 02 | -2.85E 03 | 4.10E 01 | -4.83E 02 | -2.86E 03 | 9.90E-01 |
| 15 | -2.06E 03 | -4.32E 03 | -6.11E 02 | -1.91E 03 | -4.48E 03 | -1.42E 01 |
| 16 | -9.46E 02 | -3.46E 03 | -1.41E 02 | -9.38E 02 | -3.47E 03 | -3.20E 00 |
| 17 | -2.23E 03 | -4.48E 03 | -3.02E 02 | -2.19E 03 | -4.52E 03 | -7.51E 00 |
| 18 | -1.05E 03 | -3.33E 03 | -9.14E 01 | -1.04E 03 | -3.33E 03 | -2.29E 00 |

```
ELEMENT
 NO.          X            Y        EPSILON-X  EPSILON-Y   GAMA-XY

19        3.62E 01    2.50E 01    1.37E-04  -5.89E-04  -6.02E-05
     STRIP AXIAL FORCE=  7.641E 02    MOMENT=  5.643E-03

20        3.62E 01    3.50E 01    2.37E-04  -5.56E-04  -2.02E-05
     STRIP AXIAL FORCE=  1.323E 03    MOMENT=  6.797E-03

21        1.37E 01    4.50E 01    1.78E-04  -3.36E-04   8.20E-05
     STRIP AXIAL FORCE=  9.910E 02    MOMENT=  6.618E-03
       SKIN MEMBRANE STRESS=  0.142E 05

22        2.12E 01    4.50E 01    2.03E-04  -3.96E-04   1.02E-04
     STRIP AXIAL FORCE=  1.132E 03    MOMENT=  6.690E-03

23        2.87E 01    4.50E 01    1.89E-04  -3.96E-04   5.42E-05
     STRIP AXIAL FORCE=  1.053E 03    MOMENT=  6.520E-03

24        3.62E 01    4.50E 01    1.79E-04  -3.87E-04   1.97E-05
     STRIP AXIAL FORCE=  9.984E 02    MOMENT=  6.480E-03

25        1.38E 01    5.50E 01    6.14E-05  -1.24E-04   7.51E-05
     STRIP AXIAL FORCE=  3.424E 02    MOMENT=  7.874E-03
       SKIN MEMBRANE STRESS=  0.582E 04

26        2.13E 01    5.50E 01    9.83E-05  -1.62E-04   1.15E-04
     STRIP AXIAL FORCE=  5.481E 02    MOMENT=  7.697E-03

27        2.88E 01    5.50E 01    1.25E-04  -1.84E-04   7.46E-05
     STRIP AXIAL FORCE=  6.993E 02    MOMENT=  7.496E-03

28        3.63E 01    5.50E 01    1.36E-04  -1.91E-04   2.30E-05
     STRIP AXIAL FORCE=  7.581E 02    MOMENT=  7.351E-03
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| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 19 | -2.26E 03 | -4.48E 03 | -9.65E 01 | -2.26E 03 | -4.48E 03 | -2.49E |
| 20 | -1.13E 03 | -3.36E 03 | -3.01E 01 | -1.13E 03 | -3.36E 03 | -7.75E |
| 21 | -3.54E 02 | -1.67E 03 | 1.05E 02 | -3.46E 02 | -1.68E 03 | 4.53E |
| 22 | -4.69E 02 | -2.00E 03 | 1.31E 02 | -4.58E 02 | -2.01E 03 | 4.85E |
| 23 | -5.76E 02 | -2.07E 03 | 6.94E 01 | -5.73E 02 | -2.08E 03 | 2.65E |
| 24 | -6.06E 02 | -2.06E 03 | 2.52E 01 | -6.05E 02 | -2.06E 03 | 9.98E-01 |
| 25 | -1.45E 02 | -5.68E 02 | 8.57E 01 | -1.29E 02 | -5.85E 02 | 1.10E 01 |
| 26 | -6.69E 01 | -6.61E 02 | 1.31E 02 | -3.94E 01 | -6.89E 02 | 1.19E 01 |
| 27 | 1.97E 01 | -6.86E 02 | 8.51E 01 | 2.98E 01 | -6.96E 02 | 6.78E 00 |
| 28 | 6.12E 01 | -6.84E 02 | 2.62E 01 | 6.21E 01 | -6.85E 02 | 2.01E 00 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 1 | 0.0 | 0.0 | 17 | -1.31E-03 | -3.35E-03 |
| 2 | 0.0 | -6.86E-04 | 18 | -8.76E-03 | -1.15E-02 |
| 3 | 0.0 | -7.22E-04 | 19 | -7.50E-03 | -1.60E-02 |
| 4 | 0.0 | 0.0 | 20 | -4.71E-03 | -1.27E-02 |
| 5 | 0.0 | 0.0 | 21 | -1.61E-03 | -1.37E-02 |
| 6 | 0.0 | 0.0 | 22 | 0.0 | 0.0 |
| 7 | 0.0 | 0.0 | 23 | -7.08E-04 | -2.15E-03 |
| 8 | 0.0 | 0.0 | 24 | -1.13E-03 | -4.57E-03 |
| 9 | -6.95E-04 | -1.28E-03 | 25 | -5.47E-03 | -1.03E-02 |
| 10 | -4.95E-04 | -9.64E-04 | 26 | -6.22E-03 | -1.68E-02 |
| 11 | 0.0 | 0.0 | 27 | -3.64E-03 | -1.37E-02 |
| 12 | 0.0 | 0.0 | 28 | -1.76E-03 | -1.52E-02 |
| 13 | 0.0 | 0.0 | 29 | 0.0 | 0.0 |
| 14 | 0.0 | 0.0 | 30 | -4.70E-04 | -2.34E-03 |
| 15 | 0.0 | 0.0 | 31 | -9.08E-04 | -4.84E-03 |
| 16 | -8.03E-04 | -1.69E-03 | 32 | -3.31E-03 | -1.08E-02 |
| 33 | -4.02E-03 | -1.65E-02 | | | |
| 34 | -2.43E-03 | -1.38E-02 | | | |
| 35 | -1.49E-03 | -1.55E-02 | | | |
| 36 | 0.0 | 0.0 | | | |
| 37 | -2.42E-04 | -2.38E-03 | | | |
| 38 | -4.80E-04 | -5.01E-03 | | | |
| 39 | -1.58E-03 | -1.09E-02 | | | |
| 40 | -1.98E-03 | -1.65E-02 | | | |
| 41 | -1.20E-03 | -1.36E-02 | | | |
| 42 | -8.44E-04 | -1.55E-02 | | | |
| 43 | 0.0 | 0.0 | | | |
| 44 | 0.0 | -2.40E-03 | | | |
| 45 | 0.0 | -5.03E-03 | | | |
| 46 | 0.0 | -1.09E-02 | | | |
| 47 | 0.0 | -1.64E-02 | | | |
| 48 | 0.0 | -1.36E-02 | | | |
| 49 | 0.0 | -0.02 | | | |

CONSTRUCTION INCREMENT 3

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 1 | 3.33E 00 | 5.00E 00 | -5.66E-05 | -1.07E-04 | -8.99E-05 |
| 2 | 2.96E 00 | 1.50E 01 | -1.15E-04 | 1.15E-05 | -7.43E-05 |
| 3 | 9.63E 00 | 5.00E 00 | -8.05E-06 | -1.60E-04 | -1.14E-04 |
| 4 | 7.96E 00 | 1.50E 01 | -8.76E-05 | -1.08E-04 | -3.02E-04 |
| 5 | 1.60E 01 | 5.00E 00 | 7.40E-06 | -2.06E-04 | -1.13E-04 |
| 6 | 1.44E 01 | 1.50E 01 | 1.89E-05 | -2.34E-04 | -1.67E-04 |
| 7 | 2.29E 01 | 5.00E 00 | 1.83E-05 | -2.37E-04 | -7.31E-05 |
| 8 | 2.17E 01 | 1.50E 01 | 3.35E-05 | -2.61E-04 | -7.36E-05 |
| 9 | 2.98E 01 | 5.00E 00 | 1.74E-05 | -2.47E-04 | -3.81E-05 |
| 10 | 2.92E 01 | 1.50E 01 | 4.73E-05 | -2.69E-04 | -4.68E-05 |
| 11 | 3.67E 01 | 5.00E 00 | 1.83E-05 | -2.49E-04 | -1.35E-05 |
| 12 | 3.62E 01 | 1.50E 01 | 5.18E-05 | -2.75E-04 | -1.46E-05 |
| 13 | 1.37E 01 | 2.50E 01 | 2.44E-04 | -7.30E-04 | -6.23E-04 |
| | STRIP AXIAL FORCE= 1.359E 03 | | MOMENT= 4.322E-03 | | |
| | SKIN MEMBRANE STRESS= 0.886E 05 | | | | |
| 14 | 1.37E 01 | 3.50E 01 | 3.28E-04 | -5.86E-04 | 4.75E-05 |
| | STRIP AXIAL FORCE= 1.829E 03 | | MOMENT= 8.263E-03 | | |
| | SKIN MEMBRANE STRESS= 0.209E 05 | | | | |
| 15 | 2.12E 01 | 2.50E 01 | 1.68E-04 | -6.16E-04 | -4.07E-04 |
| | STRIP AXIAL FORCE= 9.356E 02 | | MOMENT= 5.074E-03 | | |
| 16 | 2.12E 01 | 3.50E 01 | 3.10E-04 | -6.41E-04 | -9.59E-05 |
| | STRIP AXIAL FORCE= 1.727E 03 | | MOMENT= 6.989E-03 | | |
| 17 | 2.87E 01 | 2.50E 01 | 1.52E-04 | -6.20E-04 | -1.98E-04 |
| | STRIP AXIAL FORCE= 8.475E 02 | | MOMENT= 5.471E-03 | | |
| 18 | 2.87E 01 | 3.50E 01 | 2.68E-04 | -5.97E-04 | -6.65E-05 |
| | STRIP AXIAL FORCE= 1.495E 03 | | MOMENT= 6.825E-03 | | |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 1 | -2.07E 03 | -2.65E 03 | -5.19E 02 | -1.77E 03 | -2.96E 03 | -3.03E 01 |
| 2 | -2.22E 03 | -7.63E 02 | -4.29E 02 | -6.47E 02 | -2.34E 03 | 1.05E 02 |
| 3 | -1.55E 03 | -3.31E 03 | -6.55E 02 | -1.33E 03 | -3.53E 03 | -1.83E 01 |
| 4 | -2.70E 03 | -2.94E 03 | -1.74E 03 | -1.07E 03 | -4.56E 03 | -4.31E 01 |
| 5 | -1.63E 03 | -4.10E 03 | -6.53E 02 | -1.47E 03 | -4.26E 03 | -1.40E 01 |
| 6 | -1.64E 03 | -4.56E 03 | -9.63E 02 | -1.36E 03 | -4.85E 03 | -1.67E 01 |
| 7 | -1.68E 03 | -4.63E 03 | -4.22E 02 | -1.62E 03 | -4.68E 03 | -7.99E 00 |
| 8 | -1.58E 03 | -4.98E 03 | -4.25E 02 | -1.53E 03 | -5.03E 03 | -7.02E 00 |
| 9 | -1.78E 03 | -4.83E 03 | -2.20E 02 | -1.77E 03 | -4.85E 03 | -4.10E 00 |
| 10 | -1.37E 03 | -5.02E 03 | -2.70E 02 | -1.35E 03 | -5.04E 03 | -4.20E 00 |
| 11 | -1.79E 03 | -4.88E 03 | -7.76E 01 | -1.79E 03 | -4.88E 03 | -1.44E 00 |
| 12 | -1.33E 03 | -5.11E 03 | -8.41E 01 | -1.33E 03 | -5.11E 03 | -1.28E 00 |
| 13 | -2.21E 03 | -5.23E 03 | -9.76E 02 | -1.92E 03 | -5.51E 03 | -1.65E 01 |
| 14 | -5.22E 02 | -3.11E 03 | 4.07E 01 | -5.21E 02 | -3.11E 03 | 9.01E-01 |
| 15 | -2.16E 03 | -4.56E 03 | -6.47E 02 | -2.00E 03 | -4.72E 03 | -1.42E 01 |
| 16 | -1.01E 03 | -3.73E 03 | -1.57E 02 | -9.99E 02 | -3.74E 03 | -3.30E 00 |
| 17 | -2.33E 03 | -4.71E 03 | -3.19E 02 | -2.29E 03 | -4.75E 03 | -7.51E 00 |
| 18 | -1.11E 03 | -3.57E 03 | -1.02E 02 | -1.11E 03 | -3.57E 03 | -2.37E 00 |

```
ELEMENT
 NO.          X            Y        EPSILON-X  EPSILON-Y   GAMA-XY

19        3.62E 01    2.50E 01    1.45E-04  -6.14E-04  -6.32E-05
     STRIP AXIAL FORCE=  8.062E 02    MOMENT=  5.604E-03

20        3.62E 01    3.50E 01    2.53E-04  -5.90E-04  -2.23E-05
     STRIP AXIAL FORCE=  1.411E 03    MOMENT=  6.761E-03

21        1.37E 01    4.50E 01    2.02E-04  -3.81E-04   8.21E-05
     STRIP AXIAL FORCE=  1.128E 03    MOMENT=  6.590E-03
       SKIN MEMBRANE STRESS=  0.161E 05

22        2.12E 01    4.50E 01    2.28E-04  -4.41E-04   1.02E-04
     STRIP AXIAL FORCE=  1.271E 03    MOMENT=  6.673E-03

23        2.87E 01    4.50E 01    2.13E-04  -4.39E-04   5.16E-05
     STRIP AXIAL FORCE=  1.185E 03    MOMENT=  6.492E-03

24        3.62E 01    4.50E 01    2.02E-04  -4.29E-04   1.88E-05
     STRIP AXIAL FORCE=  1.127E 03    MOMENT=  6.451E-03

25        1.37E 01    5.50E 01    9.17E-05  -1.79E-04   7.52E-05
     STRIP AXIAL FORCE=  5.113E 02    MOMENT=  7.851E-03
       SKIN MEMBRANE STRESS=  0.765E 04

26        2.12E 01    5.50E 01    1.28E-04  -2.17E-04   1.14E-04
     STRIP AXIAL FORCE=  7.149E 02    MOMENT=  7.669E-03

27        2.87E 01    5.50E 01    1.55E-04  -2.38E-04   7.39E-05
     STRIP AXIAL FORCE=  8.647E 02    MOMENT=  7.470E-03

28        3.62E 01    5.50E 01    1.65E-04  -2.44E-04   2.24E-05
     STRIP AXIAL FORCE=  9.215E 02    MOMENT=  7.323E-03
```

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 19 | -2.36E 03 | -4.70E 03 | -1.02E 02 | -2.36E 03 | -4.71E 03 | -2.50E 00 |
| 20 | -1.20E 03 | -3.60E 03 | -3.37E 01 | -1.20E 03 | -3.60E 03 | -8.06E-01 |
| 21 | -4.02E 02 | -1.92E 03 | 1.05E 02 | -3.95E 02 | -1.92E 03 | 3.95E 00 |
| 22 | -5.13E 02 | -2.26E 03 | 1.30E 02 | -5.04E 02 | -2.27E 03 | 4.24E 00 |
| 23 | -6.24E 02 | -2.33E 03 | 6.54E 01 | -6.22E 02 | -2.33E 03 | 2.20E 00 |
| 24 | -6.54E 02 | -2.30E 03 | 2.38E 01 | -6.54E 02 | -2.30E 03 | 8.28E-01 |
| 25 | -1.91E 02 | -8.18E 02 | 8.58E 01 | -1.79E 02 | -8.29E 02 | 7.66E 00 |
| 26 | -1.13E 02 | -9.12E 02 | 1.31E 02 | -9.24E 01 | -9.33E 02 | 9.05E 00 |
| 27 | -2.66E 01 | -9.36E 02 | 8.42E 01 | -1.88E 01 | -9.44E 02 | 5.24E 00 |
| 28 | 1.39E 01 | -9.34E 02 | 2.55E 01 | 1.46E 01 | -9.34E 02 | 1.54E 00 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 1 | 0.0 | 0.0 | 17 | -1.37E-03 | -3.54E-03 |
| 2 | 0.0 | -7.24E-04 | 18 | -9.25E-03 | -1.21E-02 |
| 3 | 0.0 | -7.64E-04 | 19 | -8.14E-03 | -1.70E-02 |
| 4 | 0.0 | 0.0 | 20 | -5.52E-03 | -1.41E-02 |
| 5 | 0.0 | 0.0 | 21 | -2.59E-03 | -1.57E-02 |
| 6 | 0.0 | 0.0 | 22 | 0.0 | 0.0 |
| 7 | 0.0 | 0.0 | 23 | -7.37E-04 | -2.26E-03 |
| 8 | 0.0 | 0.0 | 24 | -1.19E-03 | -4.80E-03 |
| 9 | -7.29E-04 | -1.35E-03 | 25 | -5.78E-03 | -1.08E-02 |
| 10 | -5.21E-04 | -1.02E-03 | 26 | -6.69E-03 | -1.77E-02 |
| 11 | 0.0 | 0.0 | 27 | -4.24E-03 | -1.51E-02 |
| 12 | 0.0 | 0.0 | 28 | -2.50E-03 | -1.71E-02 |
| 13 | 0.0 | 0.0 | 29 | 0.0 | 0.0 |
| 14 | 0.0 | 0.0 | 30 | -4.88E-04 | -2.45E-03 |
| 15 | 0.0 | 0.0 | 31 | -9.54E-04 | -5.06E-03 |
| 16 | -8.38E-04 | -1.78E-03 | 32 | -3.50E-03 | -1.13E-02 |
| 33 | -4.32E-03 | -1.73E-02 | | | |
| 34 | -2.83E-03 | -1.51E-02 | | | |
| 35 | -1.97E-03 | -1.74E-02 | | | |
| 36 | 0.0 | 0.0 | | | |
| 37 | -2.50E-04 | -2.48E-03 | | | |
| 38 | -5.04E-04 | -5.23E-03 | | | |
| 39 | -1.67E-03 | -1.14E-02 | | | |
| 40 | -2.13E-03 | -1.73E-02 | | | |
| 41 | -1.39E-03 | -1.49E-02 | | | |
| 42 | -1.09E-03 | -1.73E-02 | | | |
| 43 | 0.0 | 0.0 | | | |
| 44 | 0.0 | -2.50E-03 | | | |
| 45 | 0.0 | -5.25E-03 | | | |
| 46 | 0.0 | -1.14E-02 | | | |
| 47 | 0.0 | -1.72E-02 | | | |
| 48 | 0.0 | -1.48E-02 | | | |
| 49 | 0.0 | -0.02 | | | |

# APPENDIX D

## LIST OF THE FINITE ELEMENT COMPUTOR PROGRAM

## AND

## EXAMPLE OF INPUT AND OUTPUT DATA

INPUT EXAMPLE

```
REINFORCED EARTH PROJECT 39 STA 551+75
12 11. 0E132VANVORIS444-4733
1 0 1 0.0 737. 1000000. .30 40. 900.
2 0 1 168. 555000. .30 40. 0.5
3 0 1 143. 737. 1000000. .30 40. 900.
4 3 1 143. 335. 1440000. .30 39.5 1000.
4104.E+6 .197 .00983 1.64 .833 0 .01
5 3 1 143. 335. 1440000. .30 39.5 1000.
4104.E+6 .197 .00983 3.28 .833 0 .01
6 3 1 143. 335. 1440000. .30 39.5 1000.
4104.E+6 .197 .00983 4.92 .833 0 .01
1
1 0. 50. 43 200. 50. 7 1.
43 200. 50. 169 410.93 206.80 9 1.
180 426. 218. 348 509.5 280.5 21 1.
348 509.5 280.5 400 562. 320.18 13 1.
406 575. 330.
1 0. 50. 3 0. 140. 1 1.
3 0. 140. 24 79. 140. 7 1.
```



HCS 90 – 062

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 24 | 79. | 140. | 45 | 148. | 150. | 7 | 1. |
| 45 | 148. | 150. | 72 | 203. | 161. | 9 | 1. |
| 72 | 203. | 161. | 126 | 300. | 207. | 9 | 1. |
| 126 | 300. | 207. | 171 | 375. | 256.17 | 9 | 1. |
| 182 | 390. | 266. | 350 | 473. | 331.8 | 21 | 1. |
| 350 | 473. | 331.8 | 402 | 525.5 | 371. | 13 | 1. |
| 408 | 540. | 381. | 409 | 528. | 399. | 1 | 1. |
| 410 | 520. | 410. | 412 | 575. | 410. | 1 | 1. |
| 407 | 558. | 355. | | | | | |
| 413 | 575. | 367. | | | | | |
| 4 | 0. | 150. | | | | | |
| 5 | 0. | 178. | | | | | |
| 11 | 27. | 150. | | | | | |
| 12 | 26.33 | 162.67 | | | | | |
| 13 | 25. | 188. | | | | | |
| 18 | 60. | 150. | 20 | 50. | 200. | 1 | 1. |
| 25 | 75. | 160. | | | | | |
| 27 | 65. | 200. | | | | | |
| 32 | 94.40 | 165.40 | | | | | |

HCS 90 – 062

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 34 | 80. | 207. | | | | | |
| 39 | 122. | 155. | | | | | |
| 40 | 113.67 | 176. | | | | | |
| 42 | 97. | 218. | | | | | |
| 45 | 148. | 150. | 47 | 131. | 185. | 1 | 1. |
| 47 | 131. | 185. | 49 | 111. | 226. | 1 | 1. |
| 49 | 111. | 226. | 103 | 196.6 | 278. | 9 | 1. |
| 47 | 131. | 185. | 110 | 238. | 240. | 9 | 1. |
| 117 | 283.83 | 199.33 | 119 | 252.38 | 249.63 | 1 | 1. |
| 126 | 300. | 207. | 128 | 274.78 | 246.71 | 1 | 1. |
| 129 | 266.75 | 259.25 | 165 | 324.25 | 297.75 | 9 | 1. |
| 132 | 239.40 | 304. | 168 | 296.46 | 338.66 | 9 | 1. |
| 101 | 222.71 | 232.14 | 103 | 196.60 | 278. | 1 | 1. |
| 110 | 238. | 240. | 113 | 210.90 | 286.70 | 1 | 1. |
| 122 | 225.13 | 295.33 | | | | | |
| 176 | 338.63 | 307.38 | 179 | 310.73 | 347.33 | 1 | 1. |
| 128 | 274.78 | 246.71 | 173 | 347.46 | 295.28 | 9 | 1. |
| 183 | 375.34 | 285.41 | 351 | 461. | 349. | 21 | 1. |
| 351 | 461. | 349. | 403 | 513. | 387. | 13 | 1. |

HCS 90 – 062

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 184 | 362. | 305. | 352 | 447.5 | 368. | 21 | 1. |
| 352 | 447.5 | 368. | 404 | 495.5 | 406. | 13 | 1. |
| 185 | 353. | 317. | 353 | 442. | 377. | 21 | 1. |
| 353 | 442. | 377. | 405 | 490. | 410. | 13 | 1. |
| 185 | 353. | 317. | 189 | 325. | 356. | 1 | 1. |
| 174 | 340. | 340. | 175 | 338. | 346.5 | 1 | 1. |
| 190 | 338. | 356. | 191 | 338. | 360. | 1 | 1. |
| 192 | 332. | 360. | 194 | 342. | 365.5 | 2 | 1. |
| 193 | 343. | 364. | | | | | |
| 195 | 347. | 338.5 | 196 | 347. | 346.5 | 1 | 1. |
| 197 | 347. | 356. | 198 | 347. | 360. | 1 | 1. |
| 199 | 350. | 365. | 200 | 350. | 370. | 1 | 1. |
| 207 | 360. | 338.5 | 208 | 360. | 346.5 | 1 | 1. |
| 209 | 360. | 356. | | | | | |
| 210 | 360. | 360. | 212 | 360. | 370. | 1 | 1. |
| 213 | 360. | 373. | 216 | 360. | 385. | 1 | 1. |
| 217 | 360. | 388. | 220 | 360. | 404.5 | 1 | 1. |
| 221 | 363.71 | 410. | | | | | |
| 228 | 371. | 338.5 | | | | | |



HCS 90 – 062

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 229 | 371. | 346.5 | 230 | 371. | 356. | 1 | 1. |
| 231 | 371. | 360. | 233 | 371. | 370. | 1 | 1. |
| 234 | 371. | 373. | 237 | 371. | 385. | 1 | 1. |
| 238 | 371. | 388. | 242 | 371. | 410. | 1 | 1. |
| 249 | 380. | 341. | 250 | 383. | 346.5 | 1 | 1. |
| 251 | 383. | 356. | 252 | 383. | 360. | 1 | 1. |
| 252 | 383. | 360. | 254 | 383. | 370. | 1 | 1. |
| 255 | 383. | 373. | 258 | 383. | 385. | 1 | 1. |
| 259 | 383. | 388. | 263 | 383. | 410. | 1 | 1. |
| 272 | 395. | 356. | 273 | 395. | 360. | 1 | 1. |
| 273 | 395. | 360. | 275 | 395. | 370. | 1 | 1. |
| 276 | 395. | 373. | 279 | 395. | 385. | 1 | 1. |
| 280 | 395. | 388. | 284 | 395. | 410. | 1 | 1. |
| 291 | 406. | 356. | 294 | 406. | 360. | 3 | 1. |
| 294 | 406. | 360. | 296 | 406. | 370. | 1 | 1. |
| 297 | 406. | 373. | 300 | 406. | 385. | 1 | 1. |
| 301 | 406. | 388. | 305 | 406. | 410. | 1 | 1. |
| 316 | 413. | 365. | 317 | 419. | 369. | 1 | 1. |
| 318 | 417. | 373. | 321 | 417. | 385. | 1 | 1. |

HCS 90 – 062

| 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 | 56–60 | 61–65 | 66–70 | 71–75 | 76–80 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 372 | | 417. | | 388. | 326 | | 417. | | 410. | 1 | | 1. | | | |
| 339 | | 427. | | 373. | 340 | | 432. | | 377. | 1 | | 1. | | | |
| 341 | | 429. | | 381. | 343 | | 429. | | 389. | 1 | | 1. | | | |
| 344 | | 429. | | 393.5 | 347 | | 429. | | 410. | 1 | | 1. | | | |
| 354 | | 440. | | 381. | 355 | | 446. | | 385. | 1 | | 1. | | | |
| 356 | | 441. | | 389. | | | | | | | | | | | |
| 357 | | 441. | | 393.5 | 360 | | 441. | | 410. | 1 | | 1. | | | |
| 367 | | 450. | | 389. | | | | | | | | | | | |
| 368 | | 455. | | 393.5 | 371 | | 455. | | 410. | 1 | | 1. | | | |
| 380 | | 465. | | 399. | 381 | | 470. | | 404.5 | 1 | | 1. | | | |
| 382 | | 470. | | 410. | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | |
| 1 | 8 | 9 | 2 | 1 | 1 | 5 | 7 | 1 | 1 | 0 | | | | | |
| 43 | 52 | 53 | 44 | 1 | 1 | 13 | 9 | 1 | 1 | 0 | | | | | |
| 169 | 180 | 181 | 170 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | | | | | |
| 180 | 201 | 202 | 181 | 1 | 1 | 7 | 21 | 1 | 1 | 0 | | | | | |
| 348 | 361 | 362 | 349 | 1 | 1 | 3 | 13 | 1 | 1 | 0 | | | | | |
| 400 | 406 | 407 | 401 | 1 | 1 | 0 | 0 | 1 | 1 | 0 | | | | | |
| 406 | 413 | 407 | | 1 | 1 | | | | | 0 | | | | | |

HCS 90 – 062

| 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 |
|---|---|---|---|---|---|---|---|---|---|---|
| 4.07 | 4.13 | 4.12 | 4.08 | 1 | 1 | | | | | 0 |
| 3 | 1.0 | 1.1 | 4 | 2 | 1 | 3 | 7 | 0 | 0 | 0 |
| 3.1 | 3.8 | 3.9 | | 2 | 1 | | | | | 0 |
| 3.1 | 3.9 | 4.0 | 3.2 | 2 | 1 | | | | | 0 |
| 3.8 | 4.5 | 4.6 | 3.9 | 2 | 1 | 0 | 0 | 1 | 1 | 0 |
| 4.5 | 5.4 | 5.5 | 4.6 | 2 | 1 | 7 | 9 | 1 | 1 | 0 |
| 1.17 | 1.26 | 1.27 | 1.18 | 2 | 1 | | | | | 0 |
| 1.18 | 1.27 | 1.28 | 1.19 | 2 | 1 | | | | | 0 |
| 1.28 | 1.29 | 1.19 | | 2 | 1 | | | | | 0 |
| 1.26 | 1.35 | 1.36 | 1.27 | 2 | 1 | 3 | 9 | 2 | 1 | 0 |
| 1.62 | 1.71 | 1.72 | 1.63 | 2 | 1 | 0 | 0 | 1 | 1 | 0 |
| 1.64 | 1.73 | 1.76 | 1.65 | 2 | 1 | | | | | 0 |
| 1.71 | 1.82 | 1.83 | 1.72 | 2 | 1 | 0 | 0 | 1 | 1 | 0 |
| 1.73 | 1.84 | 1.85 | 1.76 | 2 | 1 | | | | | 0 |
| 1.82 | 2.03 | 2.04 | 1.83 | 2 | 1 | 7 | 21 | 2 | 1 | 0 |
| 3.50 | 3.63 | 3.64 | 3.51 | 2 | 1 | 3 | 13 | 2 | 1 | 0 |
| 4.02 | 4.08 | 4.09 | 4.03 | 2 | 1 | 0 | 0 | 1 | 1 | 0 |
| 4.04 | 4.10 | 4.05 | | 2 | 1 | | | | | 0 |
| 4.08 | 4.12 | 4.11 | 4.09 | 2 | 1 | | | | | 0 |

HCS 90 – 062

| 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 |
|---|---|---|---|---|---|---|---|---|---|---|
| 409 | 411 | 410 | | 2 | 1 | | | | | 0 |
| 4 | 11 | 12 | | 3 | 2 | | | | | 0 |
| 4 | 12 | 13 | 5 | 3 | 2 | | | | | 0 |
| 11 | 18 | 19 | 12 | 3 | 2 | 2 | 7 | 1 | 1 | 0 |
| 32 | 40 | 41 | 33 | 3 | 2 | 0 | 0 | 1 | 1 | 0 |
| 40 | 47 | 48 | 41 | 3 | 2 | 0 | 0 | 1 | 1 | 0 |
| 47 | 56 | 57 | 48 | 3 | 2 | 5 | 9 | 1 | 1 | 0 |
| 101 | 110 | 111 | 102 | 3 | 2 | | | | | 0 |
| 102 | 111 | 112 | 103 | 3 | 2 | | | | | 0 |
| 112 | 113 | 103 | | 3 | 2 | | | | | 0 |
| 110 | 119 | 120 | 111 | 3 | 2 | 0 | 0 | 2 | 1 | 0 |
| 119 | 129 | 130 | 120 | 3 | 2 | 0 | 0 | 2 | 1 | 0 |
| 129 | 138 | 139 | 130 | 3 | 2 | 3 | 9 | 2 | 1 | 0 |
| 165 | 176 | 177 | 166 | 3 | 2 | 0 | 11 | 2 | 1 | 0 |
| 176 | 185 | 186 | | 3 | 2 | | | | | 0 |
| 176 | 186 | 187 | 177 | 3 | 2 | | | 2 | 1 | 0 |
| 185 | 206 | 186 | | 3 | 2 | | | | | 0 |
| 186 | 195 | 174 | 187 | 3 | 2 | | | | | 0 |
| 186 | 206 | 207 | 195 | 3 | 2 | | | | | 0 |

HCS 90 – 062

| 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 | 56–60 | 61–65 | 66–70 | 71–75 | 76–80 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 206 | 227 | 228 | 207 | 3 | 2 | | | | | 0 | | | | | |
| 227 | 248 | 249 | 228 | 3 | 2 | | | | | 0 | | | | | |
| 187 | 174 | 175 | 188 | 3 | 2 | | | | | 0 | | | | | |
| 174 | 195 | 196 | 175 | 3 | 2 | | | | | 0 | | | | | |
| 195 | 207 | 208 | 196 | 3 | 2 | | | | | 0 | | | | | |
| 207 | 228 | 229 | 208 | 3 | 2 | 1 | 21 | 0 | 0 | 0 | | | | | |
| 249 | 248 | 269 | 250 | 3 | 2 | | | | | 0 | | | | | |
| 188 | 175 | 190 | 189 | 3 | 2 | | | | | 0 | | | | | |
| 175 | 196 | 197 | 190 | 3 | 2 | | | | | 0 | | | | | |
| 196 | 208 | 209 | 197 | 3 | 2 | | | | | 0 | | | | | |
| 208 | 229 | 230 | 209 | 3 | 2 | 1 | 21 | 0 | 0 | 0 | | | | | |
| 250 | 269 | 272 | 251 | 3 | 2 | | | | | 0 | | | | | |
| 269 | 290 | 291 | 272 | 3 | 2 | | | | | 0 | | | | | |
| 209 | 230 | 231 | 210 | 4 | 3 | | | | | 1 | | | | | |
| 230 | 251 | 252 | 231 | 4 | 3 | 1 | 21 | | | 0 | | | | | |
| 272 | 291 | 294 | 273 | 4 | 3 | | | | | 0 | | | | | |
| 291 | 290 | 311 | 294 | 3 | 3 | | | | | 0 | | | | | |
| 210 | 231 | 232 | 211 | 4 | 4 | | | | | 1 | | | | | |
| 231 | 252 | 253 | 232 | 4 | 4 | 2 | 21 | | | 0 | | | | | |

HCS 90 – 062

| 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 | 56–60 | 61–65 | 66–70 | 71–75 | 76–80 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 294 | 311 | 316 | 295 | 3 | 4 | | | | | 0 | | | | | |
| 211 | 232 | 233 | 212 | 4 | 5 | | | | | 1 | | | | | |
| 232 | 253 | 254 | 233 | 4 | 5 | 2 | 21 | | | 0 | | | | | |
| 295 | 316 | 317 | 296 | 3 | 5 | | | | | 0 | | | | | |
| 311 | 332 | 317 | 316 | 3 | 5 | | | | | 0 | | | | | |
| 212 | 233 | 234 | 213 | 5 | 6 | | | | | 1 | | | | | |
| 233 | 254 | 255 | 234 | 5 | 6 | 2 | 21 | | | 0 | | | | | |
| 296 | 317 | 318 | 297 | 3 | 6 | | | | | 0 | | | | | |
| 317 | 332 | 339 | 318 | 3 | 6 | | | | | 0 | | | | | |
| 213 | 234 | 235 | 214 | 5 | 7 | | | 1 | 1 | 1 | | | | | |
| 234 | 255 | 256 | 235 | 5 | 7 | 2 | 21 | 1 | 1 | 0 | | | | | |
| 297 | 318 | 319 | 298 | 3 | 7 | 1 | 21 | 1 | 1 | 0 | | | | | |
| 332 | 353 | 340 | 339 | 3 | 7 | | | | | 0 | | | | | |
| 340 | 353 | 354 | 341 | 3 | 7 | | | | | 0 | | | | | |
| 215 | 236 | 237 | 216 | 5 | 8 | | | 1 | 1 | 1 | | | | | |
| 236 | 257 | 258 | 237 | 5 | 8 | 2 | 21 | 1 | 1 | 0 | | | | | |
| 299 | 320 | 321 | 300 | 3 | 8 | 1 | 21 | 1 | 1 | 0 | | | | | |
| 341 | 354 | 355 | 342 | 3 | 8 | | | 1 | 1 | 0 | | | | | |
| 353 | 366 | 355 | 354 | 3 | 8 | | | | | 0 | | | | | |

HCS 90 – 062

| 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 | 56–60 | 61–65 | 66–70 | 71–75 | 76–80 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 355 | 366 | 367 | 356 | 3 | 8 | | | | | 0 | | | | | |
| 217 | 238 | 239 | 218 | 6 | 9 | | | 1 | 1 | 1 | | | | | |
| 238 | 259 | 260 | 239 | 6 | 9 | 2 | 21 | 1 | 1 | 0 | | | | | |
| 301 | 322 | 323 | 302 | 3 | 9 | 1 | 21 | 1 | 1 | 0 | | | | | |
| 343 | 356 | 357 | 344 | 3 | 9 | | | 1 | 1 | 0 | | | | | |
| 356 | 367 | 368 | 357 | 3 | 9 | | | 1 | 1 | 0 | | | | | |
| 366 | 379 | 368 | 367 | 3 | 9 | | | | | 0 | | | | | |
| 368 | 379 | 380 | 369 | 3 | 9 | | | | | 0 | | | | | |
| 219 | 240 | 241 | 220 | 6 | 10 | | | | | 1 | | | | | |
| 240 | 261 | 262 | 241 | 6 | 10 | 2 | 21 | | | 0 | | | | | |
| 303 | 324 | 325 | 304 | 3 | 10 | 1 | 21 | | | 0 | | | | | |
| 345 | 358 | 359 | 346 | 3 | 10 | | | | | 0 | | | | | |
| 358 | 369 | 370 | 359 | 3 | 10 | 1 | 11 | | | 0 | | | | | |
| 379 | 392 | 381 | 380 | 3 | 10 | | | | | 0 | | | | | |
| 189 | 190 | 191 | 192 | 3 | 11 | | | | | 0 | | | | | |
| 190 | 197 | 198 | 191 | 3 | 11 | | | | | 0 | | | | | |
| 197 | 209 | 210 | 198 | 3 | 11 | | | | | 0 | | | | | |
| 192 | 191 | 193 | 194 | 3 | 11 | | | | | 0 | | | | | |
| 191 | 198 | 199 | 193 | 3 | 11 | | | | | 0 | | | | | |

D11

HCS 90 – 062

| 1–5 | 6–10 | 11–15 | 16–20 | 21–25 | 26–30 | 31–35 | 36–40 | 41–45 | 46–50 | 51–55 | 56–60 | 61–65 | 66–70 | 71–75 | 76–80 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 193 | 199 | 200 | 194 | 3 | 11 | | | | | 0 | | | | | |
| 198 | 210 | 211 | 199 | 3 | 11 | | | 1 | 1 | 0 | | | | | |
| 220 | 241 | 242 | 221 | 3 | 12 | 5 | 21 | | | 0 | | | | | |
| 346 | 359 | 360 | 347 | 3 | 12 | | | | | 0 | | | | | |
| 359 | 370 | 371 | 360 | 3 | 12 | 1 | 11 | | | 0 | | | | | |
| 392 | 405 | 382 | 381 | 3 | 12 | | | | | 0 | | | | | |
| 3 | | | | | | | | | | | | | | | |
| 2 | 1 | | | | | | | | | 5 | 1 | | | | |
| 1 | 1 | | | 1 | | | | | | 43 | 7 | | | | |
| 52 | 1 | | | 1 | | | | | | 169 | 9 | | | | |
| 180 | 1 | | | 1 | | | | | | 348 | 21 | | | | |
| 361 | | | | 1 | | | 37.07926 | | | 400 | 13 | | | | |
| 406 | | | | 1 | | | 37.07926 | | | | | | | | |
| 412 | | | | 0 | -123750 | | | | | | | | | | |
| 411 | | | | | -83710 | | | | | | | | | | |
| 410 | | | | | -44390 | | | | | | | | | | |
| 405 | | | | | -7940 | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | |



HCS 90 – 062

# INPUT DATA DESCRIPTION

REINFORCED EARTH PROJECT 39 STA 551+75

NUMBER OF CONSTRUCTION INCREMENTS = 12

PROPERTIES FOR MATERIAL 1 ********

DENSITY = 0.0

PROPERTIES ARE OVERBURDEN DEPENDENT

MODULUS VS CONFINING PRESSURE - A(INTERCEPT)= 0.1000E 07
B(SLOPE)= 0.7370E 03

FRICTION ANGLE= 0.4000E 02
COHESION= 0.9000E 03
POISSONS RATIO= 0.3000E 00

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PROPERTIES FOR MATERIAL  2   ********

      DENSITY =     0.0

      PROPERTIES ARE OVERBURDEN DEPENDENT

                MODULUS VS CONFINING PRESSURE - A(INTERCEPT)= 0.5550E 06
                                                B(SLOPE)= 0.1680E 03
                FRICTION ANGLE= 0.4000E 02
                COHESION= 0.5000E 00
                POISSONS RATIO= 0.3000E 00


PROPERTIES FOR MATERIAL  3   ********

      DENSITY =     1.43000E 02

      PROPERTIES ARE OVERBURDEN DEPENDENT

                MODULUS VS CONFINING PRESSURE - A(INTERCEPT)= 0.1000E 07
                                                B(SLOPE)= 0.7370E 03
                FRICTION ANGLE= 0.4000E 02
                COHESION= 0.9000E 03
                POISSONS RATIO= 0.3000E 00


PROPERTIES FOR MATERIAL  4   ********

      DENSITY =     1.43000E 02

  REINFORCED EARTH

      STRIP YOUNGS MODULUS= 0.4104E 10
      STRIP WIDTH= 0.1970E 00
      STRIP THICKNESS= 0.9830E-02
      HORIZONTAL SPACING= 0.1640E 01
      VERTICAL SPACING= 0.8330E 00
      ANGLE= 0.0
      SKIN THICKNESS IF BOUNDARY ELEMENT= 0.1000E-01
    SOIL PROPERTIES

      PROPERTIES ARE OVERBURDEN DEPENDENT

                MODULUS VS CONFINING PRESSURE - A(INTERCEPT)= 0.1440E 07
                                                B(SLOPE)= 0.3350E 03
                FRICTION ANGLE= 0.3950E 02
                COHESION= 0.1000E 04
                POISSONS RATIO= 0.3000E 00
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```
PROPERTIES FOR MATERIAL  5   ********

      DENSITY =     1.43000E 02

 REINFORCED EARTH

      STRIP YOUNGS MODULUS= 0.4104E 10
      STRIP WIDTH= 0.1970E 00
      STRIP THICKNESS= 0.9830E-02
      HORIZONTAL SPACING= 0.3280E 01
      VERTICAL SPACING= 0.8330E 00
      ANGLE= 0.0
      SKIN THICKNESS IF BOUNDARY ELEMENT= 0.1000E-01
    SOIL PROPERTIES

      PROPERTIES ARE OVERBURDEN DEPENDENT

                MODULUS VS CONFINING PRESSURE - A(INTERCEPT)= 0.1440E 07
                                                B(SLOPE)= 0.3350E 03
                FRICTION ANGLE= 0.3950E 02
                COHESION= 0.1000E 04
                POISSONS RATIO= 0.3000E 00


PROPERTIES FOR MATERIAL  6   ********

      DENSITY =     1.43000E 02


 REINFORCED EARTH

      STRIP YOUNGS MODULUS= 0.4104E 10
      STRIP WIDTH= 0.1970E 00
      STRIP THICKNESS= 0.9830E-02
      HORIZONTAL SPACING= 0.4920E 01
      VERTICAL SPACING= 0.8330E 00
      ANGLE= 0.0
      SKIN THICKNESS IF BOUNDARY ELEMENT= 0.1000E-01
    SOIL PROPERTIES

      PROPERTIES ARE OVERBURDEN DEPENDENT

                MODULUS VS CONFINING PRESSURE - A(INTERCEPT)= 0.1440E 07
                                                B(SLOPE)= 0.3350E 03
                FRICTION ANGLE= 0.3950E 02
                COHESION= 0.1000E 04
                POISSONS RATIO= 0.3000E 00
```

| NODAL POINT | X COORDINATE | Y COORDINATE | NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|---|---|---|
| 1 | 0.0 | 50.00 | 38 | 125.00 | 146.67 |
| 2 | 0.0 | 95.00 | 39 | 122.00 | 155.00 |
| 3 | 0.0 | 140.00 | 40 | 113.67 | 176.00 |
| 4 | 0.0 | 150.00 | 41 | 104.78 | 196.73 |
| 5 | 0.0 | 178.00 | 42 | 97.00 | 218.00 |
| 6 | 0.0 | 164.00 | 43 | 200.00 | 50.00 |
| 7 | 0.0 | 171.00 | 44 | 170.67 | 101.68 |
| 8 | 33.33 | 50.00 | 45 | 148.00 | 150.00 |
| 9 | 29.80 | 95.03 | 46 | 139.50 | 167.50 |
| 10 | 26.33 | 140.00 | 47 | 131.00 | 185.00 |
| 11 | 27.00 | 150.00 | 48 | 121.00 | 205.50 |
| 12 | 26.33 | 162.67 | 49 | 111.00 | 226.00 |
| 13 | 25.00 | 188.00 | 50 | 116.00 | 215.75 |
| 14 | 25.66 | 175.33 | 51 | 113.50 | 220.88 |
| 15 | 66.67 | 50.00 | 52 | 215.07 | 61.20 |
| 16 | 59.52 | 95.14 | 53 | 189.79 | 107.92 |
| 17 | 52.67 | 140.00 | 54 | 166.33 | 153.67 |
| 18 | 60.00 | 150.00 | 55 | 156.29 | 173.30 |
| 19 | 55.00 | 175.00 | 56 | 146.29 | 192.86 |
| 20 | 50.00 | 200.00 | 57 | 135.78 | 213.76 |
| 21 | 52.50 | 187.50 | 58 | 125.27 | 234.67 |
| 22 | 100.00 | 50.00 | 59 | 140.53 | 202.39 |
| 23 | 88.96 | 95.51 | 60 | 132.90 | 218.5[illegible] |
| 24 | 79.00 | 140.00 | 61 | 230.13 | 72.4[illegible] |
| 25 | 75.00 | 160.00 | 62 | 207.08 | 115.14 |
| 26 | 70.61 | 180.61 | 63 | 184.67 | 157.33 |
| 27 | 65.00 | 200.00 | 64 | 173.04 | 179.18 |
| 28 | 71.00 | 175.00 | 65 | 161.57 | 200.71 |
| 29 | 133.33 | 50.00 | 66 | 150.55 | 222.02 |
| 30 | 117.30 | 96.92 | 67 | 139.53 | 243.33 |
| 31 | 102.00 | 143.33 | 68 | 155.93 | 209.69 |
| 32 | 94.40 | 165.40 | 69 | 147.73 | 226.51 |
| 33 | 87.45 | 187.44 | 70 | 245.20 | 83.60 |
| 34 | 80.00 | 207.00 | 71 | 223.72 | 122.91 |
| 35 | 89.10 | 180.68 | 72 | 203.00 | 161.00 |
| 36 | 166.67 | 50.00 | 73 | 189.62 | 185.36 |
| 37 | 144.91 | 98.82 | 74 | 176.86 | 208.57 |

| NODAL POINT | X COORDINATE | Y COORDINATE | NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|---|---|---|
| 75 | 165.33 | 230.29 | 112 | 219.93 | 271.13 |
| 76 | 153.80 | 252.00 | 113 | 210.90 | 286.70 |
| 77 | 171.05 | 217.65 | 114 | 215.42 | 278.92 |
| 78 | 162.42 | 234.82 | 115 | 320.53 | 139.60 |
| 79 | 260.27 | 94.80 | 116 | 302.14 | 169.55 |
| 80 | 239.61 | 131.90 | 117 | 283.83 | 199.33 |
| 81 | 219.17 | 168.67 | 118 | 268.10 | 224.48 |
| 82 | 205.57 | 192.71 | 119 | 252.38 | 249.63 |
| 83 | 192.14 | 216.43 | 120 | 243.31 | 264.85 |
| 84 | 180.10 | 238.55 | 121 | 234.23 | 280.09 |
| 85 | 168.07 | 260.67 | 122 | 225.13 | 295.33 |
| 86 | 185.88 | 226.13 | 123 | 240.72 | 269.34 |
| 87 | 176.97 | 243.40 | 124 | 335.60 | 150.80 |
| 88 | 275.33 | 106.00 | 125 | 317.63 | 179.21 |
| 89 | 255.30 | 141.21 | 126 | 300.00 | 207.00 |
| 90 | 235.33 | 176.33 | 127 | 287.39 | 226.85 |
| 91 | 221.35 | 200.37 | 128 | 274.78 | 246.71 |
| 92 | 207.43 | 224.29 | 129 | 266.75 | 259.25 |
| 93 | 194.88 | 246.81 | 130 | 257.65 | 274.14 |
| 94 | 182.33 | 269.33 | 131 | 248.54 | 289.05 |
| 95 | 200.71 | 234.62 | 132 | 239.40 | 304.00 |
| 96 | 191.52 | 251.97 | 133 | 350.66 | 162.00 |
| 97 | 290.40 | 117.20 | 134 | 332.78 | 189.50 |
| 98 | 270.94 | 150.62 | 135 | 315.00 | 216.83 |
| 99 | 251.50 | 184.00 | 136 | 302.16 | 236.63 |
| 100 | 237.07 | 208.14 | 137 | 289.32 | 256.42 |
| 101 | 222.71 | 232.14 | 138 | 281.13 | 268.88 |
| 102 | 209.65 | 255.07 | 139 | 272.00 | 283.43 |
| 103 | 196.60 | 278.00 | 140 | 262.84 | 298.03 |
| 104 | 203.13 | 266.53 | 141 | 253.66 | 312.66 |
| 105 | 199.86 | 272.27 | 142 | 365.73 | 173.20 |
| 106 | 305.46 | 128.40 | 143 | 347.85 | 199.95 |
| 107 | 286.55 | 160.06 | 144 | 330.00 | 226.67 |
| 108 | 267.67 | 191.67 | 145 | 316.92 | 246.40 |
| 109 | 252.71 | 216.07 | 146 | 303.85 | 266.14 |
| 110 | 238.00 | 240.00 | 147 | 295.50 | 278.50 |
| 111 | 228.97 | 255.57 | 148 | 286.33 | 292.74 |

| NODAL POINT | X COORDINATE | Y COORDINATE | NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|---|---|---|
| 149 | 277.14 | 307.02 | 186 | 346.00 | 326.75 |
| 150 | 267.93 | 321.33 | 187 | 339.00 | 336.50 |
| 151 | 380.80 | 184.40 | 188 | 332.00 | 346.25 |
| 152 | 362.87 | 210.44 | 189 | 325.00 | 356.00 |
| 153 | 345.00 | 236.50 | 190 | 338.00 | 356.00 |
| 154 | 331.68 | 256.17 | 191 | 338.00 | 360.00 |
| 155 | 318.39 | 275.85 | 192 | 332.00 | 360.00 |
| 156 | 309.88 | 288.13 | 193 | 343.00 | 364.00 |
| 157 | 300.67 | 302.05 | 194 | 342.00 | 365.50 |
| 158 | 291.44 | 316.01 | 195 | 347.00 | 338.50 |
| 159 | 282.19 | 329.99 | 196 | 347.00 | 346.50 |
| 160 | 395.86 | 195.60 | 197 | 347.00 | 356.00 |
| 161 | 377.83 | 220.92 | 198 | 347.00 | 360.00 |
| 162 | 360.00 | 246.34 | 199 | 350.00 | 365.00 |
| 163 | 346.41 | 265.94 | 200 | 350.00 | 370.00 |
| 164 | 332.92 | 285.57 | 201 | 436.44 | 225.81 |
| 165 | 324.25 | 297.75 | 202 | 418.05 | 249.83 |
| 166 | 315.00 | 311.37 | 203 | 400.38 | 274.22 |
| 167 | 305.74 | 325.01 | 204 | 386.05 | 293.36 |
| 168 | 296.46 | 338.66 | 205 | 372.69 | 312.88 |
| 169 | 410.93 | 206.80 | 206 | 364.13 | 324.50 |
| 170 | 392.61 | 231.29 | 207 | 360.00 | 338.50 |
| 171 | 375.00 | 256.17 | 208 | 360.00 | 346.50 |
| 172 | 361.05 | 275.70 | 209 | 360.00 | 356.00 |
| 173 | 347.46 | 295.28 | 210 | 360.00 | 360.00 |
| 174 | 340.00 | 340.00 | 211 | 360.00 | 365.00 |
| 175 | 338.00 | 346.50 | 212 | 360.00 | 370.00 |
| 176 | 338.63 | 307.38 | 213 | 360.00 | 373.00 |
| 177 | 329.33 | 320.70 | 214 | 360.00 | 377.00 |
| 178 | 320.03 | 334.01 | 215 | 360.00 | 381.00 |
| 179 | 310.73 | 347.33 | 216 | 360.00 | 385.00 |
| 180 | 426.00 | 218.00 | 217 | 360.00 | 388.00 |
| 181 | 406.66 | 241.28 | 218 | 360.00 | 393.50 |
| 182 | 390.00 | 266.00 | 219 | 360.00 | 399.00 |
| 183 | 375.34 | 285.41 | 220 | 360.00 | 404.50 |
| 184 | 362.00 | 305.00 | 221 | 363.71 | 410.00 |
| 185 | 353.00 | 317.00 | 222 | 446.88 | 233.63 |

| NODAL POINT | X COORDINATE | Y COORDINATE | NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|---|---|---|
| 223 | 428.72 | 257.99 | 260 | 383.00 | 393.50 |
| 224 | 410.75 | 282.45 | 261 | 383.00 | 399.00 |
| 225 | 396.75 | 301.31 | 262 | 383.00 | 404.50 |
| 226 | 383.38 | 320.75 | 263 | 383.00 | 410.00 |
| 227 | 375.25 | 332.00 | 264 | 467.75 | 249.25 |
| 228 | 371.00 | 338.50 | 265 | 449.62 | 274.07 |
| 229 | 371.00 | 346.50 | 266 | 431.50 | 298.90 |
| 230 | 371.00 | 356.00 | 267 | 418.17 | 317.20 |
| 231 | 371.00 | 360.00 | 268 | 404.75 | 336.50 |
| 232 | 371.00 | 365.00 | 269 | 397.50 | 347.00 |
| 233 | 371.00 | 370.00 | 270 | 401.13 | 341.75 |
| 234 | 371.00 | 373.00 | 271 | 399.31 | 344.38 |
| 235 | 371.00 | 377.00 | 272 | 395.00 | 356.00 |
| 236 | 371.00 | 381.00 | 273 | 395.00 | 360.00 |
| 237 | 371.00 | 385.00 | 274 | 395.00 | 365.00 |
| 238 | 371.00 | 388.00 | 275 | 395.00 | 370.00 |
| 239 | 371.00 | 393.50 | 276 | 395.00 | 373.00 |
| 240 | 371.00 | 399.00 | 277 | 395.00 | 377.00 |
| 241 | 371.00 | 404.50 | 278 | 395.00 | 381.00 |
| 242 | 371.00 | 410.00 | 279 | 395.00 | 385.00 |
| 243 | 457.31 | 241.44 | 280 | 395.00 | 388.00 |
| 244 | 439.19 | 266.04 | 281 | 395.00 | 393.50 |
| 245 | 421.13 | 290.67 | 282 | 395.00 | 399.00 |
| 246 | 407.46 | 309.26 | 283 | 395.00 | 404.50 |
| 247 | 394.06 | 328.63 | 284 | 395.00 | 410.00 |
| 248 | 386.38 | 339.50 | 285 | 478.19 | 257.06 |
| 249 | 380.00 | 341.00 | 286 | 460.04 | 282.10 |
| 250 | 383.00 | 346.50 | 287 | 441.88 | 307.12 |
| 251 | 383.00 | 356.00 | 288 | 428.88 | 325.15 |
| 252 | 383.00 | 360.00 | 289 | 415.44 | 344.38 |
| 253 | 383.00 | 365.00 | 290 | 408.63 | 354.50 |
| 254 | 383.00 | 370.00 | 291 | 406.00 | 356.00 |
| 255 | 383.00 | 373.00 | 292 | 407.31 | 355.25 |
| 256 | 383.00 | 377.00 | 293 | 406.66 | 355.63 |
| 257 | 383.00 | 381.00 | 294 | 406.00 | 360.00 |
| 258 | 383.00 | 385.00 | 295 | 406.00 | 365.00 |
| 259 | 383.00 | 388.00 | 296 | 406.00 | 370.00 |

| NODAL POINT | X COORDINATE | Y COORDINATE | NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|---|---|---|
| 297 | 406.00 | 373.00 | 334 | 432.36 | 367.16 |
| 298 | 406.00 | 377.00 | 335 | 433.10 | 365.98 |
| 299 | 406.00 | 381.00 | 336 | 432.73 | 366.57 |
| 300 | 406.00 | 385.00 | 337 | 432.92 | 366.28 |
| 301 | 406.00 | 388.00 | 338 | 432.82 | 366.42 |
| 302 | 406.00 | 393.50 | 339 | 427.00 | 373.00 |
| 303 | 406.00 | 399.00 | 340 | 432.00 | 377.00 |
| 304 | 406.00 | 404.50 | 341 | 429.00 | 381.00 |
| 305 | 406.00 | 410.00 | 342 | 429.00 | 385.00 |
| 306 | 488.63 | 264.88 | 343 | 429.00 | 389.00 |
| 307 | 470.49 | 290.15 | 344 | 429.00 | 393.50 |
| 308 | 452.25 | 315.35 | 345 | 429.00 | 399.00 |
| 309 | 439.58 | 333.10 | 346 | 429.00 | 404.50 |
| 310 | 426.13 | 352.25 | 347 | 429.00 | 410.00 |
| 311 | 419.75 | 362.00 | 348 | 509.50 | 280.50 |
| 312 | 422.94 | 357.13 | 349 | 492.04 | 306.68 |
| 313 | 421.34 | 359.56 | 350 | 473.00 | 331.80 |
| 314 | 422.14 | 358.34 | 351 | 461.00 | 349.00 |
| 315 | 421.74 | 358.95 | 352 | 447.50 | 368.00 |
| 316 | 413.00 | 365.00 | 353 | 442.00 | 377.00 |
| 317 | 419.00 | 369.00 | 354 | 440.00 | 381.00 |
| 318 | 417.00 | 373.00 | 355 | 446.00 | 385.00 |
| 319 | 417.00 | 377.00 | 356 | 441.00 | 389.00 |
| 320 | 417.00 | 381.00 | 357 | 441.00 | 393.50 |
| 321 | 417.00 | 385.00 | 358 | 441.00 | 399.00 |
| 322 | 417.00 | 388.00 | 359 | 441.00 | 404.50 |
| 323 | 417.00 | 393.50 | | | |
| 324 | 417.00 | 399.00 | | | |
| 325 | 417.00 | 404.50 | | | |
| 326 | 417.00 | 410.00 | | | |
| 327 | 499.06 | 272.69 | | | |
| 328 | 481.05 | 298.27 | | | |
| 329 | 462.63 | 323.57 | | | |
| 330 | 450.29 | 341.05 | | | |
| 331 | 436.81 | 360.13 | | | |
| 332 | 430.88 | 369.50 | | | |
| 333 | 433.84 | 364.81 | | | |

| NODAL POINT | X COORDINATE | Y COORDINATE | NODAL POINT | X COORDINATE | Y COORDINATE |
|---|---|---|---|---|---|
| 360 | 441.00 | 410.00 | 386 | 470.00 | 408.28 |
| 361 | 522.63 | 290.42 | 387 | 548.88 | 310.26 |
| 362 | 504.59 | 316.15 | 388 | 530.72 | 335.71 |
| 363 | 486.13 | 341.60 | 389 | 512.38 | 361.20 |
| 364 | 474.00 | 358.50 | 390 | 500.00 | 377.50 |
| 365 | 459.50 | 377.50 | 391 | 483.50 | 396.50 |
| 366 | 454.00 | 385.25 | 392 | 478.00 | 401.75 |
| 367 | 450.00 | 389.00 | 393 | 480.75 | 399.13 |
| 368 | 455.00 | 393.50 | 394 | 479.38 | 400.44 |
| 369 | 455.00 | 399.00 | 395 | 480.06 | 399.78 |
| 370 | 455.00 | 404.50 | 396 | 479.72 | 400.11 |
| 371 | 455.00 | 410.00 | 397 | 479.89 | 399.95 |
| 372 | 455.00 | 407.25 | 398 | 479.80 | 400.03 |
| 373 | 455.00 | 408.62 | 399 | 479.85 | 399.99 |
| 374 | 535.75 | 300.34 | 400 | 562.00 | 320.17 |
| 375 | 517.58 | 325.90 | 401 | 544.05 | 345.47 |
| 376 | 499.25 | 351.40 | 402 | 525.50 | 371.00 |
| 377 | 487.00 | 368.00 | 403 | 513.00 | 387.00 |
| 378 | 471.50 | 387.00 | 404 | 495.50 | 406.00 |
| 379 | 466.00 | 393.50 | 405 | 490.00 | 410.00 |
| 380 | 465.00 | 399.00 | 406 | 575.00 | 330.00 |
| 381 | 470.00 | 404.50 | 407 | 558.00 | 355.00 |
| 382 | 470.00 | 410.00 | 408 | 540.00 | 381.00 |
| 383 | 470.00 | 407.25 | 409 | 528.00 | 399.00 |
| 384 | 470.00 | 408.63 | 410 | 520.00 | 410.00 |
| 385 | 470.00 | 407.94 | 411 | 547.50 | 410.00 |
| | | | 412 | 575.00 | 410.00 |
| | | | 413 | 575.00 | 367.00 |

| ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. | ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 1 | 8 | 9 | 2 | 1 | 1 | 38 | 161 | 162 | 153 | 152 | 1 | 1 |
| 2 | 9 | 10 | 3 | 2 | 1 | 1 | 39 | 169 | 170 | 161 | 160 | 1 | 1 |
| 3 | 8 | 15 | 16 | 9 | 1 | 1 | 40 | 170 | 171 | 162 | 161 | 1 | 1 |
| 4 | 16 | 17 | 10 | 9 | 1 | 1 | 41 | 180 | 181 | 170 | 169 | 1 | 1 |
| 5 | 15 | 22 | 23 | 16 | 1 | 1 | 42 | 170 | 181 | 182 | 171 | 1 | 1 |
| 6 | 23 | 24 | 17 | 16 | 1 | 1 | 43 | 201 | 202 | 181 | 180 | 1 | 1 |
| 7 | 22 | 29 | 30 | 23 | 1 | 1 | 44 | 181 | 202 | 203 | 182 | 1 | 1 |
| 8 | 23 | 30 | 31 | 24 | 1 | 1 | 45 | 222 | 223 | 202 | 201 | 1 | 1 |
| 9 | 29 | 36 | 37 | 30 | 1 | 1 | 46 | 202 | 223 | 224 | 203 | 1 | 1 |
| 10 | 30 | 37 | 38 | 31 | 1 | 1 | 47 | 243 | 244 | 223 | 222 | 1 | 1 |
| 11 | 36 | 43 | 44 | 37 | 1 | 1 | 48 | 223 | 244 | 245 | 224 | 1 | 1 |
| 12 | 37 | 44 | 45 | 38 | 1 | 1 | 49 | 264 | 265 | 244 | 243 | 1 | 1 |
| 13 | 43 | 52 | 53 | 44 | 1 | 1 | 50 | 265 | 266 | 245 | 244 | 1 | 1 |
| 14 | 53 | 54 | 45 | 44 | 1 | 1 | 51 | 285 | 286 | 265 | 264 | 1 | 1 |
| 15 | 52 | 61 | 62 | 53 | 1 | 1 | 52 | 286 | 287 | 266 | 265 | 1 | 1 |
| 16 | 62 | 63 | 54 | 53 | 1 | 1 | 53 | 306 | 307 | 286 | 285 | 1 | 1 |
| 17 | 70 | 71 | 62 | 61 | 1 | 1 | 54 | 307 | 308 | 287 | 286 | 1 | 1 |
| 18 | 71 | 72 | 63 | 62 | 1 | 1 | 55 | 327 | 328 | 307 | 306 | 1 | 1 |
| 19 | 79 | 80 | 71 | 70 | 1 | 1 | 56 | 307 | 328 | 329 | 308 | 1 | 1 |
| 20 | 80 | 81 | 72 | 71 | 1 | 1 | 57 | 348 | 349 | 328 | 327 | 1 | 1 |
| 21 | 88 | 89 | 80 | 79 | 1 | 1 | 58 | 328 | 349 | 350 | 329 | 1 | 1 |
| 22 | 89 | 90 | 81 | 80 | 1 | 1 | 59 | 361 | 362 | 349 | 348 | 1 | 1 |
| 23 | 97 | 98 | 89 | 88 | 1 | 1 | 60 | 349 | 362 | 363 | 350 | 1 | 1 |
| 24 | 98 | 99 | 90 | 89 | 1 | 1 | 61 | 374 | 375 | 362 | 361 | 1 | 1 |
| 25 | 106 | 107 | 98 | 97 | 1 | 1 | 62 | 362 | 375 | 376 | 363 | 1 | 1 |
| 26 | 107 | 108 | 99 | 98 | 1 | 1 | 63 | 387 | 388 | 375 | 374 | 1 | 1 |
| 27 | 115 | 116 | 107 | 106 | 1 | 1 | 64 | 375 | 388 | 389 | 376 | 1 | 1 |
| 28 | 116 | 117 | 108 | 107 | 1 | 1 | 65 | 387 | 400 | 401 | 388 | 1 | 1 |
| 29 | 124 | 125 | 116 | 115 | 1 | 1 | 66 | 388 | 401 | 402 | 389 | 1 | 1 |
| 30 | 125 | 126 | 117 | 116 | 1 | 1 | 67 | 400 | 406 | 407 | 401 | 1 | 1 |
| 31 | 133 | 134 | 125 | 124 | 1 | 1 | 68 | 407 | 408 | 402 | 401 | 1 | 1 |
| 32 | 134 | 135 | 126 | 125 | 1 | 1 | 69 | 406 | 413 | 407 | 407 | 1 | 1 |
| 33 | 142 | 143 | 134 | 133 | 1 | 1 | 70 | 413 | 412 | 408 | 407 | 1 | 1 |
| 34 | 143 | 144 | 135 | 134 | 1 | 1 | 71 | 3 | 10 | 11 | 4 | 2 | 1 |
| 35 | 151 | 152 | 143 | 142 | 1 | 1 | 72 | 10 | 17 | 18 | 11 | 2 | 1 |
| 36 | 152 | 153 | 144 | 143 | 1 | 1 | 73 | 17 | 24 | 25 | 18 | 2 | 1 |
| 37 | 160 | 161 | 152 | 151 | 1 | 1 | 74 | 24 | 31 | 32 | 25 | 2 | 1 |

| ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. | ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 75 | 31 | 38 | 39 | 39 | 2 | 1 | 112 | 164 | 173 | 176 | 165 | 2 | 1 |
| 76 | 39 | 40 | 32 | 31 | 2 | 1 | 113 | 171 | 182 | 183 | 172 | 2 | 1 |
| 77 | 38 | 45 | 46 | 39 | 2 | 1 | 114 | 172 | 183 | 184 | 173 | 2 | 1 |
| 78 | 46 | 47 | 40 | 39 | 2 | 1 | 115 | 184 | 185 | 176 | 173 | 2 | 1 |
| 79 | 45 | 54 | 55 | 46 | 2 | 1 | 116 | 182 | 203 | 204 | 183 | 2 | 1 |
| 80 | 46 | 55 | 56 | 47 | 2 | 1 | 117 | 204 | 205 | 184 | 183 | 2 | 1 |
| 81 | 54 | 63 | 64 | 55 | 2 | 1 | 118 | 184 | 205 | 206 | 185 | 2 | 1 |
| 82 | 55 | 64 | 65 | 56 | 2 | 1 | 119 | 203 | 224 | 225 | 204 | 2 | 1 |
| 83 | 63 | 72 | 73 | 64 | 2 | 1 | 120 | 225 | 226 | 205 | 204 | 2 | 1 |
| 84 | 64 | 73 | 74 | 65 | 2 | 1 | 121 | 205 | 226 | 227 | 206 | 2 | 1 |
| 85 | 81 | 82 | 73 | 72 | 2 | 1 | 122 | 224 | 245 | 246 | 225 | 2 | 1 |
| 86 | 73 | 82 | 83 | 74 | 2 | 1 | 123 | 225 | 246 | 247 | 226 | 2 | 1 |
| 87 | 81 | 90 | 91 | 82 | 2 | 1 | 124 | 226 | 247 | 248 | 227 | 2 | 1 |
| 88 | 82 | 91 | 92 | 83 | 2 | 1 | 125 | 245 | 266 | 267 | 246 | 2 | 1 |
| 89 | 90 | 99 | 100 | 91 | 2 | 1 | 126 | 246 | 267 | 268 | 247 | 2 | 1 |
| 90 | 91 | 100 | 101 | 92 | 2 | 1 | 127 | 247 | 268 | 269 | 248 | 2 | 1 |
| 91 | 99 | 108 | 109 | 100 | 2 | 1 | 128 | 266 | 287 | 288 | 267 | 2 | 1 |
| 92 | 100 | 109 | 110 | 101 | 2 | 1 | 129 | 288 | 289 | 268 | 267 | 2 | 1 |
| 93 | 108 | 117 | 118 | 109 | 2 | 1 | 130 | 268 | 289 | 290 | 269 | 2 | 1 |
| 94 | 109 | 118 | 119 | 110 | 2 | 1 | 131 | 287 | 308 | 309 | 288 | 2 | 1 |
| 95 | 126 | 127 | 118 | 117 | 2 | 1 | 132 | 288 | 309 | 310 | 289 | 2 | 1 |
| 96 | 127 | 128 | 119 | 118 | 2 | 1 | 133 | 289 | 310 | 311 | 290 | 2 | 1 |
| 97 | 128 | 129 | 119 | 119 | 2 | 1 | 134 | 308 | 329 | 330 | 309 | 2 | 1 |
| 98 | 126 | 135 | 136 | 127 | 2 | 1 | 135 | 309 | 330 | 331 | 310 | 2 | 1 |
| 99 | 127 | 136 | 137 | 128 | 2 | 1 | 136 | 310 | 331 | 332 | 311 | 2 | 1 |
| 100 | 128 | 137 | 138 | 129 | 2 | 1 | 137 | 329 | 350 | 351 | 330 | 2 | 1 |
| 101 | 135 | 144 | 145 | 136 | 2 | 1 | 138 | 330 | 351 | 352 | 331 | 2 | 1 |
| 102 | 136 | 145 | 146 | 137 | 2 | 1 | 139 | 331 | 352 | 353 | 332 | 2 | 1 |
| 103 | 137 | 146 | 147 | 138 | 2 | 1 | 140 | 363 | 364 | 351 | 350 | 2 | 1 |
| 104 | 144 | 153 | 154 | 145 | 2 | 1 | 141 | 351 | 364 | 365 | 352 | 2 | 1 |
| 105 | 145 | 154 | 155 | 146 | 2 | 1 | 142 | 365 | 366 | 353 | 352 | 2 | 1 |
| 106 | 146 | 155 | 156 | 147 | 2 | 1 | 143 | 376 | 377 | 364 | 363 | 2 | 1 |
| 107 | 153 | 162 | 163 | 154 | 2 | 1 | 144 | 364 | 377 | 378 | 365 | 2 | 1 |
| 108 | 154 | 163 | 164 | 155 | 2 | 1 | 145 | 378 | 379 | 366 | 365 | 2 | 1 |
| 109 | 155 | 164 | 165 | 156 | 2 | 1 | 146 | 389 | 390 | 377 | 376 | 2 | 1 |
| 110 | 162 | 171 | 172 | 163 | 2 | 1 | 147 | 377 | 390 | 391 | 378 | 2 | 1 |
| 111 | 163 | 172 | 173 | 164 | 2 | 1 | 148 | 391 | 392 | 379 | 378 | 2 | 1 |

| ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. | ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 149 | 402 | 403 | 390 | 389 | 2 | 1 | 186 | 121 | 122 | 113 | 112 | 3 | 2 |
| 150 | 390 | 403 | 404 | 391 | 2 | 1 | 187 | 129 | 130 | 120 | 119 | 3 | 2 |
| 151 | 404 | 405 | 392 | 391 | 2 | 1 | 188 | 130 | 131 | 121 | 120 | 3 | 2 |
| 152 | 408 | 409 | 403 | 402 | 2 | 1 | 189 | 131 | 132 | 122 | 121 | 3 | 2 |
| 153 | 403 | 409 | 410 | 404 | 2 | 1 | 190 | 138 | 139 | 130 | 129 | 3 | 2 |
| 154 | 404 | 410 | 405 | 405 | 2 | 1 | 191 | 139 | 140 | 131 | 130 | 3 | 2 |
| 155 | 412 | 411 | 409 | 408 | 2 | 1 | 192 | 140 | 141 | 132 | 131 | 3 | 2 |
| 156 | 409 | 411 | 410 | 410 | 2 | 1 | 193 | 147 | 148 | 139 | 138 | 3 | 2 |
| 157 | 4 | 11 | 12 | 12 | 3 | 2 | 194 | 148 | 149 | 140 | 139 | 3 | 2 |
| 158 | 12 | 13 | 5 | 4 | 3 | 2 | 195 | 149 | 150 | 141 | 140 | 3 | 2 |
| 159 | 11 | 18 | 19 | 12 | 3 | 2 | 196 | 156 | 157 | 148 | 147 | 3 | 2 |
| 160 | 12 | 19 | 20 | 13 | 3 | 2 | 197 | 157 | 158 | 149 | 148 | 3 | 2 |
| 161 | 25 | 26 | 19 | 18 | 3 | 2 | 198 | 158 | 159 | 150 | 149 | 3 | 2 |
| 162 | 26 | 27 | 20 | 19 | 3 | 2 | 199 | 165 | 166 | 157 | 156 | 3 | 2 |
| 163 | 25 | 32 | 33 | 26 | 3 | 2 | 200 | 166 | 167 | 158 | 157 | 3 | 2 |
| 164 | 26 | 33 | 34 | 27 | 3 | 2 | 201 | 167 | 168 | 159 | 158 | 3 | 2 |
| 165 | 40 | 41 | 33 | 32 | 3 | 2 | 202 | 176 | 177 | 166 | 165 | 3 | 2 |
| 166 | 41 | 42 | 34 | 33 | 3 | 2 | 203 | 177 | 178 | 167 | 166 | 3 | 2 |
| 167 | 40 | 47 | 48 | 41 | 3 | 2 | 204 | 178 | 179 | 168 | 167 | 3 | 2 |
| 168 | 41 | 48 | 49 | 42 | 3 | 2 | 205 | 176 | 185 | 186 | 186 | 3 | 2 |
| 169 | 47 | 56 | 57 | 48 | 3 | 2 | 206 | 186 | 187 | 177 | 176 | 3 | 2 |
| 170 | 48 | 57 | 58 | 49 | 3 | 2 | 207 | 187 | 188 | 178 | 177 | 3 | 2 |
| 171 | 56 | 65 | 66 | 57 | 3 | 2 | 208 | 188 | 189 | 179 | 178 | 3 | 2 |
| 172 | 57 | 66 | 67 | 58 | 3 | 2 | 209 | 185 | 206 | 186 | 186 | 3 | 2 |
| 173 | 65 | 74 | 75 | 66 | 3 | 2 | 210 | 195 | 174 | 187 | 186 | 3 | 2 |
| 174 | 66 | 75 | 76 | 67 | 3 | 2 | 211 | 186 | 206 | 207 | 195 | 3 | 2 |
| 175 | 74 | 83 | 84 | 75 | 3 | 2 | 212 | 227 | 228 | 207 | 206 | 3 | 2 |
| 176 | 75 | 84 | 85 | 76 | 3 | 2 | 213 | 248 | 249 | 228 | 227 | 3 | 2 |
| 177 | 83 | 92 | 93 | 84 | 3 | 2 | 214 | 187 | 174 | 175 | 188 | 3 | 2 |
| 178 | 84 | 93 | 94 | 85 | 3 | 2 | 215 | 195 | 196 | 175 | 174 | 3 | 2 |
| 179 | 92 | 101 | 102 | 93 | 3 | 2 | 216 | 195 | 207 | 208 | 196 | 3 | 2 |
| 180 | 93 | 102 | 103 | 94 | 3 | 2 | 217 | 207 | 228 | 229 | 208 | 3 | 2 |
| 181 | 110 | 111 | 102 | 101 | 3 | 2 | 218 | 228 | 249 | 250 | 229 | 3 | 2 |
| 182 | 111 | 112 | 103 | 102 | 3 | 2 | 219 | 248 | 269 | 250 | 249 | 3 | 2 |
| 183 | 112 | 113 | 103 | 103 | 3 | 2 | 220 | 188 | 175 | 190 | 189 | 3 | 2 |
| 184 | 119 | 120 | 111 | 110 | 3 | 2 | 221 | 175 | 196 | 197 | 190 | 3 | 2 |
| 185 | 120 | 121 | 112 | 111 | 3 | 2 | 222 | 196 | 208 | 209 | 197 | 3 | 2 |

| ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. | ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 223 | 208 | 229 | 230 | 209 | 3 | 2 | 257 | 297 | 318 | 319 | 298 | 3 | 7 |
| 224 | 229 | 250 | 251 | 230 | 3 | 2 | 258 | 298 | 319 | 320 | 299 | 3 | 7 |
| 225 | 269 | 272 | 251 | 250 | 3 | 2 | 259 | 339 | 340 | 319 | 318 | 3 | 7 |
| 226 | 290 | 291 | 272 | 269 | 3 | 2 | 260 | 319 | 340 | 341 | 320 | 3 | 7 |
| 227 | 209 | 230 | 231 | 210 | 4 | 3 | 261 | 332 | 353 | 340 | 339 | 3 | 7 |
| 228 | 230 | 251 | 252 | 231 | 4 | 3 | 262 | 340 | 353 | 354 | 341 | 3 | 7 |
| 229 | 251 | 272 | 273 | 252 | 4 | 3 | 263 | 215 | 236 | 237 | 216 | 5 | 8 |
| 230 | 272 | 291 | 294 | 273 | 4 | 3 | 264 | 216 | 237 | 238 | 217 | 5 | 8 |
| 231 | 290 | 311 | 294 | 291 | 3 | 3 | 265 | 236 | 257 | 258 | 237 | 5 | 8 |
| 232 | 210 | 231 | 232 | 211 | 4 | 4 | 266 | 237 | 258 | 259 | 238 | 5 | 8 |
| 233 | 231 | 252 | 253 | 232 | 4 | 4 | 267 | 257 | 278 | 279 | 258 | 5 | 8 |
| 234 | 252 | 273 | 274 | 253 | 4 | 4 | 268 | 258 | 279 | 280 | 259 | 5 | 8 |
| 235 | 273 | 294 | 295 | 274 | 4 | 4 | 269 | 278 | 299 | 300 | 279 | 5 | 8 |
| 236 | 311 | 316 | 295 | 294 | 3 | 4 | 270 | 279 | 300 | 301 | 280 | 5 | 8 |
| 237 | 211 | 232 | 233 | 212 | 4 | 5 | 271 | 299 | 320 | 321 | 300 | 3 | 8 |
| 238 | 232 | 253 | 254 | 233 | 4 | 5 | 272 | 300 | 321 | 322 | 301 | 3 | 8 |
| 239 | 253 | 274 | 275 | 254 | 4 | 5 | 273 | 320 | 341 | 342 | 321 | 3 | 8 |
| 240 | 274 | 295 | 296 | 275 | 4 | 5 | 274 | 321 | 342 | 343 | 322 | 3 | 8 |
| 241 | 295 | 316 | 317 | 296 | 3 | 5 | 275 | 341 | 354 | 355 | 342 | 3 | 8 |
| 242 | 332 | 317 | 316 | 311 | 3 | 5 | 276 | 342 | 355 | 356 | 343 | 3 | 8 |
| 243 | 212 | 233 | 234 | 213 | 5 | 6 | 277 | 366 | 355 | 354 | 353 | 3 | 8 |
| 244 | 233 | 254 | 255 | 234 | 5 | 6 | 278 | 355 | 366 | 367 | 356 | 3 | 8 |
| 245 | 254 | 275 | 276 | 255 | 5 | 6 | 279 | 217 | 238 | 239 | 218 | 6 | 9 |
| 246 | 275 | 296 | 297 | 276 | 5 | 6 | 280 | 218 | 239 | 240 | 219 | 6 | 9 |
| 247 | 296 | 317 | 318 | 297 | 3 | 6 | 281 | 238 | 259 | 260 | 239 | 6 | 9 |
| 248 | 332 | 339 | 318 | 317 | 3 | 6 | 282 | 239 | 260 | 261 | 240 | 6 | 9 |
| 249 | 213 | 234 | 235 | 214 | 5 | 7 | 283 | 259 | 280 | 281 | 260 | 6 | 9 |
| 250 | 214 | 235 | 236 | 215 | 5 | 7 | 284 | 260 | 281 | 282 | 261 | 6 | 9 |
| 251 | 234 | 255 | 256 | 235 | 5 | 7 | 285 | 280 | 301 | 302 | 281 | 6 | 9 |
| 252 | 235 | 256 | 257 | 236 | 5 | 7 | 286 | 281 | 302 | 303 | 282 | 6 | 9 |
| 253 | 255 | 276 | 277 | 256 | 5 | 7 | 287 | 301 | 322 | 323 | 302 | 3 | 9 |
| 254 | 256 | 277 | 278 | 257 | 5 | 7 | 288 | 302 | 323 | 324 | 303 | 3 | 9 |
| 255 | 276 | 297 | 298 | 277 | 5 | 7 | 289 | 322 | 343 | 344 | 323 | 3 | 9 |
| 256 | 277 | 298 | 299 | 278 | 5 | 7 | 290 | 323 | 344 | 345 | 324 | 3 | 9 |

| ELEM NO. | ELEMENT NODAL POINTS | | | | MAT NO. | CONST INCR. |
|---|---|---|---|---|---|---|
| 291 | 343 | 356 | 357 | 344 | 3 | 9 |
| 292 | 344 | 357 | 358 | 345 | 3 | 9 |
| 293 | 356 | 367 | 368 | 357 | 3 | 9 |
| 294 | 357 | 368 | 369 | 358 | 3 | 9 |
| 295 | 366 | 379 | 368 | 367 | 3 | 9 |
| 296 | 368 | 379 | 380 | 369 | 3 | 9 |
| 297 | 219 | 240 | 241 | 220 | 6 | 10 |
| 298 | 240 | 261 | 262 | 241 | 6 | 10 |
| 299 | 261 | 282 | 283 | 262 | 6 | 10 |
| 300 | 282 | 303 | 304 | 283 | 6 | 10 |
| 301 | 303 | 324 | 325 | 304 | 3 | 10 |
| 302 | 324 | 345 | 346 | 325 | 3 | 10 |
| 303 | 345 | 358 | 359 | 346 | 3 | 10 |
| 304 | 358 | 369 | 370 | 359 | 3 | 10 |
| 305 | 380 | 381 | 370 | 369 | 3 | 10 |
| 306 | 379 | 392 | 381 | 380 | 3 | 10 |
| 307 | 189 | 190 | 191 | 192 | 3 | 11 |
| 308 | 190 | 197 | 198 | 191 | 3 | 11 |
| 309 | 197 | 209 | 210 | 198 | 3 | 11 |
| 310 | 191 | 193 | 194 | 192 | 3 | 11 |
| 311 | 191 | 198 | 199 | 193 | 3 | 11 |
| 312 | 199 | 200 | 194 | 193 | 3 | 11 |
| 313 | 198 | 210 | 211 | 199 | 3 | 11 |
| 314 | 199 | 211 | 212 | 200 | 3 | 11 |
| 315 | 241 | 242 | 221 | 220 | 3 | 12 |
| 316 | 241 | 262 | 263 | 242 | 3 | 12 |
| 317 | 262 | 283 | 284 | 263 | 3 | 12 |
| 318 | 283 | 304 | 305 | 284 | 3 | 12 |
| 319 | 304 | 325 | 326 | 305 | 3 | 12 |
| 320 | 325 | 346 | 347 | 326 | 3 | 12 |
| 321 | 346 | 359 | 360 | 347 | 3 | 12 |
| 322 | 359 | 370 | 371 | 360 | 3 | 12 |
| 323 | 370 | 381 | 382 | 371 | 3 | 12 |
| 324 | 392 | 405 | 382 | 381 | 3 | 12 |

*****BOUNDARY CONDITIONS*****

| BOUNDARY NODE | | | | | | INCREMENT NO. |
|---|---|---|---|---|---|---|
| 2 | U-X= | 0.0 | P-Y= | 0.0 | ANG= 0.0 | 1 |
| 3 | U-X= | 0.0 | P-Y= | 0.0 | ANG= 0.0 | 1 |
| 4 | U-X= | 0.0 | P-Y= | 0.0 | ANG= 0.0 | 1 |
| 5 | U-X= | 0.0 | P-Y= | 0.0 | ANG= 0.0 | 1 |
| 1 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 8 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 15 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 22 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 29 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 36 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 43 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 52 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 61 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 70 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 79 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 88 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 97 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 106 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 115 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |
| 124 | U-X= | 0.0 | U-Y= | 0.0 | ANG= 0.0 | 1 |

| | | | | |
|---|---|---|---|---|
| 133 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 142 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 151 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 160 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 169 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 180 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 201 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 222 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 243 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 264 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 285 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 306 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 327 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 348 | U-X= 0.0 | U-Y= 0.0 | ANG= 0.0 | 1 |
| 361 | P-N= 0.0 | U-S= 0.0 | ANG= 3.71E 01 | 1 |
| 374 | P-N= 0.0 | U-S= 0.0 | ANG= 3.71E 01 | 1 |
| 387 | P-N= 0.0 | U-S= 0.0 | ANG= 3.71E 01 | 1 |
| 400 | P-N= 0.0 | U-S= 0.0 | ANG= 3.71E 01 | 1 |
| 406 | P-N= 0.0 | U-S= 0.0 | ANG= 3.71E 01 | 1 |
| 412 | P-X= 0.0 | P-Y= -1.24E 05 | ANG= 0.0 | 1 |
| 411 | P-X= 0.0 | P-Y= -8.37E 04 | ANG= 0.0 | 1 |
| 410 | P-X= 0.0 | P-Y= -4.44E 04 | ANG= 0.0 | 1 |
| 405 | P-X= 0.0 | P-Y= -7.94E 03 | ANG= 0.0 | 1 |

PROGRAM LISTING

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```
++WRITE PRINT,ENG085A                                                    000191
C          DATA SET ENG085A    AT LEVEL 008 AS OF 01/17/74
      SUBROUTINE   FINEL(PAPSIZ)                                         00001
      COMMON /CNTRL/  WIDTH, INOUT, INCR2,LC1,PGM1,PGM2,PHON             00002
      COMMON  /HDLIN/  HED(18), DUM(2)                                   00003
      COMMON/BLK1/ R(700),Z(700), IX(600,4),IXXX                         00004
      COMMON/BLK2/MNO(600),NODB(200),BIV(200,3),IIFLG(3),BIVD(3)         00005
     1, NUMEL , NUMNP, NUMPC, NINC                                       00006
      DIMENSION   IBUF(1024) ,IPS(5),INS(5),ISYMBL(3),PGMR(3)            00007
      REAL*8 MSG(5)/'END OF P','LOT TAPE',3*' '/ ,DATE/' DATED'  /       00008
      DATA LC /'F132'/,NT/5/,NPLOTS/1/ ,BLANK/' '/,IBLNK/' '/            00009
      REAL*8 PAPER1  /'BLANK'/,PAPER2/'WHITE'/                           00010
      REAL*8 VOL,START   /'ANYWHERE'/  ,NAME/'ENG085'/                   00011
      REAL*4 DOUT(6)/'RETU','RN -',' DIS','TR.1','5 BA','SKET'/          00012
      REAL  MRGN,MRGNT,MPGNB ,NROUND,X(4),Y(4)                           00013
      REAL*4 XSYMB(3,2) / 0.,.05,0.,.04,.08,0./                          00014
      REAL*4  XY (50 ,2)                                                 00015
      DATA  IPS/3,2,2,2,2/,INS/1,2,3,4,1/,ISYMBL/76,18,1/                00016
      DATA PGMR/'TRAN','SP.','LAB.'/,NPEN /3/,VOL/'****'/                00017
      REAL*4  PHON(3),  PHONE(3) / 2* '   -','    '/                    00018
      IF (PAPSIZ .GT.1.0 .AND. PAPSIZ .LT. 30.1) GOTO 51                 00019
   49 CONTINUE                                                           00020
   50 FORMAT( '1  *** IMPROPER PLOT WIDTH =',E16.7,' ***' )              00021
      RETURN                                                             00022
   51 CONTINUE                                                           00023
       INCH = 11                                                         00024
      IF( PAPSIZ .GT. 11.1 )  INCH = 30                                  00025
      WIDTH = INCH                                                       00026
      CALL  PLOTS (IBUF,1024,8)                                          00027
      IF(LC1 .NE. IBLNK) LC=LC1                                          00028
      IF(PGM1 .EQ. BLANK .AND. PGM2 .EQ. BLANK) GOTO 52                  00029
      PGMR(1) = PGM1                                                     00030
      PGMR(2) = PGM2                                                     00031
      PGMR(3) =  BLANK                                                   00032
   52 CONTINUE                                                           00033
      IF (PHON(1) .NE. BLANK)  PHONE(1) = PHON(1)                        00034
      IF (PHON(2) .NE. BLANK)  PHONE(2) = PHON(2)                        00035
      IF (PHON(3) .NE. BLANK)  PHONE(3) = PHON(3)                        00036
C                                                                        00037
      R1 = R(1)                                                          00038
      R2 = R(1)                                                          00039
      Z1 = Z(1)                                                          00040
      Z2 = Z(1)                                                          00041
      DO 100 I=1,NUMNP                                                   00042
```

```
      IF(R(I) .LT. R1)  R1=R(I)
      IF(Z(I) .LT. Z1)  Z1=Z(I)
      IF(R(I) .GT. R2)  R2=R(I)
      IF(Z(I) .GT. Z2)  Z2=Z(I)
  100 CONTINUE
      RR = R2-R1
      ZZ = Z2-Z1
      MRGN = 0.
      NROUND = 1
      DO 60 ITR1 = 1, 7
      SCL1 =        ZZ/(PAPSIZ  - MRGN)
      IF ( SCL1 .LT. 1) GO TO 16
       IF(SCL1 .GT. 19) NROUND = 5
       IF(SCL1 .GT. 99) NROUND = 10
      I = SCL1 / NROUND
      SCL5 = I*NROUND
      IF (SCL5      .LT. SCL1 )  SCL5 = SCL5+NROUND
   16 CONTINUE
      IF (SCL1 .LT. 1)  SCL5 = SCL1
      PAP5 = ZZ / SCL5
      IF ( WIDTH .GT. (PAP5 +2.0)) GOTO 61
      MRGN = MRGN + .70 ** (ITR1-1)
   60 CONTINUE
C     ***************************
      GOTO 49
   61 MRGN =  WIDTH  - PAP5
      MRGNB= MRGN * .61
      MRGNT= MRGN - MRGNB
      FACT =  1. /SCL5
C     INITIALIZE  PEN POSITION  & DRAW  AXES
      CALL PLOT ( 2.5,   -WIDTH ,23)
      CALL PLOT (1.6,MRGNB,23)
      RLEN = RR / SCL5  + 1.
      RLEN  = AINT(RLEN)
      NF = RLEN /12. + 2.00
      CALL  AXIS (0.,0.,6HR-AXIS,-6,RLEN,0.,R1,SCL5)
      IF  (RLEN  .GE.  15.0)
     *CALL  SYMBOL ( 0.0, -.85, .21, HED, 0.,72)
      IF  (RLEN  .LT.  15.0)
     *CALL  SYMBOL ( 0.0, -.75, .14, HED, 0.,72)
      ZLEN = AINT ( ZZ / SCL5 +.51)
      CALL  AXIS (0.,0.,6HZ-AXIS,+6,ZLEN,90.,Z1,SCL5,10.)
C     ***************************
      NP =1
      DO    30  I = 1,NUMEL
      DIV = 0.0
       N1 = 0
      XXX= 0
```

```
      YYY= 0
      NP= NP+1
      DO    20  J = 1,5
      IP  = IPS(J)
      JN =  INS (J)
      N   = IX(I,JN)
      XX  = (R(N)-R1  ) * FACT
      YY  = (Z(N)-Z1  ) * FACT
      CALL PLOT (XX,YY,IP)
      IF( N1.EQ. N)GOTO 20
       N1= N
      IF(J .GT. 4)  GOTO 20
      IF (N .LT. 1 ) GOTO  20
      XXX = XXX+XX
      YYY = YYY+YY
      DIV = DIV+1.0
      X(J) = XX
      Y(J) = YY
   20 CONTINUE
      YYY = YYY/DIV-0.034
      XXX = XXX/DIV-0.07
      IF (NP .GT. 2)  GOTO 34
      CMP = .0334
      IF ( DIV .GT. 3.1) GOTO 25
      CMP=  .061
   25 CONTINUE
      AREA2=X(1)*Y(2)+Y(1)*X(3)+Y(3)*X(2)-Y(2)*X(3)-Y(1)*X(2)-X(1)*Y(3)
      AREA2= ABS(AREA2) / 2.0
      IF (AREA2 .LT. CMP)  GOTO 28
      GOTO  34
   28  CONTINUE
      CALL SYMBOL (XXX+ .03, YYY+.004,.07,14,0.,-1)
      GOTO 30
   34 FPN = I
      YYY = YYY + 0.025
      CALL NUMBER(XXX,YYY,.07,FPN,0., -1)
      NP =    0
   30 CONTINUE
C     ***************************
      CALL SERIAL(VOL,IER)
      DO 40 IN = 1,NUMPC
      I=NODB(IN)/10000
      NB=NODB(IN) - I*10000
      NB4= NB/100
      NB = NB - NB4 * 100
      IF(NB .LT. 1) GOTO 40
      K1    =  11/NB + 9/NB + 2*NB - 20
      IF (K1 .LT. 1 .OR. K1 .GT.  3 )  GO TO 40
```

```
      XX =( R(I)-R1)*FACT -XSYMB(K1,1)
      YY =( Z(I)-Z1)*FACT - XSYMB(K1,2)
      INTEQ = ISYMBL(K1)
 70   FORMAT (4I12,7X,4F16.4)
      CALL SYMBOL (XX, YY, 0.07, INTEQ, 0.0, -1)
      CALL SYMBOL (XX, YY, 0.07, INTEQ, 0.0, -1)

 40   CONTINUE

      N2 = 1
      NXY = 0
      N1  = 1
      DO  97 I=1,NUMNP
      XX = (R(I)-R1)* FACT -0.046
      YY = (Z(I)-Z1)* FACT +0.03
      IF  (I .LT. 2)   GOTO  79
      IF ( NXY .GT. N2 ) N2 = NXY
      DO 77 N = N1,N2
      DIS2 =  (XX - XY(N,1)) **2  +  (YY - XY(N,2)) **2
      IF (DIS2 .LT. 0.064) GOTO 97
 77   CONTINUE
 79   CONTINUE
      FPN = I
      NXY = NXY +1
      CALL NUMBER(XX,YY,.07,FPN,0.,-I)
      IF (NXY .LE. 50 ) GOTO 73
      NXY = 1
 73   CONTINUE
      XY (NXY,1)  = XX
      XY (NXY,2)  = YY
 97   CONTINUE
                                                  END OF NODES
      RR =RR* FACT
      MSG(3)= VOL
      MSG(4)=DATE
      CALL  DHDATE(0,DATE)
      MSG(5)=DATE
      CALL  PLOT (RR+1.5,0., -03)
      ZMSG =0.73 * ZLEN
      CALL SYMBOL (0.0, ZMSG, 0.14, MSG, 270.0, 40)
      CALL PLOT(2.0,0.0,999)
      XX =  NUMNP + NUMEL
      TIME = .021* XX + RLEN * ZLEN / 70.0
      NT = TIME+4.
      WRITE(3,699)
     * (VOL,I=1,7),NPEN,VOL,VOL,INCH,VOL,PAPER1     ,PAPER2     ,VOL,
     * START     ,VOL,NT,VOL,DATE   ,VOL,NF,(VOL,I=1,5),PGMR,PHONE,
```

```
     * VOL,VOL,NAME,VOL,LC,(VOL,I=1,4),DOUT,VOL,VOL
      WRITE(8,699)
     * (VOL,I=1,7),NPEN,VOL,VOL,INCH,VOL,PAPER1     ,PAPER2     ,VOL,
     * START     ,VOL,NT,VOL,DATE   ,VOL,NF,(VOL,I=1,5),PGMR,PHONE,
     * VOL,VOL,NAME,VOL,LC,(VOL,I=1,4),DOUT,VOL,VOL
  699 FORMAT(1H1,19X,A6,59(1H*)/20X,A6,58X,1H*
     */     20X, A6,9X,40HINSTRUCTIONS TO CALCOMP PLOTTER OPERATOR,9X,1H*
     */     20X, A6,58X,1H*/20X,A6,59(1H*)/20X,A6,58X,1H*
     */     20X, A6,21X,10HUSE NUMBER,I2,4H PEN,21X,1H*/20X,A6,58X,1H*
     */     20X, A6,9X,10HPLOT WIDTH,15X,2H= ,I2,5H INCH,15X,1H*
     */     20X, A6,9X,13HTYPE OF PAPER,12X,2H= ,2A8, 6X,1H*
     */     20X, A6,9X, 9HSTART PEN,16X,2H= , A8,14X,1H*
     */     20X, A6,9X,13HPLOTTING TIME,12X,1H=, I3,8H MINUTES,12X,1H*
     */     20X, A6,9X,15HDATE OF PLOT    ,10X,2H= ,A8,14X,1H*
     */     20X, A6,9X,15HLENGTH OF PAPER,10X,1H=,I3,5H FEET,15X,1H*
     */     20X, A6,9X,18HLAST BLOCK ADDRESS,6X, 6H = 999,19X,1H*
     */     20X, A6,58X,1H*/20X,A6,59(1H*)/20X,A6,58X,1H*
     */     20X, A6, 9X, 13HSUBMITTED BY , 3A4, 5X, 6HPHONE ,3A4, 2H *
     */     20X, A6,58X,1H*
     */     20X, A6,17X, 7HPROGRAM ,11(1H.),A6,17X,1H*
     */     20X, A6,17X,19HLABOR COST CODE.....,A4,1HL,17X,1H*
     */     20X, A6,17X,18HREEL NUMBER........,A6,17X,1H*
     */     20X, A6,58X,1H*/20X,A6,17X,6A4,17X,1H*
     */     20X, A6,58X,1H*/20X,A6,59(1H*))
      RETURN
      END
      SUBROUTINE STRESS(        IA,NELEMT, HTOP,HTOPP)
      COMMON/BLK1/ X(700),Y(700),NOD(600,4),IX
      COMMON/BLK2/MNO(600),NODB(200),BIV(200,3),IIFLG(3),BIVD(3)
     1     ,NELEM, NPT, NBPTC, NINC
      COMMON/BLK3/ C1(17,17),ZY(17),RT(3),ZT(3),RQ(4),ZQ(4),
     1           NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2            , IS(5), BS(3), AS(3),  RO, J1,
     3            AL(3,3), BT(3,3), GA(3,3) , Z5(12,12), Z4( 12)
     4    ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      COMMON/BLK4/ SL(112),S(112,56)
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
      COMMON/BLK6/AB(10),EB(10),XIB(10),BE(10),DE(10),TE(10),F(3)
     1 ,TK(10)

      DIMENSION  DUMY (8)
C
C     FORMAT STATEMENTS
C
  917 FORMAT(1H1,22HCONSTRUCTION INCREMENT,I4////)
  920 FORMAT(I7 ,4X,1P11E11.2)
  922 FORMAT(5X, 7HELEMENT, 45X,
```

```
     1                    28HELEMENT STRAINS AND STRESSES / ,6X,3HNO.,8X
     1  ,1HX,10X,1HY,6X,9HEPSILON-X, 2X, 9HEPSILON-Y, 3X, 7HGAMA-XY, 4X,
     2 7HSIGMA-X, 4X, 7HSIGMA-Y,4X,6HTAU-XY,5X,7HSIGMA-1, 4X, 7HSIGMA-2,
     3   6X, 3HANG, /)
  924 FORMAT(1H1,4X,4HNODE, 7X, 13HDISPLACEMENTS, / 6X, 3HNO. , 8X,
     1          1HU, 10X, 1HV, /)
  925 FORMAT(1H1)
  926 FORMAT(10X,18HSTRIP AXIAL FORCE=,1PE11.3,3X,7HMOMENT=,E11.3)
  927 FORMAT(12X,21HSKIN MEMBRANE STRESS=,E11.3)
  929 FORMAT(1X)
  930 FORMAT(I7,5X, 9HBEAM-- P=,1PE11.3,3X,2HV=,E11.3,3X,2HM=, E11.3)

      BOUNDARY POINTS TRANSFORMED TO X-Y COORDINATE SYSTEM

      DO 600 K=1,NBPTC
      KK=IABS(NODB(K))
      NODB(K)=KK
      ANG=BIV(K,3)
      IF(ANG .EQ. 0.0) GO TO 600
      K1=KK/15000
      JJ=NO(K1)/100
      IF(JJ.EQ.NO(K1+1)/100) GO TO 600
      CT=COS(ANG)
      SA=SIN(ANG)
      D1=SL(JJ)
      D2=SL(JJ+1)
      SL(JJ)=D1*CT-D2*SA
      SL(JJ+1)=D1*SA+D2*CT
  600 CONTINUE

      FOR EACH ELEMENT FIND STRAINS AND STRESSES

      REWIND 2
      DO 726 III=1,NELEMT

      RECALL ELEMENT STIFFNESS MATRIX

      READ (2)(ZY(M),STORE(M),(C1(M,N),N=1,17),M=1,17),((CP(J,K),K=1,3),
     1     J=1,3)
      I=STORE(17)+0.1
      MN=MNO(I)/1000
      ITYP=MOD(NON(MN),10)+1
      NOD(I,1)=IABS(NOD(I,1))

      CALCULATE ELEMENT UNKNOWNS

      L=1
      DO  620 J=1,4
```

```
      K=NOD(I,J)
      ND=NO(K)/100
      DUMY (L)   = -ZY (L)
      DUMY (L+1) = -ZY (L+1)
      ZY(L)=SL(ND)
      ZY(L+1)=SL(ND+1)
  620 L=L+2
      IF ( I .NE. 280 )  GOTO 7215
      DO 7025 J = 1, 8
      DO 7025 K = 1, 8
7025  DUMY (J) = DUMY (J) + C1 (J, K) * ZY (K)
7215  CONTINUE
      IF(ITYP.NE.5) GO TO 621
      ZY(6)=SL(ND+2)
      CALL BEAMST(I,MN)
      GO TO 718
  621 JTRY=2
      IF(NOD(I,3) .NE. NOD(I,4))GO TO 625
      JTRY=1
      DO 622 J=9,17
  622 ZY(J)=0.0
      GO TO 658
  625 DO  630 J=1,8
      DO  630 K=9,17
  630 ZY(K)=ZY(K)-C1(K,J)*ZY(J)
      ZY(9)=ZY(9)/C1(9,9)
      DO  650 J=10,17
      KA=J-1
      DO  645 K=9,KA
  645 ZY(J)=ZY(J)-ZY(K)*C1(J,K)
  650 ZY(J)=ZY(J)/C1(J,J)
  658 DO 660 K=1,4
  660 RO(K)   =0.0
C
C     CALCULATE SUB-ELEMENT EXPANSION COEFFICIENTS
C
      DUXX=0.0
      DUXY=0.0
      DUYY=0.0
      DVXX=0.0
      DVXY=0.0
      DVYY=0.0
      DO  715 J1=1,JTRY
      DO  670 K=1,12
  670 Z4(K)=0.0
      M=6*J1-7
      DO 675 K=1,3
      M=M+2
```

```
      RT(K)=STORE(M)
  675 ZT(K)=STORE(M+1)
      J1P=J1
      DU=0.5
      IF (JTRY .EQ. 2)GO TO 677
      DU=1.0
      J1P=2
  677 CALL GEOM(AA,D1,D2,D3)
      DU=DU/AA
      MP=1
      DO  680 K=1,17
      KA=NETCL(K,J1)
      DO  680 MM=1,KA
      M=ITRW(MP,J1)
      Z4(M)=Z4(M)+ZY(K)*T(MP,J1)
  680 MP=MP+1
C
C     STRAINS CALCULATED FOR SUBELEMENTS
C
      IF(ITYP .NE. 4)GO TO 697
      DD1=0.5/AA/AA
      DO 695 K=1,3
      JI=IS(K+1)
      KI=IS(K+2)
      BJI=BS(JI)
      BKI=BS(KI)
      AJI=AS(JI)
      AKI=AS(KI)
      BI=Z4(K+6)
      CI=Z4(K+9)
      DUXX=DUXX+DD1*2.0*BJI*BKI*BI
      DUXY=DUXY+DD1*(AJI*BKI+BJI*AKI)*BI
      DUYY=DUYY+DD1*2.0*AJI*AKI*BI
      DVXX=DVXX+DD1*2.0*BJI*BKI*CI
      DVXY=DVXY+DD1*(AJI*BKI+BJI*AKI)*CI
  695 DVYY=DVYY+DD1*2.0*AJI*AKI*CI
  697 EX=0.
      EY=0.0
      GAMXY=0.0
      DO 701 K=1,3
      D1=AS(K)
      D2=BS(K)
      EX=EX+Z4(K)*D2
      EY=EY+Z4(K+3)*D1
  701 GAMXY=GAMXY+Z4(K)*D1+Z4(K+3)*D2
      RQ(1)=EX*DU+RQ(1)
      RQ(2)=EY*DU+RQ(2)
      RQ(3)=GAMXY*DU+RQ(3)
```

```
      DU=(1.0-DU*AA)*0.5/AA
      IF(J1 .EQ. 2)GO TO 705
      RQ(1)=RQ(1)-DU*BS(1)*(Z4(7)-Z4(8)-Z4(9))
      RQ(2)=RQ(2)-DU*AS(1)*(Z4(10)-Z4(11)-Z4(12))
      RQ(3)=RQ(3)-DU*(AS(1)*(Z4(7)-Z4(8)-Z4(9)) +BS(1)*(Z4(10)-Z4(11)
     1     -Z4(12)))
      GO TO 715
  705 RQ(1)=RQ(1)-DU  *BS(3)*(Z4(9)-Z4(8)-Z4(7))
      RQ(2)=RQ(2)-DU  *AS(3)*(Z4(12)-Z4(11)-Z4(10))
      RQ(3)=RQ(3)-DU  *(AS(3)*(Z4(9)-Z4(8)-Z4(7)) +BS(3)*(Z4(12)-Z4(11)
     1     -Z4(10)))
  715 CONTINUE
C
C     INCREMENTAL STRESSES CALCULATED
C
      DO 717 L=1,3
      DU=0.0
      DO 716 J=1,3
  716 DU=DU+RQ(J)*CP(L,J)
  717 ZQ(L)=DU
C
C     FORCES IN REINFORCING STRIP DETERMINED FROM COMPOSITE MATERIAL
C
      IF(ITYP.NE.4)GO TO 718
      NP=NON(MN)/1000
      IAC=MOD(MNO(I),1000)/10
      ND=IAC-IA
      CALL STREH(DUXX,DUXY,DUYY,DVXX,DVXY,DVYY,MN,HTOP,ND,HTOPP,I,NP)
C
C             INCREMENTAL STRESSES AND STRAINS ADDED TO TOTAL VALUES
C
  718 DO 719 J=1,3
      ST(I,J+6)=ST(I,J+6)+F(J)
      ST(I,J+3)=ST(I,J+3)+ZQ(J)
  719 ST(I,J)=ST(I,J)+RQ(J)
  726 CONTINUE
C
C     PRINT ELEMENT STRAINS AND STRESSES
C
      WRITE (6,917) IA
      WRITE(6,922)
      IPG=8
      DO 760 I=1,NELEM
      N=MNO(I)
      IAC=MOD(N,1000)/10
      IF(IAC .GT. IA ) GO TO 760
      MN=N/1000
      ITYP=MOD(NON(MN),10)+1
```

```
      IF(ITYP.NE.5) GO TO 728
      IPG=IPG+1
      WRITE(6,930)I,(ST(I,K),K=1,3)
      GO TO 760
  728 N1=NOD(I,1)
      N2=NOD(I,2)
      N3=NOD(I,3)
      N4=NOD(I,4)
      XC=(X(N2)+X(N4))*0.5
      YC=(Y(N2)+Y(N4))*0.5
      IF(N3 .NE. N4)GO TO 730
      XC=(XC*2.0+X(N1))/3.0
      YC=(YC*2.0+Y(N1))/3.0
  730 DO 740 J=1,3
  740 RQ(J)=ST(I,J+3)

      PRINCIPAL STRESSES CALCULATED

      CALL PRINC (RQ,ZQ)
      IF(IPG .LT. 40) GO TO 744
      WRITE(6,925)
      WRITE(6,922)
      IPG=4

      WRITE ELEMENT STRESSES AND STRAINS

  744 WRITE(6,920) I,XC  , YC, (ST(I,K)              ,K=1,6),(ZQ(L),L=1,3)
      IPG=IPG+1
      IF(ITYP.NE.4)GO TO 760
      WRITE(6,926)(ST(I,K),K=7,8)
      IPG=IPG+2

       MEMBRANE STRESS DETERMINATION    EQUALS PR/T

      IPRNT=MOD(N      ,10)
      IF(IPRNT.EQ.0)GO TO 755
      TH=TE(MN)*.014533
      CT=COS(TH)
      SINT=SIN(TH)
      S1=ST(I,4)*CT*CT+ST(I,5)*SINT*SINT+2.*ST(I,6)*CT*SINT
      STRM=-S1*DE(MN)/(2.*TK(MN))
      WRITE(6,927)STRM
      IPG=IPG+1
  755 WRITE(6,929)
  760 CONTINUE
C
C     DISPLACEMENTS PRINTED
C
```

```
      DO 785 I=1,NPT
      IF (MOD(NQ(I),100) .EQ. 0)GO TO 785
      JJ=NQ(I)/100
      DU=SL(JJ)
      DV=SL(JJ+1)
      X(I)=X(I)+DU
      Y(I)=Y(I)+DV
      U(I)=U(I)+DU
      V(I)=V(I)+DV
  785 CONTINUE
      CALL  RESOUT(4)
      REWIND 2
      WRITE (6, 9421)  ( DUMY(J),J = 1, 8)
 9421 FORMAT (1P8E12.4)
      RETURN
      END
      SUBROUTINE PREP
C
C     THIS SUBROUTINE SETS UP THE DESCRIPTION OF THE PROBLEM
C
      DIMENSION ANI(8),AN(3),TITLE(20)  , IMAGE(20)
      DIMENSION PHON (3)
      COMMON /CNTRL/  WIDTH, INOUT, INCR2,LC1,PGM1,PGM2,PHON
      COMMON  /HDLIN/  TITLE
      COMMON/BLK1/ X(700),Y(700),NOD(600,4),IX
      COMMON/BLK2/MNO(600),NODB(200),BIV(200,3),IIFLG(3),BIVD(3)
     1     ,NELEM, NPT, NBPTC, NINC
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
      COMMON/BLK6/AB(10),EB(10),XIB(10),BE(10),DE(10),TE(10),F(3)
     1 ,TK(10)
C
C        FORMAT STATEMENTS
C
  800 FORMAT (I5, F10.0, 2I5, 6A4)
  801 FORMAT (       3E10.5)
  802 FORMAT (I1,I4,10I5)
  803 FORMAT (9X,20A4)
  805 FORMAT (20A4)
  806 FORMAT (I1,I4,I5,F10.0,I5,2F10.0,3I5 ,2F10.0)
  807 FORMAT (I1,I4,I2, I3, 6E10.5)
  808 FORMAT (I1,I4,2F10.0, I5,2F10.0,I5,F10.0)
  809 FORMAT(7F10.5)
  900 FORMAT (1H1 8X 20A4, ///)
  901 FORMAT(1H0,4X,35HNUMBER OF CONSTRUCTION INCREMENTS =,I4//////)
  902 FORMAT(1H1//////10X,29H*****ELEMENT INFORMATION*****///1X,
     1        7HELEMENT,10X,                    7HELEMENT,13X,
     2        8HMATERIAL,4X,12HCONSTRUCTION/1X,6HNUMBER,
```

```
     3                                10X,11HNODE POINTS,10X,6HNUMBER,6X,
     4          16HINCREMENT NUMBER)
  903 FORMAT(1H0,9X, 35HPROPERTIES ARE OVERBURDEN DEPENDENT // 20X,
     1 45HMODULUS VS CONFINING PRESSURE - A(INTERCEPT)=, E11.4, /,52X,
     2  9HB(SLOPE)=, E11.4,/, 20X, 15HFRICTION ANGLE=, E11.4,/,20X,
     3   9HCOHESION=, E11.4, /, 20X, 15HPOISSONS RATIO=, E11.4)
  904 FORMAT(1H0,10X,15HYOUNGS MODULUS=,   E11.4, /, 11X,
     1                15HPOISSONS RATIO=,   E11.4)
  905 FORMAT(1H0, 9X,5HC-11=,  E11.4,/, 10X, 5HC-12=,    E11.4, /,
     1           10X,5HC-22=,   E11.4,/, 10X, 5HC-33=,   E11.4, /,
     2          10X,3HTH=,   E11.4)
  906 FORMAT(I7,6X,3(A6,1PE10.2,9X),I7/)
  907 FORMAT(1H0//5X,23HPROPERTIES FOR MATERIAL,I3,3X,8H********//,10X,
     1         9HDENSITY =,1PE15.5)
 908  FORMAT(/////1H     )
  909 FORMAT(I11,5X,1P2E10.2)
  911 FORMAT            (//, 1X 23HERROR-TO MANY MATERIALS)
  912 FORMAT            (//, 1X 23HERROR-TOO MANY ELEMENTS)
  913 FORMAT            (//, 1X 26HERROR-TOO MANY NODE POINTS)
  914 FORMAT            (//, 1X,34HERROR-TOO MANY BOUNDARY CONDITIONS)
  915 FORMAT(1H1//////10X,29H*****BOUNDARY CONDITIONS*****///1X,
     1         13HBOUNDARY NODE,74X,13HINCREMENT NO./)
  916 FORMAT(1H ,9X,1P3E20.2)
  917 FORMAT(I5,5X,              4I5,2I12)
  918 FORMAT(1H0// 5X, 8HMATERIAL,I4,2X,21HREPRESENTS A BENDING ,
    17HELEMENT, // ,11X, 5HAREA=,E11.4,//,11X,18HMOMENT OF INERTIA=,
    2F11.4,//,11X,15HYOUNGS MODULUS=,E11.4, //, 11X,
     3    15HPOISSONS RATIO=, E11.4)
  920 FORMAT(   28H ERROR-DATA ERROR IN ELEMENT, I5)
 921  FORMAT(1H0/,6X,16HREINFORCED EARTH//,
     1     10X,21HSTRIP YOUNGS MODULUS=,E11.4,/,
     2     10X,12HSTRIP WIDTH=,E11.4,/,
     3     10X,16HSTRIP THICKNESS=,E11.4,/,
     4     10X,19HHORIZONTAL SPACING=,E11.4,/,
     5     10X,17HVERTICAL SPACING=,E11.4,/,
     6     10X,6HANGLE=,E11.4,/,
     7     10X,35HSKIN THICKNESS IF BOUNDARY ELEMENT=,E11.4,/,
     8      8X,15HSOIL PROPERTIES)
  923 FORMAT(1H0,9X,31HELASTIC PROPERTIES - OVERBURDEN//20X,
     1         10HOVERBURDEN,10X,14HYOUNGS MODULUS,6X,14HPOISSONS RATIO)

      DATA ANI,AN(3)
     2      /4HU-X=, 4HP-X=, 4HU-Y=, 4HP-Y=, 4HU-N=, 4HP-N=,
     3 .    4HU-S=, 4HP-S=, 4HANG= /
C
C     INPUT DATA IS READ
C
      DO    1 I=1,3000
```

```
    1 ST(I,1)=0.0
      IXP=1
      READ(5,805,END=700) TITLE
      WRITE (6,900) TITLE
      WRITE(3,803) TITLE
      READ   (5,800)  NINC, WIDTH,INOUT,INCL,LC1,PGM1,PGM2,PHON
      READ (99,805)  IMAGE
      WRITE (3,803 ) IMAGE
      IF (INCL .LT. 1 )NINC = NINC + INCL
      IF (NINC .LT. 1)  NINC=1
      WRITE (6,901) NINC
C
C     MATERIAL PROPERTIES
C
      NMAT=0
    2 READ(5,807) NSEC,I,ITYP,NOMI,D1,D2,D3,D4, D5,D6
      READ (99,805)  IMAGE
      WRITE (3,803 ) IMAGE
      IF(NSEC .NE. 0) GO TO 106
      NOMI=NOMI+1
      NON(I)=NOMI*1000+ITYP
      DEN(I)=D1
      NMAT=NMAT+1
      ITYP=ITYP+1
      IF(ITYP.EQ.5) GO TO 95
      WRITE(6,907) I, D1
      GO TO (60,60,58,59),ITYP
C
C                ANISOTROPIC PROPERTIES
C
   58 WRITE(6,905) D2,D3,D4,D5,D6
      CALL ANISP(D2,D3,D4,D5,D6)
      GO TO 65
C
C               REINFORCED EARTH PROPERTIES
C
 59   READ(5,809)(EB(I),AB(I),XIB(I),BE(I),DE(I),TE(I),TK(I))
      READ (99,805)  IMAGE
      WRITE (3,803 ) IMAGE
      WRITE(6,921)(EB(I),AB(I),XIB(I),BE(I),DE(I),TE(I),TK(I))
      AB(I)=AB(I)*XIB(I)
      XIB(I)=AB(I)*XIB(I)*XIB(I)/12.
   60 IF (  NOMI .GE. 2) GO TO 80
C
C                LINEAR ISOTROPIC PROPERTIES
C
      WRITE(6,904) D3,D4
      E(I,1)=D3
```

```
      GNU(I,1)=D4
      IF(ITYP  .EQ. 4) GO TO 2
      CALL CONVT(D3,D4)
   65 L=0
      DO 70 J=1,3
      DO 70 K=J,3
      L=L+1
   70 H(I,L)=CP(J,K)
      GO TO 2
C
C              OVERBURDEN DEPENDENT ISOTROPIC PROPERTIES - TYPE A
C
   80 H(I,1)=D2
      E(I,1)=D3
      GNU(I,1)=D4
      IF(NOMI .GT. 2)GO TO 82
      H(I,2)=D5
      H(I,3)=D6
      WRITE(6,903) D3,D2,D5,D6,D4
      GO TO 2
C
C              OVERBURDEN DEPENDENT ISOTROPIC PROPERTIES - TYPE B
C
   82 NOMI=NOMI-1
      DO  90 N=2,NOMI
      READ(5,801)  H(I,N),E(I,N),GNU(I,N)
      READ (99,805)  IMAGE
      WRITE (3,803 ) IMAGE
   90 IF(GNU(I,N).EQ.0.0) GNU(I,N)=GNU(I,N-1)
      WRITE(6,923)
      WRITE(6,916) (H(I,N),E(I,N),GNU(I,N),N=1,NOMI)
      GO TO 2
C
C     BEAM PROPERTIES
C
   95 E(I,1)=D3
      GNU(I,1)=D4
      H(I,1)=D1
      H(I,2)=D2
      WRITE(6,918)I,D1,D2,D3,D4
      GO TO 2
C
C     INPUT CONTROL UNIT
C
  106 GO TO (107,112,175,195),NSEC
C
C     NODE POINT COORDINATES
C
```

```
  107 NPT=0
  108 READ(5,808) NSEC,N,XS  ,YS  ,NP,XP,YP,INCR,D
      READ (99,805)  IMAGE
      WRITE (3,803 ) IMAGE
      IF(NSEC .NE. 0) GO TO 106
      X(N)=XS
      Y(N)=YS
      ST(N,1)=1.0E+20
      IF(NPT .LT. N) NPT=N
      IF(NP  .EQ.0) GO TO 108
      IF(INCR .EQ. 0) INCR=1
      NS=N
      IF( D .LT. .01 .OR.  D .GT. 100. )  D = 1.0
      NM=(NP-NS)/INCR
      NMIS = IABS (NM)
      IF ( NMIS  .GT. 1) GO TO   1080
      INCR = NP- NS
      NM = 1
      NMIS = 1
      GOTO  1081
 1080 CONTINUE
      NPS=  (NP - NS)
      NPS2 = IABS(NPS)
      INCR2 = IABS (INCR)
      NCHK  =  NMIS * INCR2- NPS2
      IF (NCHK  .EQ.  0) GOTO 1081
      NP = N + NPS/NPS2 *INCR2 * NMIS
 1081 CONTINUE
      INCR=INCR*NM/NMIS
      DU2=NMIS
      DU1=1.0/DU2
      IF(D.EQ.1.0) GO TO 109
      DU1=(1.0-D)/(1.0-D**NMIS)
  109 DX=(XP  -XS)*DU1
      DY=(YP  -YS)*DU1
      DO 110 I=1,NMIS
      NS=NS+INCR
      XS=XS+DX
      YS=YS+DY
      ST(NS,1)=1.0E+20
      X(NS)=XS
      Y(NS)=YS
      DX=DX*D
  110 DY=DY*D
      IF(NPT .LT. NS) NPT=NS
      GO TO 108
C
C     ELEMENT INFORMATION
```

```
 112 MS=1
     N=1
     MNORS=1
25   FORMAT (    5(2H (,I3,1H),2F10.1))
     IF ( INOUT .GT.0 )
    1WRITE (3,25)(( I, X(I),  Y(I)) ,I= 1,NPT)
 113 READ(5,802) NSEC,(NOD(N,I),I=1,4),MNOR,M,NMIS,INCR,NMISP,INCRP
    1  ,IPRNT
     READ (99,805)  IMAGE
     WRITE (3,803 ) IMAGE
     IF(NSEC .NE. 0) GO TO 132
     M = M+INCL
     IF ( M .LT. 0)  M=0
     IF(NOD(N,3).EQ.0)NOD(N,3)=NOD(N,2)
     IF(NOD(N,4) .EQ. 0)NOD(N,4)=NOD(N,3)
     NS=N
     INCRS=0
     INCRZ=INCR
     NMISZ=NMISP
     IF(MNOR.EQ.0) MNOR=MNORS
     MNORS=MNOR
     IF(M.EQ.0) M=MS
     MS=M
     MNO(N)=MNOR*1000+M*10+IPRNT
 114 DO 115 M=1,4
 115 NOD(N,M)=NOD(NS ,M)+INCRS
     MNO(N)=MNO(NS)
     N=N+1
     INCRS=INCRS+INCRP
     NMISP=NMISP-1
     IF(NMISP .GE. 0)GO TO 114
     NMISP=NMISZ
     INCRS=INCRZ
     INCRZ=INCRZ+INCR
     NMIS=NMIS-1
     IF(NMIS .GE. 0)GO TO 114
     GO TO 113
C
C    GENERATE COORDINATES FOR UNSPECIFIED INTERIOR NODES
C
 132 NELEM =N-1
28   FORMAT ( 5 (3H  (,I3,1H),4I4  )  )
     IF ( INOUT .GT.0 )
    1WRITE (3,28) ( (I, ( NOD(I,K),K=1,4)),I=1,NELEM )
     NMIS=0
     DO 135 K=3,NPT
     IF(ST(K,1) .GT. .9E+20)GO TO 135
```

```
      X(K)=0.5*(X(K-2)+X(K-1))
      Y(K)=0.5*(Y(K-2)+Y(K-1))
      NMIS=NMIS+6
  135 CONTINUE
      IF(NMIS .EQ. 0)GO TO 163
      DO 155 NN=1,NMIS
      IOT=0
      DO 137 K=1,NPT
      ST(K,2)=0.0
      ST(K,3)=0.0
  137 ST(K,4)=0.0
      DO 141 IE=1,NELEM
      MN=MNO(IE)/1000
      ITYP=MOD(NON(MN),10)+1
      IF(ITYP.EQ.5) GO TO 141
      DO 140 JJ=1,4
      J=NOD(IE,JJ)
      I=JJ-1
      IF(I .EQ. 0)I=4
      I=NOD(IE,I)
      K=JJ+1
      IF(K .EQ. 5)K=1
      K=NOD(IE,K)
      ST(J,2)=ST(J,2)+X(I)+X(K)
      ST(J,3)=ST(J,3)+Y(I)+Y(K)
  140 ST(J,4)=ST(J,4)+2.0
  141 CONTINUE
      DO 150 K=1,NPT
      IF(ST(K,1) .GT. 0.9E+20 .OR. ST(K,4) .EQ. 0.0)GO TO 150
      D1=X(K)
      D2=Y(K)
      X(K)=ST(K,2)/ST(K,4)
      Y(K)=ST(K,3)/ST(K,4)
      D1=ABS((X(K)-D1)/(ABS(D1)+1.0E-20))
      D2=ABS((Y(K)-D2)/(ABS(D2)+1.0E-20))
      IF(D1+D2 .GT. .0001)IOT=1
  150 CONTINUE
      IF(IOT .EQ. 0)GO TO 163
  155 CONTINUE
C
C       PRINT NODE AND ELEMENT DATA
C
  163 CONTINUE
      CALL  RESOUT(1)
      WRITE (6,908)
      DO 168 N=1,NELEM
      MS=MOD(MNO(N),1000)/10
      MNORS=MNO(N)/1000
```

```
C
C     CHECK FOR NEGATIVE ELEMENT AREA
C
      N1=NOD(N,1)
      N2=NOD(N,2)
      N3=NOD(N,3)
      N4=NOD(N,4)
      IF (N4 .NE. N3)GO TO 164
      N4=0
      IF(N3.EQ.N2)N3=0
      GO TO 166
  164 A1=X(N1)*(Y(N2)-Y(N4))+X(N2)*(Y(N4)-Y(N1))+X(N4)*(Y(N1)-Y(N2))
      A2=X(N2)*(Y(N3)-Y(N4))+X(N3)*(Y(N4)-Y(N2))+X(N4)*(Y(N2)-Y(N3))
      B1=X(N1)*(Y(N2)-Y(N3))+X(N2)*(Y(N3)-Y(N1))+X(N3)*(Y(N1)-Y(N2))
      B2=X(N1)*(Y(N3)-Y(N4))+X(N3)*(Y(N4)-Y(N1))+X(N4)*(Y(N1)-Y(N3))
      IF(A1+A2 .GT. 0.0) GO TO 165
      IXP=3
      WRITE(6,920) N
  165 A1=A1*A2
      A2=B1*B2
      IF(A1 .GE. A2) GO TO 166
      NOD(N,1)=N2
      NOD(N,2)=N3
      NOD(N,3)=N4
      NOD(N,4)=N1
  166 CONTINUE
  168 CONTINUE
      CALL  RESOUT(2)
      GO TO 106
C
C     BOUNDARY CONDITIONS
C
  175 WRITE (6,915)
      I=1
  180 READ (5,806)NSEC,KK,(IIFLG(N),BIVD(N),N=1,2),TH,IA ,KKP,INCR,PJ,PK
      READ (99,805)  IMAGE
      WRITE (3,803 ) IMAGE
      IF(NSEC .NE. 0) GO TO 106
      NMIS=0
      IF(KKP .EQ. 0)GO TO 182
      IF(INCR .EQ. 0) INCR=1
      NM=(KKP-KK)/INCR
      NMIS=IABS(NM)
      INCR=INCR*NM/NMIS
  182 IF(IA .EQ. 0) IA=1
      NM=1+NMIS
      DP=PK-PJ
      IF(NMIS .EQ. 0) GO TO 185
```

```
      M=KK
      XL=0.0
      DO 183 L=1,NMIS
      MP=M
      M=M+INCR
  183 XL=SQRT((X(M)-X(MP) )**2+(Y(M)-Y(MP) )**2)+XL
      DP=DP/XL
  185 DXB=0.0
      DYB=0.0
      IADD=0
      IF(TH.NE.0.0) IADD=4
      DO 190 L=1,NM
      DXF=0.0
      DYF=0.0
      IF(L .EQ. NM) GO TO 186
      DXF=X(KK+INCR)-X(KK)
      DYF=Y(KK+INCR)-Y(KK)
      PK=PJ+DP*(SQRT(DXF*DXF+DYF*DYF))
  186 BIV(I,1)=BIVD(1)-(2.0*(DYF+DYB)*PJ+DYB*PI+DYF*PK)/6.0
      BIV(I,2)=BIVD(2)+(2.0*(DXF+DXB)*PJ+DXB*PI+DXF*PK)/6.0
      DXB=DXF
      DYB=DYF
      PI=PJ
      PJ=PK
      BIV(I,3)=TH
      NODB(I)=KK*10000+IIFLG(I)*10+IIFLG(2) +IA*100
      DO 187 J=1,2
      K=2*J-1+IADD
      AN(J  )=ANI(K+1)
      IF (IIFLG(J)   .EQ. 0) GO TO 187
      AN(J)=ANI(K)
  187 CONTINUE
      WRITE (6,906) KK        ,(AN(J),BIV(I,J),J=1,3),IA
      KK=KK+INCR
      BIV(I,3)=TH*0.0174533
  190 I=I+1
      GO TO 180
  195 NBPTC=I-1
C
C         THE SIZE OF THE PROBLEM IS CHECKED TO SEE IF IT IS TOO LARGE
C     AND DATA ERRORS ARE SOUGHT
C
      IF (NELEM .LT. 600) GO TO 206
      WRITE (6,912)
      IX=0
  206 IF (NPT .LT. 701)GO TO 207
      WRITE (6,913)
      IX=0
```

```
207 IF(NBPTC.LT.200) GO TO 208
    WRITE (6,914)
    IX=0
208 IF (NMAT.LT.11) GO TO 210
    WRITE (6,911)
    IX=0

210 IF(IXP .EQ. 0)IX=0
    CALL FINEL( WIDTH)
    RETURN
700 STOP
    END
    SUBROUTINE  RESOUT(ITYP)
    COMMON/BLK1/ X(700),Y(700),NOD(600,4),IXXX
    COMMON/BLK2/MNO(600),NODB(200),BIV(200,3),IIFLG(3),BIVD(3)
   1, NELEM , NPT   , NUMPC, NINC
    COMMON/BLK3/ C1(17,17),ZY(17),RT(3),ZT(3),RQ(4),ZQ(4),
   1          NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
902 FORMAT ( 1H1,3(' ELEM',7X,'ELEMENT',7X,'MAT   CONST',5X,1H  )/
   * 3('   NO.',4X,'NODAL POINTS     NO.   INCR.     '  ) /1H      )
908 FORMAT(1H1,3(1X,'NODAL',8X,'X',13X,'Y',11X,1H ) /  1X,
   * 3(1X,'POINT',3X,'COORDINATE',4X,'COORDINATE',7X,1H  ) /1H     )
909 FORMAT( 3(1X,I4,2(1X,F13.2) , 7X,1H   ) )
917 FORMAT( 2X,3(I3,3X,I3,3(1X,I3),2(4X,I2),9X,1H ) )
922 FORMAT(1H1,3(1X,'NODAL',8X,'X',13X,'Y',11X,1H ) /  1X,
   * 3(1X,'POINT',3X,'DISPLCEMNT',4X,'DISPLCEMNT',7X,1H  ) /1H     )
1001 FORMAT(83X,I4,  2F14.2   )
1002 FORMAT(83X,I4, 2(1X,1PE13.2))
1006 FORMAT( 3(1X,I4,2(1X,1PE13.2),7X,1H   ) )
1010 FORMAT(88X,  I3,3X,I3,3(1X,I3),2(4X,I2))
    IF(ITYP .EQ. 2) GOTO 166
163 CONTINUE
    LLINE = NPT / 3
    NPG   = LLINE / 37
    LINES = NPG *37
    LINS = 1
    N1 = 1
    IF (LLINE .LT. 37) GO TO  550
    INC = 37
    KSHIFT = 3*INC
502 CONTINUE
    IF( LINS .GT. LINES)  GOTO 550
    N3 = N1+2*INC
    LINE = 1
    IF(ITYP.EQ.4) GOTO 504
    WRITE (6,908)
    GOTO  505
504 WRITE (6,922)
```

```
505   CONTINUE
      IF( LINS .GT. LINES)  GOTO 550
      IF(ITYP .EQ. 4) GOTO  520
      WRITE (6,909)  (N, X(N), Y(N) ,N=N1,N3,INC )
      GOTO 523
520   CONTINUE
      WRITE(6,1006)( N, U(N), V(N), N=N1,N3,INC )
523   CONTINUE
      LINS = LINS + 1
      LINE = LINE + 1
      N1 = N1 + 1
      N3 = N3 + 1
      IF (LINE  .LE.  37 ) GO TO 505
      N1 = N1 + 2*INC
      GO TO 502
 550  CONTINUE
      IF (LINES .EQ. LLINE ) GOTO 552
      INC = LLINE -LINES
      LINES = LLINE
      GOTO  502
552   CONTINUE
      N3=LINES*3+1
      IF ( N3   .GT.  NPT)  GOTO 555
      IF(ITYP .EQ. 4) GOTO  554
      WRITE(6,1001) (N,X(N),Y(N),N=N3,NPT )
      GOTO  555
554   CONTINUE
      WRITE(6,1001) (N,U(N),V(N),N=N3,NPT )
555   CONTINUE
      IF(ITYP .EQ. 1) GOTO  730
      IF(ITYP .EQ. 4) GOTO  730
166   CONTINUE
      LLINE = NELEM/3
      NPG   = LLINE / 37
      LINES = NPG *37
      LINS = 1
      N1 = 1
      IF (LLINE .LT. 37) GO TO  700
      INC = 37
      KSHIFT = 3*INC
600   CONTINUE
      IF( LINS .GT. LINES)  GOTO 700
      N2 = N1 + INC
      N3 = N1+2*INC
      WRITE(6,902)
      LINE = 1
610   CONTINUE
      IF( LINS .GT. LINES)  GOTO 700
```

```
      MN1    = MNO(N1)/1000
      MN2    = MNO(N2)/1000
      MN3    = MNO(N3)/1000
      INC1   = MOD(MNO(N1),1000)/10
      INC2   = MOD(MNO(N2),1000)/10
      INC3   = MOD(MNO(N3),1000)/10
      WRITE(6,917) N1,(NOD(N1,K),K=1,4),MN1,INC1, N2,(NOD(N2,K),K=1,4)
     * ,MN2, INC2, N3,(NOD(N3,K),K=1,4), MN3, INC3
      LINE = LINE + 1
      LINS = LINS + 1
      N1 = N1 + 1
      N2=N2+1
      N3 = N3 + 1
      IF (LINE  .LE.  37 ) GO TO 610
      N1 = N1 + 2*INC
      GO TO 600
  700 CONTINUE
      IF (LINES .EQ. LLINE ) GOTO 707
      INC = LLINE -LINES
      LINES = LLINE
      GOTO 600
  707 CONTINUE
        N3=LINES*3+1
  709 CONTINUE
      IF ( N3   .GT. NELEM) GOTO 730
      MN3    = MNO(N3)/1000
      INC3   = MOD(MNO(N3),1000)/10
      WRITE(6,1010)N3,(NOD(N3,K),K=1,4),MN3,INC3
      N3=N3+1
      GOTO 709
  730 CONTINUE
      RETURN
      END
C
C
C     INCREMENTAL PLAIN STRAIN ANALYSIS
      COMMON /CNTRL/  WIDTH, INOUT, INCL
      COMMON/BLK1/ X(700),Y(700),NOD(600,4),IX
      COMMON/BLK2/MNO(600),NODB(200),BIV(200,3),IIFLG(3),BIVD(3)
     1     ,NELEM, NPT, NBPTC, NINC
      COMMON/BLK3/ C1(17,17),ZY(17),RT(3),ZT(3),RQ(4),ZQ(4),
     1           NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2            , IS(5), BS(3), AS(3),  RO, J1,
     3            AL(3,3), BT(3,3), GA(3,3) , Z5(12,12), Z4( 12)
     4   ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      COMMON/BLK4/ SL(112),S(112,56)
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
```

```
      COMMON/BLK6/AB(10),EB(10),XIB(10),BE(10),DE(10),TE(10),F(3)
     1 ,TK(10)
   30 FORMAT( 1H1,8X,28HINPUT DATA CARD IMAGE ****    /2X,1H          )
      WRITE (3,30)
C
C
C     THE SIZE OF THE EQUATION BLOCK IS SET
C
      CALL DHRERD
      NEQ=56
      NBW=NEQ
      CALL ESTAB
C
C     INPUT DATA IS READ
C
  100 IX=NEQ
      HTOP=-1.0E+09
      CALL PREP
      IF ( INOUT .GT.0 )  GOTO 590
      IF(IX  .EQ. 0) GO TO 100
C
C     INITIALIZATION OF STORAGE ARRAYS
C
      DO 140 I=1,NPT
      U(I)=0.0
  140 V(I)=0.0
      DO 142 I=1,NELEM
      DO 142 J=1,9
  142 ST(I,J)=0.0
C
C     INCREMENTAL ANALYSIS LOOP
C
      IA=0
  150 IA=IA+1
C
C     THE EQUATION POSITIONING MATRIX FOR THE SYSTEM MATRIX IS FORMED
C     AND THE ELEVATION OF THE TOP OF THE CONSTRUCTION INCREMENT ESTABLI
C
      DO 160 I=1,NPT
  160 NQ(I+1)=0
      HTOPP=HTOP
      DO 198 M=1,NELEM
      IAC=MOD(MNO(M),1000)/10
      IF(IAC.GT.IA) GO TO 198
      LS=200
      MN=MNO(M)/1000
      ITYP=MOD(NON(MN),10)+1
      IF(ITYP.EQ.5)LS=300
```

```
      I=(300-LS)/100
      DU1=I
      DO 180 J=1,4
      I=NOD(M,J)+1
      DU=Y(I-1)*DU1
      IF(HTOP .LT. DU)HTOP=DU
  180 IF(NQ(I).LT.300)NQ(I)=LS
  198 CONTINUE
      NQ(1)=100
      DO 200 I=1,NPT
  200 NQ(I+1)=NQ(I)+NQ(I+1)
C
C     THE BAND WIDTH-NPC- IS COMPUTED
C
      NPC=0
      DO 218 I=1,NELEM
      MN=MND(I)
      MN=MOD(MN     ,1000)/10
      IF(MN.GT.IA) GO TO 218
      DO 202 J=1,4
      JJ=NOD(I,J)
      NQ(JJ)=NQ(JJ)+1
      DO 202 K=1,4
      KK=NOD(I,K)+1
      IV=NQ(KK)/100-NQ(JJ)/100
      IF (NPC  .LT. IV) NPC=IV
  202 CONTINUE
  218 CONTINUE
C
C     COMPUTE MATRIX SPECIFICATIONS
C
      IF (NPC .LE. NEQ) GO TO 220
      WRITE (6,910)
  910 FORMAT              (//, 1X 25HERROR-BAND WIDTH TO LARGE)
      GO TO 100
  220 NCOL = NPC
      NROW=NQ(NPT +1)/100-1
C
C     INITIALIZE SYSTEM MATRIX
C
      MN=2*NEQ
      DO 223 N=1,MN
      SL(N)=0.
      DO 223 J=1,NEQ
  223 S(N,J) = 0.
C
C     THE STIFFNESS MATRIX IS GENERATED IN BLOCKS AND STORED ON TAPE
C
```

```
      REWIND 1
      LB=0
      LB1=0
      NELEMT=0
  288 LB=LB+1
      NB=(LB-1)*NEQ+1
      MB=LB*NEQ
C
C     EACH ELEMENT IS EXAMINED TO DETERMINE IF IT CONTRIBUTES TO THE
C     BLOCK
C
      DO  355 I=1,NELEM
      IX=I
      IF(NOD(I,1) .LT. 0) GO TO 355
      IAC=MOD(MNO(I),1000)/10
      MN=MNO(I)/1000
      RO=DEN(MN)
      IF(IAC-IA) 290,292,355
  290 RO=0.0
  292 DO 300 L=1,4
      KK=NOD(I,L)
      K1=NO(KK)/100
      IF ( K1       .LE. MB) GO TO 305
  300 CONTINUE
      GO TO 355
C
C     CALCULATE THAT PORTION OF THE STIFFNESS MATRIX GIVEN BY A
C     CONSIDERATION OF ELEMENT I
C
  305 ITYP=MOD(NON(MN),10)+1
      NP=NON(MN)/1000
      ND=IAC-IA
      GO TO (306,308,306,320,349),ITYP
  306 L=0
      IF(NP .GT. 1)GO TO 308
      DO 307 J=1,3
      DO 307 K=J,3
      L=L+1
      CP(J,K)=  H(MN,L)
  307 CP(K,J)=CP(J,K)
      GO TO 349
  308 CALL INTP1(   EI,GNUI,MN,HTOP,ND,HTOPP,I,NP)
      CALL CONVT(EI,GNUI)
      GO TO 349
  320 CALL REINF(MN,HTOP,ND,HTOPP,I,NP)
  349 CALL STIFNS(IA,LB1,NEQ,MN)
      NELEMT=NELEMT+1
      NOD(I,1)=-NOD(I,1)
```

```
355 CONTINUE
C
C     IF HAVE LESS THAN 1 BLOCK  OF EQUATIONS LEFT NO ADDITIONAL TAPE
C     STORAGE IS USED
C
      IF(NROW .LE. MB ) GO TO 560
      LB1=LB1+1
C
C     THE BLOCK OF EQUATIONS IS REDUCED AND PUT ON TAPE
C
      CALL REDUCI(NEQ,NCOL)
      WRITE (1) (SL(N),(S(N,M),M=1,NCOL), N=1,NEQ)
C
C     THE NUMBER TWO BLOCK OF EQUATIONS IS SHIFTED INTO THE NUMBER ONE
C     POSITION
C
      DO 555 L=1,NEQ
      LRH=L+NEQ
      SL(L)=SL(LRH)
      SL(LRH)=0.0
      DO 555  M=1,NCOL
      S(L,M)=S(LRH,M)
555   S(LRH,M)=0.0
      GO TO 289
560   NT=NROW-LB1*NEQ
C
C     THE FINAL TWO BLOCKS OF EQUATIONS ARE REDUCED AND BACK-SUBSTITUED
C
      CALL REDUCI(NT,NCOL)
      NS=LB1
      CALL BAKSUB(NT,NCOL,LB,NEQ)
      IF (LB1 .EQ. 0) GO TO 564
      DO 563 J=1,LB1
      DO 562 L=1, NEQ
      LL=L+NEQ
562   SL(LL)=SL(L)
      L =LB1-J+1
C
C     ANY BLOCKS ON TAPE ARE RECALLED AND BACK SUBSTITUED
C
      BACKSPACE 1
      READ (1) (SL(N),(S(N,M),M=1,NCOL),N=1,NEQ)
      BACKSPACE 1
      CALL BAKSUB(NEQ,NCOL,L,NEQ)
563   CONTINUE
564   L=0
      DO 566 N=1,LB
      K=NEQ
```

```
      DO 566 KK=1,NEQ
      K=K+1
      L=L+1
  566 SL(L)=S(K,N)
C
C     STRESSES AND STRAINS COMPUTED
C
      CALL STRESS(        IA,NELEMT,HTOP,HTOPP)
      IF (IA .LT. NINC) GO TO 150
 590  CONTINUE
      GO TO 100
      END
      SUBROUTINE BEAMST(I,MN)
C
C     THIS SUBROUTINE CALCULATES BEAM FORCES, SHEARS AND MOMENTS
C
      COMMON/BLK1/ X(700),Y(700),NOD(600,4),IX
      COMMON/BLK3/ C1(17,17),ZY(17),RT(3),ZT(3),RQ(4),ZQ(4),
     1          NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2            , IS(5), BS(3), AS(3),  RO, J1,
     3            AL(3,3), BT(3,3), GA(3,3) , Z5(12,12), Z4( 12)
     4   ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      COMMON/BLK4/ SL(112),S(112,56)
C
C     STIFFNESS MATRIX TIMES DISPLACEMENT
C
      COST=STORE(1)
      SINT=STORE(2)
      ZY(5)=ZY(4)
      ZY(4)=ZY(3)
      N1=NOD(I,1)
      ND=NQ(N1)/100+2
      ZY(3)=SL(ND)
      DO 100 K=1,6
      DU=0.0
      DO 90 L=1,6
   90 DU=DU+C1(K,L)*ZY(L)
  100 STORE(K)=DU
      RQ(1)=-STORE(1)*COST-STORE(2)*SINT
      RQ(2)=STORE(1)*SINT-STORE(2)*COST
      RQ(3)=-STORE(3)
      ZQ(1)=STORE(4)*COST+STORE(5)*SINT
      ZQ(2)=-STORE(4)*SINT+STORE(5)*COST
      ZQ(3)=STORE(6)
      DO 200 K=1,3
  200 RQ(K)=0.5*(RQ(K)+ZQ(K))
      RETURN
      END
```

```
      SUBROUTINE BEAMEL(I,MN)
C
C     THIS SUBROUTINE CALCULATES THE STIFFNESS MATRIX FOR A BENDING ELEM
C
      COMMON/BLK3/ C1(17,17),ZY(17),RT(3),ZT(3),RQ(4),ZQ(4),
     1           NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2            , IS(5), BS(3), AS(3),  RO, J1,
     3            AL(3,3), BT(3,3), GA(3,3) , Z5(12,12), Z4( 12)
     4   ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
      CA=RQ(2)-RQ(1)
      SA=ZQ(2)-ZQ(1)
      XL=SQRT(CA*CA+SA*SA)
      CA=CA/XL
      SA=-SA/XL
      STORE(1)=CA
      STORE(2)=-SA
      GNUB=GNU(MN,1)
      EB=E(MN,1)/(1.0-GNUB*GNUB)
      XIB=H(MN,2)
      AB=H(MN,1)
      DU=EB*AB/XL
      C1(1,1)=DU
      C1(4,1)=-DU
      C1(1,4)=-DU
      C1(4,4)=DU
      XL=0.5*XL
      RQ(1)=0.0
      RQ(3)=0.0
      D=.25/XL
      RQ(2)=-D
      RQ(4)=D
      ZQ(2)=D
      ZQ(4)=D
      D=D/XL
      ZQ(1)=D
      ZQ(3)=-D
      D=8.0*XL*EB*XIB
      DO 120 L=1,4
      LS=L+1+L/3
      DO 120 J=1,4
      JS=J+1+J/3
C
  120 C1(LS,JS)=D*(RQ(J)*RQ(L)+3.       *ZQ(J)*ZQ(L))
C
C     LOCAL UNKNOWNS TRANSFORMED TO GLOBAL UNKNOWNS
      DO 400 NR=1,4,3
```

```
      DO 315 JJ=1,6
      D2=C1(NR+1,JJ)
      D1=C1(NR,JJ)
      C1(NR,JJ)=D1*CA+D2*SA
  315 C1(NR+1,JJ)=-D1*SA+D2*CA
      DO 318 II=1,6
      D1=C1(II,NR)
      D2=C1(II,NR+1)
      C1(II,NR)=D1*CA+D2*SA
  318 C1(II,NR+1)=-D1*SA+D2*CA
  400 CONTINUE
      RETURN
      END
      SUBROUTINE CONVT(D1,D2)
C
C     THIS SUBROUTINE EXPRESSES ISOTROPIC PROPERTIES IN ANISOTROPIC FORM
C
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
      IF(D2 .EQ. 0.5)D2=.495
      CP(3,3)=D1*0.5/(1.0+D2)
      D1=D1/((1.0+D2)*(1.0-2.0*D2))
      CP(1,2)=D2*D1
      CP(2,1)=CP(1,2)
      CP(1,3)=0.0
      CP(2,3)=0.0
      CP(3,1)=0.0
      CP(3,2)=0.0
      D1=D1*(1.0-D2)
      CP(1,1)=D1
      CP(2,2)=D1
      RETURN
      END
      SUBROUTINE ANISP(C11, C12, C22, C33, PI)
C
C     THIS SUBROUTINE TRANSFORMS ORTHOTROPIC PROPERTIES FROM THEIR
C     PREFERED DIRECTIONS TO GLOBAL COORDINATES
C
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
      DIMENSION  TH(3,3),RO(3,3)
      CP(1,3)=0.0
      CP(2,3)=0.0
      CP(3,1)=0.0
      CP(3,2)=0.0
      CP(1,1)=C11
      CP(1,2)=C12
      CP(2,2)=C22
```

```
      CP(3,3)=C33
      CP(2,1)=C12
      IF(PI .EQ. 0.0)GO TO 80
      PI=PI*0.0174533
      SPH=SIN(PI)
      CPH=COS(PI)
      D1=CPH*CPH
      D2=SPH*SPH
      C1=SPH*CPH
      TH(1,1)=D1
      TH(1,2)=D2
      TH(1,3)=C1
      TH(2,1)=D2
      TH(2,2)=D1
      TH(2,3)=-C1
      TH(3,1)=-2.0*C1
      TH(3,2)=2.0*C1
      TH(3,3)=D1-D2
      DO 67 M=1,3
      DO 67 N=1,3
      DU=0.0
      DO 65 L=1,3
   65 DU=DU+TH(L,N)*CP(M,L)
   67 RO(M,N)=DU
      DO 75 M=1,3
      DO 75 N=1,3
      DU1=0.0
      DO 72 L=1,3
   72 DU1=DU1+TH(L,M)*RO(L,N)
   75 CP(M,N)=DU1
   80 RETURN
      END
      SUBROUTINE INTP1(   EI,GNUI,MN,HTOP,ND,HTOPP,I,NP)
C
C     THIS SUBROUTINE CALCULATES   THE VALUES OF THE MATERIAL
C     PROPERTIES FOR A GIVEN OVERBURDEN
C
      COMMON/BLK1/ X(700),Y(700),NOD(600,4),IX
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
C
      IF(NP .LT. 2)GO TO 440
C
C      TYPE A
C
      GAM=DEN(MN)
      HAVG=0.0
      DO 300 J=1,4
```

```
      N=NOD(I,J)
  300 HAVG=HAVG+0.25*Y(N)
      HO=HTOPP-HAVG+0.5*(HTOP-HTOPP)
      IF(ND .EQ. 0)HO=0.5*(HTOP-HAVG)
      HO=HO*GAM
      HO = -ST (I,5)
      IF (HO .LT. 100.0)  HO = 100.0
      IF(NP .GT. 2)GO TO 390
      A=E(MN,1)
      B=H(MN,1)
      PH=H(MN,2)
      DU=(45.0+0.5*PH)*0.0174533
      PH=PH*0.0174533
      C=H(MN,3)
      SINP=SIN(PH)
      XNPH=(SIN(DU)/COS(DU))**2
      DU1=(1.0-SINP)*HO
      DU2=2.0*(C*COS(PH)+SINP* (HO/XNPH-2.0*C/SQRT(XNPH)))
      DU3=          (1.0-DU1*SINP/DU2)**2
      EI=(A+B*DU1)*DU3
      GO TO 445
C
C      TYPE B
C
  390 IC=NP-1
      IF(ND .NE. 0)HO=GAM*0.5*(HTOP-HTOPP)
      P1=ABS(ST(I,5))+ABS(HO)
      DO 400 J=1,IC
      K=J
      DU1=H(MN,K)
      IF(P1.LE.DU1) GO TO 430
  400 CONTINUE
      P1=DU1
  430 IF(K.EQ.1) GO TO 440
      DU2=GNU(MN,K-1)
      DU3=H(MN,K-1)
      GNUI=DU2+(GNU(MN,K)-DU2)*(P1-DU3)/(DU1-DU3)
      DU2=E(MN,K-1)
      EI=DU2+(E(MN,K)-DU2)*(P1-DU3)/(DU1-DU3)
      GO TO 450
  440 EI=E(MN,1)
  445 GNUI=GNU(MN,1)
  450 RETURN
      END
      SUBROUTINE STIFNS(IA,LB1,NEQ,MN)
C
C     THIS SUBROUTINE FORMS THE ELEMENT MATRIX FOR A QUADRILATERAL
C     ELEMENT
```

```
      COMMON/BLK1/ X(700),Y(700),NOD(600,4),I
      COMMON/BLK2/MNO(600),NODB(200),BIV(200,3),IIFLG(3),BIVD(3)
     1     ,NELEM, NPT, NBPTC, NINC
      COMMON/BLK3/ C1(17,17),ZY(17),XT(3),YT(3),RQ(4),ZQ(4),
     1           NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2            , IS(5), BS(3), AS(3),  RO, J1,
     3            AL(3,3), RT(3,3), GA(3,3) , CT(12,12), ZT( 12)
     4    ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      COMMON/BLK4/ SL(112),S(112,56)
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)

      IDENTIFICATION CODE FOR TRIANGULAR ELEMENTS SET

      JTRY=2
      IF(NOD(I,4).EQ.NOD(I,3)) JTRY=1
      DO 60 J=1,17
      DO 50 K=1,17
   50 C1(J,K)=0.0
   60 ZY(J)=0.0

      THE CORNER POINT COORDINATES ARE FOUND

      DO  90 J=1,4
      K=NOD(I,J)
      RQ(J)=X(K)
   90 ZQ(J)=Y(K)
      NU=2
      IF(NOD(I,3).NE.NOD(I,2)) GO TO 97
      CALL BEAMEL(I,MN)
      NU=3
      GO TO 313

      THE SUB-ELEMENT MATRICES ARE FOUND AND ADDED INTO THE ELEMENT
      MATRIX

   97 DO 300 J=1,JTRY
      JI=J

      NODE COORDINATES OF SUB-ELEMENT ARE FOUND

      DO 100 K=1,3
      XT(K)=RQ(K)
  100 YT(K)=ZQ(K)
      IF(JTRY.EQ.1) GO TO 105
      IF(J1 .EQ. 2) GO TO 103
      XT(3)=RQ(4)
```

```
      YT(3)=ZQ(4)
      GO TO 105
  103 XT(1)=RQ(4)
      YT(1)=ZQ(4)
  105 M=6*J1-7
      DO 220 K=1,3
      M=M+2
      STORE(M)=XT(K)
  220 STORE(M+1)=YT(K)
      CALL STFSUB
  300 CONTINUE
C
C     THE ELEMENT UNKNOWNS ARE ELIMINATED
C
      IF(JTRY.EQ.1) GO TO 313
      DO 312 K=1,9
      LL=17-K
      KK=18-K
      DU3=C1(KK,KK)
      DU2=ZY(KK)
      DO 312 L=1,LL
      DU1=C1(L,KK)/DU3
      DO 310 M=1,LL
  310 C1(L,M)=C1(L,M)-C1(KK,M)*DU1
  312 ZY(L)=ZY(L)-DU1*DU2
C
C     STIFFNESS MATRIX STORED
C
  313 STORE(17)=I
      WRITE(2)(ZY(M),STORE(M),(C1(M,N),N=1,17),M=1,17),((CP(J,K),K=1,3),
     1    J=1,3)
C
C     THE BOUNDARY CONDITIONS ARE CONSIDERED
C
      DO 334 J=1,4
      NRQ=NOD(I,J)
      DO 331 K=1,NBPTC
      KK=IABS(NODB(K))
      K1=KK/10000
      IF (NRQ .NE. K1) GO TO 331
      XX=1.0
      IF (NODB(K) .LT. 0) XX=0.0
      NODB(K)=-KK
      NR=NU*(J-1)
      IIFLG(1)=MOD(KK,100)/10
      IIFLG(2)=MOD(KK,10)
      IIFLG(3)=IIFLG(1)+IIFLG(2)
      BIVD(1)=BIV(K,1)
```

```
      BIVD(2)=BIV(K,2)
      BIVD(3)=0.0
      IAN=MOD(KK,10000)/100
      ANG=BIV(K,3)
      IF(ANG .EQ. 0.0) GO TO 320
C
C     TRANSFORMATION TO N-S AXES
C
      CA=COS(ANG)
      SA=SIN(ANG)
      D1=ZY(NR+1)
      D2=ZY(NR+2)
      ZY(NR+1)=D1*CA+D2*SA
      ZY(NR+2)=-D1*SA+D2*CA
      DO 315 JJ=1,8
      D1=C1(NR+1,JJ)
      D2=C1(NR+2,JJ)
      C1(NR+1,JJ)=D1*CA+D2*SA
  315 C1(NR+2,JJ)=-D1*SA+D2*CA
      DO 318 II=1,8
      D1=C1(II,NR+1)
      D2=C1(II,NR+2)
      C1(II,NR+1)=D1*CA+D2*SA
  318 C1(II,NR+2)=-D1*SA+D2*CA
  320 DO 330 N=1,NU
      DU1=0.0
      IF(IAN .EQ. IA) DU1=BIVD( N)
      NR=NR+1
C
C     LOADS ADDED IN
C
      ZY(NR)=ZY(NR)+XX*DU1
      IF(IIFLG(N)    .EQ. 0) GO TO 330
C
C     DISPLACEMENTS SPECIFIED
C
      ZY(NR)=DU1*XX
      C1(NR,NR)=0.0
      DO 327 M=1,8
      ZY(M)=ZY(M)-C1(M,NR)*DU1
      C1(M,NR)=0.0
  327 C1(NR,M)=0.0
  330 CONTINUE
  331 CONTINUE
  334 CONTINUE
C
C     THE ELEMENT MATRIX IS NOW ADDED INTO THE SYSTEM MATRIX
C
```

```
      NRCC=0
      IJU=LB1*NEQ
      DO 350 K=1,4
      KK=NOD(I,K)
      NR=NQ(KK)/100-1
      NRM=NR-IJU
      DO 350 M=1,NU
      NRCC=NRCC+1
      NRM=NRM+1
      NCCC=0
      DO 345 L=1,4
      JJ=NOD(I,L)
      NCN=NQ(JJ)/100-NR-M
      DO 345 N=1,NU
      NCCC=NCCC+1
      NCN=NCN+1
      IF (NCN.LT. 1) GO TO 344
      S(NRM,NCN) =S(NRM,NCN) +C1(NRCC,NCCC)
  344 CONTINUE
  345 CONTINUE
  350 SL(NRM) =SL(NRM) +ZY(NRCC)
      RETURN
      END
      SUBROUTINE GEOM(AA,D1,D2,D3)
      COMMON/BLK3/ C1(17,17),ZY(17),XT(3),YT(3),RQ(4),ZQ(4),
     1          NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2           , IS(5), BS(3), AS(3),  RO, J1,
     3           AL(3,3), BT(3,3), GA(3,3) , Z5(12,12), Z4( 12)
     4   ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
C
C     GEOMETRIC PROPERTIES OF ELEMENT CALCULATED
C
      AA=0.0
      D1=0.0
      D2=0.0
      D3=0.0
      DO 110 I=1,3
      J=IS(I+1)
      K=IS(I+2)
      D4=YT(J)-YT(K)
      D5=XT(K)-XT(J)
      AA=AA+XT(I)*D4
      D1=D1+D4*D4
      D2=D2+D4*D5
      D3=D3+D5*D5
      BS(I)=D4
  110 AS(I)=D5
C
```

```
C     CONSTRAINT EQUATIONS NECESSARY FOR CONVERGENCE FORMED
C
      DU=1.0/AA
      IF(J1 .EQ. 2) GO TO 117
      DO 112 I=1,3
      T(I+18,1)=YT(I)*DU
      T(I+24,1)=YT(I)*DU
  112 T(I+21,1)=-XT(I)*DU
      GO TO 140
  117 DO 121 I=1,3
      T(I+19,2)=-XT(I)*DU
      T(I+25,2)=-XT(I)*DU
  121 T(I+22,2)= YT(I)*DU
  140 RETURN
      END
      SUBROUTINE STFSUB
C
C     THIS SUBROUTINE FORMS THE ELEMENT MATRIX FOR A TRIANGULAR
C     ELEMENT
C
      COMMON/BLK1/ X(700),Y(700),NOD(600,4),IX
      COMMON/BLK3/ C1(17,17),ZY(17),XT(3),YT(3),RQ(4),ZQ(4),
     1          NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2           , IS(5), BS(3), AS(3),  RO, J1,
     3           AL(3,3), BT(3,3), GA(3,3) , CT(12,12), ZT( 12)
     4   ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      COMMON/BLK5/ DEN(10),NON(10),GNU(10,10),E(10,10),H(10,10),
     1     ST(600,9),CP(3,3)
      CALL GEOM(AA,D1,D2,D3)
      DO 155 N=1,3
      BN=BS(N)/12.0
      AN=AS(N)/12.0
      DO 150 I=1,3
      AL(N,I)=2.0*BN    *BS(I)
      BT(N,I)=AN    *BS(I)+AS(I)*BN
  150 GA(N,I)=2.0*AN    *AS(I)
      AL(N,N)=D1/12.0
      BT(N,N)=D2/12.0
  155 GA(N,N)=D3/12.0
      DU=0.5/AA
      C11=CP(1,1)*DU
      C12=CP(1,2)*DU
      C13=CP(1,3)*DU
      C22=CP(2,2)*DU
      C23=CP(2,3)*DU
      C33=CP(3,3)*DU
      FY = -RO * AA / 8.0
C
```

```
C     CHECK FOR DATA ERROR
C
      IF(AA.LE.0.0) WRITE(6,911) IX
  911 FORMAT (// 7X 21HDATA ERROR IN ELEMENT  , I4//)
C
C     FORM ELEMENT STIFFNESS MATRIX
C
      DO 250 N=1,3
      DU1 = 1.0
      IF ( N*J1  .LT.  2  .OR.  N*J1  .GT. 4 ) DU1 = 2.0
      BN=BS(N)
      AN=AS(N)
      ZT(N  )=0.0
      ZT ( N+3) = FY * DU1
      ZT(N+6)=0.0
      ZT ( N+9) = 0.0
      DO 250 I=1,3
      D2=-1.0/3.0
      D4=AL(I,N)
      D5=BT(I,N)
      D6=GA(I,N)
      BI=BS(I)
      AI=AS(I)
      X1=BI*BN
      X2=BI*AN
      X3=AI*BN
      X4=AI*AN
      X5=X2+X3
      CT(N,I)=    C11*X1+C13* X5    +C33*X4
      CT(N,I+3)=    C12*X3+C13*X1+C23*X4+C33*X2
      CT(N,I+6)=D2*CT(N,I)
      CT(N,I+9)=D2*CT(N,I+3)
      CT(N+3,I+3)=    C22*X4+C23* X5    +C33*X1
      CT(N+3,I+6)=D2*(C13*X1+C12*X2+     C33*X3+C23*X4)
      CT(N+3,I+9)=D2*CT(N+3,I+3)
      CT(N+6,I+6)=C11*D4+2.0*C13*D5+C33*D6
      CT(N+6,I+9)=C13*D4    +(C12+C33)*D5+C23*D6
  250 CT(N+9,I+9)=C22*D6+2.0*C23*D5+C33*D4
      DO 300 N=1,12
      DO 300 I=N,12
  300 CT(I,N)=CT(N,I)
C
C     SUB-ELEMENT UNKNOWNS TRANSFORMED TO ELEMENT UNKNOWNS
C
      KP=1
      MC=1
      DO 400 K=1,17
      KA=NETCL(K,J1)
```

```
      DO 320 MM=1,KA
      M=ITRW(KB,J1)
      ZY(K)=ZY(K)+ZT(M)*T(KB,J1)
  320 KB=KB+1
      DO 380 L=1,12
      CTP(L,K)=0.0
      MP=MC
      DO 380 MM=1,KA
      M=ITRW(MP,J1)
      CTP(L,K)=CTP(L,K)+CT(L,M)*T(MP,J1)
  380 MP=MP+1
  400 MC=MC+KA
      MC=1
      DO 410 I=1,17
      KA=NETCL(I,J1)
      DO 405 K=1,17
      MP=MC
      DO 405 MM=1,KA
      M=ITRW(MP,J1)
      C1(I,K)=C1(I,K)+CTP(M,K)*T(MP,J1)
  405 MP=MP+1
  410 MC=MC+KA
      RETURN
      END
      SUBROUTINE REDUCI(NN,NCOL)
C
C     THIS SUBROUTINE REDUCES A BLOCK OF EQUATIONS
C
      COMMON/BLK4/ B(112),A(112,56)
      DO 300 N=1,NN
      IF(A(N,1) .EQ. 0.0)GO TO 300
      D    =B(N)/A(N,1)
      B(N)=D
      I=N
      DO 275 L=2,NCOL
      C=A(N,L)/A(N,1)
      I=I+1
      IF (C .EQ. 0.0) GO TO 275
      J=0
      DO 250 K=L,NCOL
      J=J+1
  250 A(I,J)=A(I,J)-C*A(N,K)
      B(I)=B(I)-A(N,L)*D
  275 A(N,L)=C
  300 CONTINUE
      RETURN
      END
      SUBROUTINE BAKSUB(NN,NCOL,LB,NEQ)
```

```
C
C     THIS SUBROUTINE BACK SUBSTITUTES A BLOCK OF EQUATIONS
C
      COMMON/BLK4/ B(112),A(112,56)
      N=NN+1
      DO 450 M=1,NN
      N=N-1
      DU1=B(N)
      IF (A(N,1) .EQ. 0.0) GO TO 430
      L=N
      DO 425 K=2,NCOL
      L=L+1
  425 DU1=DU1-A(N,K)*B(L)
  430 LL=N+NEQ
      A(LL,LP)=DU1
  450 B(N)=DU1
      RETURN
      END
      SUBROUTINE PRINC (XM, XML)
C
C     THIS SUBROUTINE FINDS THE PRINCIPAL COMPONENTS OF A SECOND RANK
C     TENSOR IN TWO-DIMENSIONS
C
      DIMENSION XM(4), XML(4)
      XML(3)=0.0
      DU1=(XM(1)+XM(2))/2.0
      DU2=SQRT(((XM(1)-XM(2))/2.0)**2+XM(3)**2)
      XML(1)=DU1+DU2
      XML(2)=DU1-DU2
      IF (XM(1) .LE. XM(2)) GO TO 705
      DU3=XML(1)-XM(2)
      IF(DU3.EQ.0.0) GO TO 718
      DU2=XM(3)/DU3
      DU1=SQRT(1.0/(1.0+DU2**2))
      DU2=DU2*DU1
      GO TO 716
  705 DU3=XML(1)-XM(1)
      IF(DU3.EQ.0.0) GO TO 718
      DU1=XM(3)/DU3
      DU2=SQRT(1.0/(1.0+DU1**2))
      DU1=DU1*DU2
  716 XML(3)=ATAN2(DU2,DU1)/0.01745329
  718 RETURN
      END
      SUBROUTINE ESTAB
C
C     TRANSFORMATION RELATIONSHIPS BETWEEN ELEMENT AND SUB-ELEMENT
C           UNKNOWNS ESTABLISHED
```

```
C
      COMMON/BLK3/ C1(17,17),ZY(17),RT(3),ZT(3),RQ(4),ZQ(4),
     1          NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2            , IS(5), BS(3), AS(3),  RO, J1,
     3            AL(3,3), BT(3,3), GA(3,3) , Z5(12,12), Z4( 12)
     4   ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      IS(1)=1
      IS(2)=2
      IS(3)=3
      IS(4)=1
      IS(5)=2
      DO 55 I=1,2
      DO 50 J=1,28
      ITRW(J,I)=1
   50 T(J,I)=1.0
      DO 55 J=1,17
   55 NETCL(J,I)=1
      DO 57 I=1,3
      ITRW(I+ 8,1)=I+6
      ITRW(I+12,1)=I+9
      ITRW(I+18,1)=I+6
      ITRW(I+21,1)=I+9
      ITRW(I+24,1)=I+6
      ITRW(I+ 9,2)=I+6
      ITRW(I+13,2)=I+9
      ITRW(I+19,2)=I+9
      ITRW(I+22,2)=I+6
   57 ITRW(I+25,2)=I+9
      NETCL( 9,1)=3
      NETCL(11,1)=3
      NETCL(15,1)=6
      NETCL(16,1)=3
      NETCL(10,2)=3
      NETCL(12,2)=3
      NETCL(16,2)=3
      NETCL(17,2)=6
      ITRW(2,1)=4
      ITRW(3,1)=2
      ITRW(4,1)=5
      ITRW(7,1)=3
      ITRW(8,1)=6
      ITRW(17,1)=7
      ITRW(18,1)=10
      T(5,1)=0.0
      T(6,1)=0.0
      T(12,1)=0.0
      T(16,1)=0.0
      T(28,1)=0.0
```

```
      ITRW(3,2)=2
      ITRW(4,2)=5
      ITRW(5,2)=3
      ITRW(6,2)=6
      ITRW(8,2)=4
      ITRW(17,2)=9
      ITRW(18,2)=12
      T(1,2)=0.0
      T(2,2)=0.0
      T( 9,2)=0.0
      T(13,2)=0.0
      T(19,2)=0.0
      DO 60 I=1,2
      DO 60 J=1,3
      ATOQ(I,J)=0.5
   60 ITOQ(I,J)=J
      ITOQ(1,3)=4
      ITOQ(2,1)=4
      ATOQ(1,1)=1.0
      ATOQ(2,3)=1.0
      RETURN
      END
      SUBROUTINE REINF(MN,HTOP,ND,HTOPP,I,NP)
C
C     THIS SUBROUTINE FORMS THE STRESS STRAIN MATRIX FOR THE COMPOSITE
C
      COMMON/BLK6/AB(10),EB(10),XIB(10),BE(10),DE(10),TE(10),F(3)
     1 ,TK(10)
      CALL INTP1(   EI,GNUI,MN,HTOP,ND,HTOPP,I,NP)
      ALPH=AB(MN)*EB(MN)/(BE(MN)*DE(MN)*EI)
      A11=1./(EI*(1.+ALPH))
      A12=-A11*GNUI
      A13=A12
      A22=A11*(1.+ALPH*(1.-GNUI*GNUI))
      A23=-A11*GNUI*(1.+ALPH*(1.+GNUI))
      A33=A22
      D1=A22*A33-A23*A23
      D2=A13*A23-A12*A33
      D3=A12*A23-A13*A22
      DET=A11*D1+A12*D2+A13*D3
      D4=1.0/DET
      C11=D1*D4
      C12=D2*D4
      C22=(A11*A33 -A13*A13)*D4
      C33=   EI/(2.*(1.+GNUI))
      C6=TE(MN)
      CALL ANISP(C11,C12,C22,C33,C6)
      RETURN
```

```
      END
      SUBROUTINE STREH(DUXX,DUXY,DUYY,DVXX,DVXY,D,MN,HTOP,ND,HTOPP,I,NP)
C
C   THIS SUBROUTINE DETERMINES THE STRESSES IN THE SOIL AND THE STRIP
C
      COMMON/BLK3/ C1(17,17),ZY(17),RT(3),ZT(3),RQ(4),ZQ(4),
     1            NQ(700),U(700),V(700),ITOQ(2,3),ATOQ(2,3),EST(4,3)
     2             , IS(5), BS(3), AS(3),  RO, J1,
     3             AL(3,3), BT(3,3), GA(3,3) , Z5(12,12), Z4( 12)
     4    ,T(28,2), ITRW(28,2), NETCL(17,2), CTP(12,17), STORE(17)
      COMMON/BLK6/AB(10),EB(10),XIB(10),BE(10),DE(10),TE(10),F(3)
     1 ,TK(10)
      DVYY=D
      THETA=TE(MN)*.0174533
      COST=COS(THETA)
      SINT=SIN(THETA)
      E1=RQ(1)*COST*COST+RQ(2)*SINT*SINT+RQ(3)*COST*SINT
      G12=2.*(RQ(2)-RQ(1))*SINT*COST+RQ(3)*(COST*COST-SINT*SINT)
C
C    STRESSES IN COMPOSITE  AXES ALIGNED WITH STRIP
C
      S1=ZQ(1)*COST*COST+ZQ(2)*SINT*SINT+2.*ZQ(3)*SINT*COST
      S2=ZQ(1)*SINT*SINT+ZQ(2)*COST*COST-2.*ZQ(3)*SINT*COST
      T12=SINT*COST*(-ZQ(1)+ZQ(2))+ZQ(3)*(COST*COST-SINT*SINT)
      CALL INTPI(   EI,GNUI,MN,HTOP,ND,HTOPP,I,NP)
      SS=EB(MN)*E1
      S1=S1-SS*AB(MN)/(BE(MN)*DE(MN))
      C2=EI/(2.*(1.+GNUI))
      TA12=C2*G12
C
C     FORCES IN REINFORCING STRIP
C
      F(1)=SS*AB(MN)
      DU1=COST*DVXX+SINT*(-DUXX+2.*DVXY)
      DU2=SINT*DUYY+COST*(2.*DUXY-DVYY)
      DU3=COST*COST*DU1-SINT*SINT*DU2
      F(2)=EB(MN)*XIB(MN)*DU3
      TH=-TE(MN)*.0174533
      COST=COS(TH)
      SINT=SIN(TH)
      ZQ(1)=S1*COST*COST+S2*SINT*SINT+2.*TA12*SINT*COST
      ZQ(2)=S1*SINT*SINT+S2*COST*COST-2.*TA12*SINT*COST
      ZQ(3)=COST*SINT*(-S1+S2)+TA12*(COST*COST-SINT*SINT)
      RETURN
      END
***** ABOVE ACTION SATISFACTORILY COMPLETED *****
```

OUTPUT EXAMPLE

FOR

THE LAST CONSTRUCTION INCREMENT

CONSTRUCTION INCREMENT 12

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | ELEMENT ST GAMA-XY |
|---|---|---|---|---|---|
| 1 | 1.67E 01 | 7.24E 01 | -3.87E-04 | -5.27E-03 | -3.80E-04 |
| 2 | 1.31E 01 | 1.17E 02 | -1.31E-03 | -4.47E-03 | -5.35E-04 |
| 3 | 4.82E 01 | 7.24E 01 | -2.66E-04 | -5.44E-03 | -9.19E-04 |
| 4 | 4.12E 01 | 1.17E 02 | -1.04E-03 | -4.81E-03 | -1.64E-03 |
| 5 | 7.97E 01 | 7.24E 01 | -1.10E-04 | -5.64E-03 | -1.17E-03 |
| 6 | 6.92E 01 | 1.17E 02 | -5.63E-04 | -5.34E-03 | -2.05E-03 |
| 7 | 1.11E 02 | 7.26E 01 | 3.07E-05 | -5.75E-03 | -1.11E-03 |
| 8 | 9.81E 01 | 1.18E 02 | -2.42E-04 | -5.68E-03 | -2.07E-03 |
| 9 | 1.42E 02 | 7.33E 01 | 9.10E-05 | -5.65E-03 | -8.47E-04 |
| 10 | 1.23E 02 | 1.21E 02 | 1.61E-05 | -5.83E-03 | -2.02E-03 |
| 11 | 1.72E 02 | 7.43E 01 | 6.29E-05 | -5.23E-03 | -5.07E-04 |
| 12 | 1.48E 02 | 1.24E 02 | 1.67E-04 | -5.87E-03 | -1.70E-03 |
| 13 | 1.93E 02 | 8.13E 01 | 1.02E-04 | -4.76E-03 | 8.05E-04 |
| 14 | 1.68E 02 | 1.27E 02 | 2.23E-04 | -5.84E-03 | -1.53E-03 |
| 15 | 2.10E 02 | 9.00E 01 | 2.77E-04 | -5.07E-03 | 1.64E-03 |
| 16 | 1.87E 02 | 1.32E 02 | 2.84E-04 | -5.69E-03 | -9.02E-04 |
| 17 | 2.27E 02 | 9.75E 01 | 5.47E-04 | -5.39E-03 | 1.91E-03 |
| 18 | 2.05E 02 | 1.38E 02 | 4.72E-04 | -5.76E-03 | -1.63E-04 |
| 19 | 2.42E 02 | 1.08E 02 | 7.61E-04 | -5.65E-03 | 2.13E-03 |
| 20 | 2.21E 02 | 1.45E 02 | 6.57E-04 | -5.95E-03 | 2.36E-04 |
| 21 | 2.58E 02 | 1.18E 02 | 9.47E-04 | -5.87E-03 | 2.24E-03 |
| 22 | 2.37E 02 | 1.54E 02 | 8.85E-04 | -6.14E-03 | 6.02E-04 |
| 23 | 2.73E 02 | 1.28E 02 | 1.12E-03 | -6.04E-03 | 2.31E-03 |
| 24 | 2.53E 02 | 1.62E 02 | 1.10E-03 | -6.30E-03 | 9.03E-04 |
| 25 | 2.88E 02 | 1.38E 02 | 1.27E-03 | -6.17E-03 | 2.32E-03 |
| 26 | 2.69E 02 | 1.71E 02 | 1.30E-03 | -6.41E-03 | 1.17E-03 |
| 27 | 3.04E 02 | 1.49E 02 | 1.41E-03 | -6.27E-03 | 2.30E-03 |
| 28 | 2.85E 02 | 1.79E 02 | 1.47E-03 | -6.48E-03 | 1.38E-03 |
| 29 | 3.19E 02 | 1.59E 02 | 1.54E-03 | -6.37E-03 | 2.26E-03 |
| 30 | 3.01E 02 | 1.88E 02 | 1.63E-03 | -6.53E-03 | 1.52E-03 |
| 31 | 3.34E 02 | 1.70E 02 | 1.67E-03 | -6.44E-03 | 2.27E-03 |
| 32 | 3.16E 02 | 1.98E 02 | 1.76E-03 | -6.64E-03 | 1.55E-03 |
| 33 | 3.49E 02 | 1.81E 02 | 1.76E-03 | -6.47E-03 | 2.28E-03 |
| 34 | 3.31E 02 | 2.08E 02 | 1.91E-03 | -6.71E-03 | 1.68E-03 |
| 35 | 3.64E 02 | 1.92E 02 | 1.83E-03 | -6.46E-03 | 2.29E-03 |
| 36 | 3.46E 02 | 2.18E 02 | 2.06E-03 | -6.76E-03 | 1.81E-03 |
| 37 | 3.79E 02 | 2.03E 02 | 1.87E-03 | -6.39E-03 | 2.31E-03 |
| 38 | 3.61E 02 | 2.28E 02 | 2.20E-03 | -6.76E-03 | 1.98E-03 |
| 39 | 3.94E 02 | 2.13E 02 | 1.88E-03 | -6.26E-03 | 2.31E-03 |
| 40 | 3.76E 02 | 2.38E 02 | 2.30E-03 | -6.69E-03 | 2.20E-03 |
| 41 | 4.09E 02 | 2.24E 02 | 1.88E-03 | -6.08E-03 | 2.26E-03 |
| 42 | 3.91E 02 | 2.48E 02 | 2.33E-03 | -6.51E-03 | 2.41E-03 |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 1 | -3.56E 03 | -7.32E 03 | -1.46E 02 | -3.56E 03 | -7.32E 03 | -2.23E 00 |
| 2 | -4.34E 03 | -6.77E 03 | -2.06E 02 | -4.32E 03 | -6.78E 03 | -4.80E 00 |
| 3 | -3.50E 03 | -7.48E 03 | -3.53E 02 | -3.47E 03 | -7.51E 03 | -5.04E 00 |
| 4 | -4.17E 03 | -7.07E 03 | -6.30E 02 | -4.04E 03 | -7.20E 03 | -1.18E 01 |
| 5 | -3.40E 03 | -7.66E 03 | -4.51E 02 | -3.35E 03 | -7.70E 03 | -5.99E 00 |
| 6 | -3.84E 03 | -7.51E 03 | -7.89E 02 | -3.67E 03 | -7.67E 03 | -1.16E 01 |
| 7 | -3.27E 03 | -7.72E 03 | -4.27E 02 | -3.23E 03 | -7.76E 03 | -5.44E 00 |
| 8 | -3.60E 03 | -7.79E 03 | -7.97E 02 | -3.46E 03 | -7.93E 03 | -1.04E 01 |
| 9 | -3.13E 03 | -7.55E 03 | -3.26E 02 | -3.11E 03 | -7.57E 03 | -4.20E 00 |
| 10 | -3.34E 03 | -7.84E 03 | -7.77E 02 | -3.21E 03 | -7.97E 03 | -9.54E 00 |
| 11 | -2.93E 03 | -7.01E 03 | -1.95E 02 | -2.93E 03 | -7.02E 03 | -2.74E 00 |
| 12 | -3.16E 03 | -7.81E 03 | -6.54E 02 | -3.07E 03 | -7.90E 03 | -7.86E 00 |
| 13 | -2.61E 03 | -6.35E 03 | 3.10E 02 | -2.58E 03 | -6.38E 03 | 4.70E 00 |
| 14 | -3.07E 03 | -7.73E 03 | -5.87E 02 | -2.99E 03 | -7.80E 03 | -7.07E 00 |
| 15 | -2.55E 03 | -6.67E 03 | 6.32E 02 | -2.46E 03 | -6.76E 03 | 8.54E 00 |
| 16 | -2.90E 03 | -7.50E 03 | -3.47E 02 | -2.87E 03 | -7.52E 03 | -4.29E 00 |
| 17 | -2.37E 03 | -6.94E 03 | 7.35E 02 | -2.26E 03 | -7.05E 03 | 8.92E 00 |
| 18 | -2.69E 03 | -7.48E 03 | -6.28E 01 | -2.69E 03 | -7.48E 03 | -7.50E-01 |
| 19 | -2.24E 03 | -7.17E 03 | 8.21E 02 | -2.10E 03 | -7.30E 03 | 9.20E 00 |
| 20 | -2.55E 03 | -7.64E 03 | 9.07E 01 | -2.55E 03 | -7.64E 03 | 1.02E 00 |
| 21 | -2.11E 03 | -7.36E 03 | 8.63E 02 | -1.97E 03 | -7.50E 03 | 9.11E 00 |
| 22 | -2.35E 03 | -7.75E 03 | 2.32E 02 | -2.34E 03 | -7.76E 03 | 2.45E 00 |
| 23 | -1.98E 03 | -7.49E 03 | 8.87E 02 | -1.84E 03 | -7.63E 03 | 8.93E 00 |
| 24 | -2.16E 03 | -7.84E 03 | 3.47E 02 | -2.13E 03 | -7.86E 03 | 3.48E 00 |
| 25 | -1.85E 03 | -7.57E 03 | 8.93E 02 | -1.72E 03 | -7.71E 03 | 8.67E 00 |
| 26 | -1.95E 03 | -7.88E 03 | 4.51E 02 | -1.91E 03 | -7.91E 03 | 4.32E 00 |
| 27 | -1.72E 03 | -7.63E 03 | 8.85E 02 | -1.59E 03 | -7.76E 03 | 8.34E 00 |
| 28 | -1.76E 03 | -7.87E 03 | 5.33E 02 | -1.71E 03 | -7.92E 03 | 4.94E 00 |
| 29 | -1.60E 03 | -7.69E 03 | 8.68E 02 | -1.48E 03 | -7.81E 03 | 7.96E 00 |
| 30 | -1.57E 03 | -7.85E 03 | 5.86E 02 | -1.52E 03 | -7.90E 03 | 5.29E 00 |
| 31 | -1.46E 03 | -7.71E 03 | 8.72E 02 | -1.35E 03 | -7.82E 03 | 7.80E 00 |
| 32 | -1.46E 03 | -7.92E 03 | 5.97E 02 | -1.40E 03 | -7.97E 03 | 5.23E 00 |
| 33 | -1.36E 03 | -7.70E 03 | 8.76E 02 | -1.24E 03 | -7.82E 03 | 7.73E 00 |
| 34 | -1.30E 03 | -7.93E 03 | 6.45E 02 | -1.24E 03 | -7.99E 03 | 5.50E 00 |
| 35 | -1.27E 03 | -7.64E 03 | 8.82E 02 | -1.15E 03 | -7.76E 03 | 7.73E 00 |
| 36 | -1.12E 03 | -7.90E 03 | 6.97E 02 | -1.05E 03 | -7.98E 03 | 5.81E 00 |
| 37 | -1.17E 03 | -7.53E 03 | 8.88E 02 | -1.05E 03 | -7.65E 03 | 7.80E 00 |
| 38 | -9.40E 02 | -7.83E 03 | 7.63E 02 | -8.57E 02 | -7.91E 03 | 6.24E 00 |
| 39 | -1.08E 03 | -7.34E 03 | 8.88E 02 | -9.52E 02 | -7.47E 03 | 7.91E 00 |
| 40 | -7.70E 02 | -7.69E 03 | 8.47E 02 | -6.68E 02 | -7.79E 03 | 6.88E 00 |
| 41 | -9.84E 02 | -7.11E 03 | 8.69E 02 | -8.63E 02 | -7.23E 03 | 7.93E 00 |
| 42 | -6.23E 02 | -7.43E 03 | 9.26E 02 | -4.99E 02 | -7.55E 03 | 7.62E 00 |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 43 | 4.22E 02 | 2.34E 02 | 1.86E-03 | -5.84E-03 | 2.22E-03 |
| 44 | 4.04E 02 | 2.58E 02 | 2.26E-03 | -6.31E-03 | 2.43E-03 |
| 45 | 4.33E 02 | 2.42E 02 | 1.82E-03 | -5.60E-03 | 2.07E-03 |
| 46 | 4.14E 02 | 2.66E 02 | 2.17E-03 | -6.01E-03 | 2.41E-03 |
| 47 | 4.43E 02 | 2.50E 02 | 1.80E-03 | -5.32E-03 | 1.80E-03 |
| 48 | 4.25E 02 | 2.74E 02 | 2.03E-03 | -5.63E-03 | 2.23E-03 |
| 49 | 4.53E 02 | 2.58E 02 | 1.80E-03 | -5.04E-03 | 1.39E-03 |
| 50 | 4.35E 02 | 2.82E 02 | 1.85E-03 | -5.18E-03 | 1.83E-03 |
| 51 | 4.64E 02 | 2.66E 02 | 1.84E-03 | -4.78E-03 | 8.01E-04 |
| 52 | 4.46E 02 | 2.90E 02 | 1.62E-03 | -4.67E-03 | 1.22E-03 |
| 53 | 4.74E 02 | 2.74E 02 | 1.93E-03 | -4.55E-03 | 3.21E-06 |
| 54 | 4.56E 02 | 2.98E 02 | 1.34E-03 | -4.10E-03 | 4.40E-04 |
| 55 | 4.85E 02 | 2.81E 02 | 2.10E-03 | -4.44E-03 | -1.10E-03 |
| 56 | 4.66E 02 | 3.07E 02 | 9.11E-04 | -3.40E-03 | -4.63E-04 |
| 57 | 4.95E 02 | 2.90E 02 | 2.16E-03 | -4.09E-03 | -2.66E-03 |
| 58 | 4.77E 02 | 3.15E 02 | 2.21E-04 | -2.78E-03 | -8.05E-04 |
| 59 | 5.07E 02 | 2.98E 02 | -2.41E-04 | -4.15E-03 | -6.98E-03 |
| 60 | 4.89E 02 | 3.24E 02 | 5.78E-04 | -2.53E-03 | -3.24E-04 |
| 61 | 5.20E 02 | 3.08E 02 | -6.46E-04 | -2.59E-03 | -6.30E-03 |
| 62 | 5.02E 02 | 3.34E 02 | 6.85E-04 | -2.67E-03 | -1.71E-03 |
| 63 | 5.33E 02 | 3.18E 02 | -8.07E-04 | -1.90E-03 | -5.17E-03 |
| 64 | 5.15E 02 | 3.43E 02 | 6.84E-04 | -2.42E-03 | -2.75E-03 |
| 65 | 5.46E 02 | 3.28E 02 | -5.86E-04 | -1.88E-03 | -3.86E-03 |
| 66 | 5.28E 02 | 3.53E 02 | 8.19E-04 | -2.50E-03 | -3.01E-03 |
| 67 | 5.59E 02 | 3.37E 02 | 3.84E-04 | -3.02E-03 | -1.94E-03 |
| 68 | 5.42E 02 | 3.63E 02 | 1.16E-03 | -2.67E-03 | -3.46E-03 |
| 69 | 5.69E 02 | 3.50E 02 | 1.66E-03 | -4.37E-03 | -8.43E-04 |
| 70 | 5.66E 02 | 3.82E 02 | 2.64E-03 | -6.12E-03 | -1.54E-03 |
| 71 | 1.31E 01 | 1.45E 02 | -2.34E-03 | -7.39E-03 | -1.55E-03 |
| 72 | 3.98E 01 | 1.45E 02 | -1.53E-03 | -8.32E-03 | -4.06E-03 |
| 73 | 6.94E 01 | 1.44E 02 | -1.36E-03 | -9.66E-03 | -5.44E-03 |
| 74 | 8.83E 01 | 1.51E 02 | -5.40E-04 | -1.00E-02 | -5.27E-03 |
| 75 | 1.16E 02 | 1.48E 02 | 1.31E-04 | -1.08E-02 | -4.92E-03 |
| 76 | 1.08E 02 | 1.59E 02 | -2.13E-04 | -1.06E-02 | -5.75E-03 |
| 77 | 1.35E 02 | 1.52E 02 | 3.13E-04 | -1.09E-02 | -4.74E-03 |
| 78 | 1.26E 02 | 1.69E 02 | 2.14E-04 | -1.10E-02 | -5.75E-03 |
| 79 | 1.53E 02 | 1.60E 02 | 6.69E-04 | -1.11E-02 | -4.24E-03 |
| 80 | 1.43E 02 | 1.78E 02 | 5.87E-04 | -1.13E-02 | -5.74E-03 |
| 81 | 1.70E 02 | 1.65E 02 | 9.09E-04 | -1.13E-02 | -3.95E-03 |
| 82 | 1.59E 02 | 1.85E 02 | 1.02E-03 | -1.16E-02 | -5.29E-03 |
| 83 | 1.88E 02 | 1.69E 02 | 1.09E-03 | -1.12E-02 | -3.12E-03 |
| 84 | 1.75E 02 | 1.92E 02 | 1.39E-03 | -1.19E-02 | -4.87E-03 |
| 85 | 2.04E 02 | 1.76E 02 | 1.54E-03 | -1.13E-02 | -1.85E-03 |
| 86 | 1.91E 02 | 2.00E 02 | 1.68E-03 | -1.21E-02 | -4.32E-03 |
| 87 | 2.20E 02 | 1.84E 02 | 1.92E-03 | -1.17E-02 | -1.09E-03 |
| 88 | 2.06E 02 | 2.07E 02 | 2.06E-03 | -1.23E-02 | -3.47E-03 |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 43 | -8.62E 02 | -6.79E 03 | 8.54E 02 | -7.42E 02 | -6.91E 03 | 8.03E 00 |
| 44 | -5.94E 02 | -7.19E 03 | 9.34E 02 | -4.64E 02 | -7.31E 03 | 7.92E 00 |
| 45 | -7.76E 02 | -6.48E 03 | 7.96E 02 | -6.66E 02 | -6.59E 03 | 7.80E 00 |
| 46 | -5.44E 02 | -6.83E 03 | 9.28E 02 | -4.09E 02 | -6.97E 03 | 8.22E 00 |
| 47 | -6.52E 02 | -6.13E 03 | 6.92E 02 | -5.65E 02 | -6.22E 03 | 7.09E 00 |
| 48 | -5.14E 02 | -6.40E 03 | 8.56E 02 | -3.92E 02 | -6.53E 03 | 8.10E 00 |
| 49 | -4.89E 02 | -5.75E 03 | 5.34E 02 | -4.36E 02 | -5.80E 03 | 5.74E 00 |
| 50 | -4.97E 02 | -5.91E 03 | 7.03E 02 | -4.07E 02 | -6.00E 03 | 7.28E 00 |
| 51 | -2.81E 02 | -5.37E 03 | 3.08E 02 | -2.63E 02 | -5.39E 03 | 3.45E 00 |
| 52 | -5.05E 02 | -5.34E 03 | 4.70E 02 | -4.60E 02 | -5.39E 03 | 5.49E 00 |
| 53 | -2.69E 01 | -5.01E 03 | 1.24E 00 | -2.69E 01 | -5.01E 03 | 1.42E-02 |
| 54 | -5.68E 02 | -4.75E 03 | 1.69E 02 | -5.61E 02 | -4.76E 03 | 2.31E 00 |
| 55 | 2.67E 02 | -4.76E 03 | -4.22E 02 | 3.02E 02 | -4.80E 03 | -4.77E 00 |
| 56 | -7.36E 02 | -4.05E 03 | -1.78E 02 | -7.27E 02 | -4.06E 03 | -3.06E 00 |
| 57 | 5.46E 02 | -4.26E 03 | -1.02E 03 | 7.56E 02 | -4.46E 03 | -1.15E 01 |
| 58 | -1.31E 03 | -3.61E 03 | -3.10E 02 | -1.26E 03 | -3.65E 03 | -7.52E 00 |
| 59 | -2.72E 03 | -5.73E 03 | -2.69E 03 | -1.14E 03 | -7.30E 03 | -3.04E 01 |
| 60 | -6.84E 02 | -3.08E 03 | -1.24E 02 | -6.77E 02 | -3.08E 03 | -2.97E 00 |
| 61 | -2.37E 03 | -3.86E 03 | -2.42E 03 | -5.81E 02 | -5.65E 03 | -3.64E 01 |
| 62 | -6.22E 02 | -3.21E 03 | -6.60E 02 | -4.63E 02 | -3.36E 03 | -1.35E 01 |
| 63 | -2.18E 03 | -3.03E 03 | -1.99E 03 | -5.75E 02 | -4.64E 03 | -3.90E 01 |
| 64 | -4.76E 02 | -2.86E 03 | -1.06E 03 | -7.39E 01 | -3.27E 03 | -2.08E 01 |
| 65 | -1.87E 03 | -2.87E 03 | -1.49E 03 | -8.02E 02 | -3.94E 03 | -3.58E 01 |
| 66 | -3.38E 02 | -2.89E 03 | -1.16E 03 | 1.09E 02 | -3.33E 03 | -2.11E 01 |
| 67 | -1.22E 03 | -3.84E 03 | -7.47E 02 | -1.03E 03 | -4.04E 03 | -1.49E 01 |
| 68 | 1.59E 01 | -2.93E 03 | -1.33E 03 | 5.29E 02 | -3.44E 03 | -2.11E 01 |
| 69 | -2.91E 02 | -4.93E 03 | -3.24E 02 | -2.69E 02 | -4.95E 03 | -3.98E 00 |
| 70 | 2.79E 01 | -6.71E 03 | -5.93E 02 | 7.97E 01 | -6.77E 03 | -4.99E 00 |
| 71 | -4.11E 03 | -6.27E 03 | -3.30E 02 | -4.06E 03 | -6.32E 03 | -8.51E 00 |
| 72 | -3.80E 03 | -6.70E 03 | -8.67E 02 | -3.56E 03 | -6.94E 03 | -1.54E 01 |
| 73 | -4.11E 03 | -7.66E 03 | -1.16E 03 | -3.77E 03 | -8.00E 03 | -1.66E 01 |
| 74 | -3.61E 03 | -7.65E 03 | -1.12E 03 | -3.31E 03 | -7.94E 03 | -1.45E 01 |
| 75 | -3.35E 03 | -8.01E 03 | -1.05E 03 | -3.13E 03 | -8.23E 03 | -1.21E 01 |
| 76 | -3.56E 03 | -8.00E 03 | -1.23E 03 | -3.24E 03 | -8.32E 03 | -1.45E 01 |
| 77 | -3.26E 03 | -8.04E 03 | -1.01E 03 | -3.05E 03 | -8.25E 03 | -1.15E 01 |
| 78 | -3.36E 03 | -8.14E 03 | -1.23E 03 | -3.06E 03 | -8.43E 03 | -1.36E 01 |
| 79 | -3.04E 03 | -8.06E 03 | -9.06E 02 | -2.89E 03 | -8.21E 03 | -9.94E 00 |
| 80 | -3.17E 03 | -8.24E 03 | -1.23E 03 | -2.89E 03 | -8.52E 03 | -1.29E 01 |
| 81 | -2.94E 03 | -8.14E 03 | -8.43E 02 | -2.80E 03 | -8.28E 03 | -8.97E 00 |
| 82 | -2.95E 03 | -8.33E 03 | -1.13E 03 | -2.72E 03 | -8.55E 03 | -1.14E 01 |
| 83 | -2.78E 03 | -8.04E 03 | -6.66E 02 | -2.70E 03 | -8.12E 03 | -7.10E 00 |
| 84 | -2.76E 03 | -8.42E 03 | -1.04E 03 | -2.58E 03 | -8.61E 03 | -1.01E 01 |
| 85 | -2.47E 03 | -7.97E 03 | -3.95E 02 | -2.44E 03 | -8.00E 03 | -4.09E 00 |
| 86 | -2.61E 03 | -8.47E 03 | -9.21E 02 | -2.47E 03 | -8.61E 03 | -8.72E 00 |
| 87 | -2.31E 03 | -8.14E 03 | -2.32E 02 | -2.30E 03 | -8.15E 03 | -2.28E 00 |
| 88 | -2.40E 03 | -8.54E 03 | -7.41E 02 | -2.31E 03 | -8.63E 03 | -6.79E 00 |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 89 | 2.36E 02 | 1.91E 02 | 2.24E-03 | -1.19E-02 | -5.18E-04 |
| 90 | 2.22E 02 | 2.15E 02 | 2.47E-03 | -1.26E-02 | -2.53E-03 |
| 91 | 2.52E 02 | 1.99E 02 | 2.52E-03 | -1.21E-02 | -1.28E-04 |
| 92 | 2.37E 02 | 2.23E 02 | 2.83E-03 | -1.26E-02 | -1.70E-03 |
| 93 | 2.68E 02 | 2.07E 02 | 2.81E-03 | -1.23E-02 | 3.70E-04 |
| 94 | 2.53E 02 | 2.31E 02 | 3.16E-03 | -1.29E-02 | -1.38E-03 |
| 95 | 2.85E 02 | 2.12E 02 | 3.07E-03 | -1.23E-02 | 8.61E-04 |
| 96 | 2.71E 02 | 2.35E 02 | 3.36E-03 | -1.29E-02 | -5.78E-04 |
| 97 | 2.64E 02 | 2.51E 02 | 3.33E-03 | -1.32E-02 | -1.56E-03 |
| 98 | 3.01E 02 | 2.21E 02 | 3.35E-03 | -1.23E-02 | 1.49E-03 |
| 99 | 2.88E 02 | 2.41E 02 | 3.56E-03 | -1.28E-02 | 1.29E-05 |
| 100 | 2.77E 02 | 2.57E 02 | 3.71E-03 | -1.32E-02 | -1.12E-03 |
| 101 | 3.16E 02 | 2.31E 02 | 3.69E-03 | -1.25E-02 | 1.67E-03 |
| 102 | 3.03E 02 | 2.50E 02 | 3.86E-03 | -1.29E-02 | 2.53E-04 |
| 103 | 2.92E 02 | 2.66E 02 | 4.07E-03 | -1.33E-02 | -8.84E-04 |
| 104 | 3.31E 02 | 2.41E 02 | 4.02E-03 | -1.27E-02 | 1.82E-03 |
| 105 | 3.17E 02 | 2.60E 02 | 4.23E-03 | -1.31E-02 | 4.34E-04 |
| 106 | 3.06E 02 | 2.76E 02 | 4.42E-03 | -1.34E-02 | -7.18E-04 |
| 107 | 3.46E 02 | 2.51E 02 | 4.33E-03 | -1.29E-02 | 2.08E-03 |
| 108 | 3.32E 02 | 2.70E 02 | 4.67E-03 | -1.34E-02 | 6.64E-04 |
| 109 | 3.21E 02 | 2.85E 02 | 4.83E-03 | -1.36E-02 | -6.72E-04 |
| 110 | 3.60E 02 | 2.60E 02 | 4.60E-03 | -1.29E-02 | 2.49E-03 |
| 111 | 3.47E 02 | 2.80E 02 | 5.13E-03 | -1.36E-02 | 1.11E-03 |
| 112 | 3.35E 02 | 2.95E 02 | 5.37E-03 | -1.41E-02 | -5.19E-04 |
| 113 | 3.75E 02 | 2.70E 02 | 4.76E-03 | -1.28E-02 | 3.14E-03 |
| 114 | 3.61E 02 | 2.89E 02 | 5.59E-03 | -1.39E-02 | 1.72E-03 |
| 115 | 3.50E 02 | 3.05E 02 | 5.87E-03 | -1.43E-02 | -1.11E-04 |
| 116 | 3.88E 02 | 2.79E 02 | 4.81E-03 | -1.24E-02 | 4.03E-03 |
| 117 | 3.74E 02 | 2.98E 02 | 6.01E-03 | -1.41E-02 | 2.78E-03 |
| 118 | 3.62E 02 | 3.14E 02 | 6.74E-03 | -1.54E-02 | 8.48E-05 |
| 119 | 3.98E 02 | 2.87E 02 | 4.69E-03 | -1.20E-02 | 4.67E-03 |
| 120 | 3.84E 02 | 3.06E 02 | 6.08E-03 | -1.38E-02 | 4.21E-03 |
| 121 | 3.73E 02 | 3.21E 02 | 7.38E-03 | -1.59E-02 | 2.30E-03 |
| 122 | 4.09E 02 | 2.95E 02 | 4.35E-03 | -1.11E-02 | 5.02E-03 |
| 123 | 3.95E 02 | 3.14E 02 | 5.85E-03 | -1.31E-02 | 5.71E-03 |
| 124 | 3.84E 02 | 3.29E 02 | 7.30E-03 | -1.54E-02 | 4.51E-03 |
| 125 | 4.19E 02 | 3.04E 02 | 3.89E-03 | -1.00E-02 | 4.89E-03 |
| 126 | 4.06E 02 | 3.22E 02 | 5.32E-03 | -1.17E-02 | 6.61E-03 |
| 127 | 3.95E 02 | 3.37E 02 | 7.09E-03 | -1.43E-02 | 6.01E-03 |
| 128 | 4.30E 02 | 3.12E 02 | 3.45E-03 | -8.91E-03 | 4.39E-03 |
| 129 | 4.16E 02 | 3.30E 02 | 4.89E-03 | -1.01E-02 | 6.27E-03 |
| 130 | 4.06E 02 | 3.45E 02 | 7.40E-03 | -1.23E-02 | 7.13E-03 |
| 131 | 4.40E 02 | 3.20E 02 | 3.02E-03 | -7.71E-03 | 3.80E-03 |
| 132 | 4.27E 02 | 3.38E 02 | 5.02E-03 | -9.20E-03 | 5.83E-03 |
| 133 | 4.17E 02 | 3.52E 02 | 8.52E-03 | -1.13E-02 | 8.44E-03 |
| 134 | 4.51E 02 | 3.28E 02 | 2.67E-03 | -6.67E-03 | 3.44E-03 |
| 135 | 4.38E 02 | 3.46E 02 | 5.08E-03 | -8.23E-03 | 5.36E-03 |
| 136 | 4.28E 02 | 3.60E 02 | 6.82E-03 | -9.65E-03 | 9.71E-03 |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 89 | -2.15E 03 | -8.19E 03 | -1.11E 02 | -2.15E 03 | -8.19E 03 | -1.05E 00 |
| 90 | -2.19E 03 | -8.63E 03 | -5.41E 02 | -2.15E 03 | -8.68E 03 | -4.77E 00 |
| 91 | -2.01E 03 | -8.27E 03 | -2.73E 01 | -2.01E 03 | -8.27E 03 | -2.50E-01 |
| 92 | -1.93E 03 | -8.54E 03 | -3.64E 02 | -1.91E 03 | -8.56E 03 | -3.14E 00 |
| 93 | -1.83E 03 | -8.27E 03 | 7.90E 01 | -1.83E 03 | -8.27E 03 | 7.02E-01 |
| 94 | -1.78E 03 | -8.64E 03 | -2.94E 02 | -1.77E 03 | -8.66E 03 | -2.45E 00 |
| 95 | -1.65E 03 | -8.22E 03 | 1.84E 02 | -1.64E 03 | -8.22E 03 | 1.60E 00 |
| 96 | -1.62E 03 | -8.56E 03 | -1.23E 02 | -1.62E 03 | -8.56E 03 | -1.02E 00 |
| 97 | -1.74E 03 | -8.79E 03 | -3.34E 02 | -1.72E 03 | -8.81E 03 | -2.70E 00 |
| 98 | -1.44E 03 | -8.12E 03 | 3.18E 02 | -1.42E 03 | -8.13E 03 | 2.72E 00 |
| 99 | -1.44E 03 | -8.43E 03 | 2.76E 00 | -1.44E 03 | -8.43E 03 | 2.26E-02 |
| 100 | -1.44E 03 | -8.65E 03 | -2.40E 02 | -1.44E 03 | -8.66E 03 | -1.91E 00 |
| 101 | -1.25E 03 | -8.17E 03 | 3.56E 02 | -1.23E 03 | -8.19E 03 | 2.94E 00 |
| 102 | -1.25E 03 | -8.40E 03 | 5.39E 01 | -1.25E 03 | -8.40E 03 | 4.32E-01 |
| 103 | -1.21E 03 | -8.62E 03 | -1.89E 02 | -1.21E 03 | -8.62E 03 | -1.46E 00 |
| 104 | -1.06E 03 | -8.21E 03 | 3.89E 02 | -1.04E 03 | -8.23E 03 | 3.11E 00 |
| 105 | -1.03E 03 | -8.42E 03 | 9.27E 01 | -1.03E 03 | -8.42E 03 | 7.18E-01 |
| 106 | -9.90E 02 | -8.60E 03 | -1.53E 02 | -9.87E 02 | -8.61E 03 | -1.15E 00 |
| 107 | -8.78E 02 | -8.21E 03 | 4.45E 02 | -8.51E 02 | -8.24E 03 | 3.46E 00 |
| 108 | -7.91E 02 | -8.49E 03 | 1.42E 02 | -7.88E 02 | -8.49E 03 | 1.05E 00 |
| 109 | -7.55E 02 | -8.63E 03 | -1.44E 02 | -7.53E 02 | -8.64E 03 | -1.04E 00 |
| 110 | -7.03E 02 | -8.19E 03 | 5.32E 02 | -6.65E 02 | -8.23E 03 | 4.04E 00 |
| 111 | -5.29E 02 | -8.53E 03 | 2.37E 02 | -5.22E 02 | -8.54E 03 | 1.69E 00 |
| 112 | -5.21E 02 | -8.85E 03 | -1.11E 02 | -5.20E 02 | -8.85E 03 | -7.62E-01 |
| 113 | -5.47E 02 | -8.05E 03 | 6.71E 02 | -4.87E 02 | -8.11E 03 | 5.07E 00 |
| 114 | -2.74E 02 | -8.60E 03 | 3.67E 02 | -2.58E 02 | -8.61E 03 | 2.52E 00 |
| 115 | -2.06E 02 | -8.84E 03 | -2.37E 01 | -2.06E 02 | -8.84E 03 | -1.58E-01 |
| 116 | -3.89E 02 | -7.76E 03 | 8.61E 02 | -2.90E 02 | -7.85E 03 | 6.58E 00 |
| 117 | -1.23E 01 | -8.58E 03 | 5.93E 02 | 2.85E 01 | -8.62E 03 | 3.94E 00 |
| 118 | 1.13E 02 | -9.33E 03 | 1.81E 01 | 1.13E 02 | -9.33E 03 | 1.10E-01 |
| 119 | -3.29E 02 | -7.44E 03 | 9.96E 02 | -1.92E 02 | -7.58E 03 | 7.82E 00 |
| 120 | 1.15E 02 | -8.39E 03 | 8.99E 02 | 2.09E 02 | -8.48E 03 | 5.97E 00 |
| 121 | 4.37E 02 | -9.48E 03 | 4.91E 02 | 4.62E 02 | -9.51E 03 | 2.83E 00 |
| 122 | -3.10E 02 | -6.92E 03 | 1.07E 03 | -1.41E 02 | -7.09E 03 | 8.99E 00 |
| 123 | 1.83E 02 | -7.90E 03 | 1.22E 03 | 3.63E 02 | -8.08E 03 | 8.39E 00 |
| 124 | 5.10E 02 | -9.19E 03 | 9.62E 02 | 6.05E 02 | -9.29E 03 | 5.61E 00 |
| 125 | -3.06E 02 | -6.26E 03 | 1.04E 03 | -1.28E 02 | -6.43E 03 | 9.67E 00 |
| 126 | 2.40E 02 | -7.00E 03 | 1.41E 03 | 5.05E 02 | -7.27E 03 | 1.06E 01 |
| 127 | 7.07E 02 | -8.44E 03 | 1.28E 03 | 8.84E 02 | -8.62E 03 | 7.83E 00 |
| 128 | -2.76E 02 | -5.55E 03 | 9.36E 02 | -1.15E 02 | -5.71E 03 | 9.77E 00 |
| 129 | 4.13E 02 | -6.00E 03 | 1.34E 03 | 6.81E 02 | -6.26E 03 | 1.13E 01 |
| 130 | 1.60E 03 | -6.79E 03 | 1.52E 03 | 1.87E 03 | -7.06E 03 | 9.97E 00 |
| 131 | -2.10E 02 | -4.79E 03 | 8.10E 02 | -7.11E 01 | -4.93E 03 | 9.74E 00 |
| 132 | 8.07E 02 | -5.27E 03 | 1.24E 03 | 1.05E 03 | -5.51E 03 | 1.11E 01 |
| 133 | 2.75E 03 | -5.72E 03 | 1.80E 03 | 3.11E 03 | -6.09E 03 | 1.15E 01 |
| 134 | -1.44E 02 | -4.13E 03 | 7.35E 02 | -1.32E 01 | -4.26E 03 | 1.01E 01 |
| 135 | 1.16E 03 | -4.52E 03 | 1.36E 03 | 1.46E 03 | -4.83E 03 | 1.28E 01 |
| 136 | 2.00E 03 | -5.03E 03 | 2.07E 03 | 2.57E 03 | -5.59E 03 | 1.53E 01 |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 137 | 4.61E 02 | 3.36E 02 | 2.78E-03 | -5.87E-03 | 3.13E-03 |
| 138 | 4.48E 02 | 3.54E 02 | 4.44E-03 | -6.88E-03 | 6.41E-03 |
| 139 | 4.39E 02 | 3.68E 02 | 6.04E-03 | -7.84E-03 | 9.48E-03 |
| 140 | 4.73E 02 | 3.45E 02 | 2.33E-03 | -4.82E-03 | 1.98E-03 |
| 141 | 4.60E 02 | 3.63E 02 | 3.94E-03 | -5.42E-03 | 5.78E-03 |
| 142 | 4.50E 02 | 3.76E 02 | 5.66E-03 | -6.40E-03 | 8.96E-03 |
| 143 | 4.86E 02 | 3.55E 02 | 2.24E-03 | -3.88E-03 | 9.56E-04 |
| 144 | 4.73E 02 | 3.72E 02 | 3.50E-03 | -3.99E-03 | 4.48E-03 |
| 145 | 4.62E 02 | 3.85E 02 | 5.11E-03 | -4.49E-03 | 8.38E-03 |
| 146 | 4.99E 02 | 3.64E 02 | 2.52E-03 | -3.70E-03 | -5.41E-04 |
| 147 | 4.85E 02 | 3.82E 02 | 3.44E-03 | -3.11E-03 | 2.67E-03 |
| 148 | 4.74E 02 | 3.94E 02 | 4.62E-03 | -2.74E-03 | 7.28E-03 |
| 149 | 5.12E 02 | 3.74E 02 | 2.98E-03 | -3.79E-03 | -1.88E-03 |
| 150 | 4.98E 02 | 3.91E 02 | 3.61E-03 | -2.97E-03 | 8.92E-04 |
| 151 | 4.86E 02 | 4.03E 02 | 3.60E-03 | -1.30E-03 | 3.90E-03 |
| 152 | 5.26E 02 | 3.85E 02 | 3.11E-03 | -4.28E-03 | -1.87E-03 |
| 153 | 5.11E 02 | 4.02E 02 | 4.44E-03 | -3.72E-03 | 7.02E-04 |
| 154 | 5.01E 02 | 4.08E 02 | 5.09E-03 | -3.50E-03 | 1.06E-03 |
| 155 | 5.43E 02 | 3.95E 02 | 4.32E-03 | -6.22E-03 | -2.76E-03 |
| 156 | 5.31E 02 | 4.06E 02 | 5.69E-03 | -5.60E-03 | -1.50E-03 |
| 157 | 1.77E 01 | 1.54E 02 | -2.79E-03 | -1.28E-02 | -4.65E-03 |
| 158 | 1.24E 01 | 1.68E 02 | -5.56E-03 | -4.85E-03 | -4.70E-03 |
| 159 | 4.30E 01 | 1.56E 02 | -2.21E-03 | -1.35E-02 | -7.87E-03 |
| 160 | 3.98E 01 | 1.81E 02 | -4.28E-03 | -3.80E-03 | -7.80E-03 |
| 161 | 6.51E 01 | 1.65E 02 | -1.00E-03 | -1.40E-02 | -7.18E-03 |
| 162 | 5.97E 01 | 1.87E 02 | -4.82E-03 | -3.34E-03 | -6.37E-03 |
| 163 | 8.22E 01 | 1.72E 02 | -3.61E-04 | -1.53E-02 | -8.30E-03 |
| 164 | 7.58E 01 | 1.93E 02 | -4.87E-03 | -4.19E-03 | -8.61E-03 |
| 165 | 9.92E 01 | 1.80E 02 | 4.78E-04 | -1.61E-02 | -7.99E-03 |
| 166 | 9.17E 01 | 2.02E 02 | -3.61E-03 | -5.19E-03 | -1.03E-02 |
| 167 | 1.17E 02 | 1.90E 02 | 1.35E-03 | -1.70E-02 | -7.99E-03 |
| 168 | 1.08E 02 | 2.10E 02 | -2.82E-03 | -5.57E-03 | -9.35E-03 |
| 169 | 1.33E 02 | 1.98E 02 | 2.25E-03 | -1.79E-02 | -8.13E-03 |
| 170 | 1.23E 02 | 2.18E 02 | -2.28E-03 | -6.08E-03 | -9.15E-03 |
| 171 | 1.48E 02 | 2.06E 02 | 2.85E-03 | -1.87E-02 | -7.83E-03 |
| 172 | 1.37E 02 | 2.27E 02 | -1.87E-03 | -6.35E-03 | -8.72E-03 |
| 173 | 1.63E 02 | 2.14E 02 | 3.40E-03 | -1.95E-02 | -7.40E-03 |
| 174 | 1.52E 02 | 2.35E 02 | -1.51E-03 | -6.62E-03 | -8.18E-03 |
| 175 | 1.78E 02 | 2.22E 02 | 3.90E-03 | -2.02E-02 | -6.87E-03 |
| 176 | 1.66E 02 | 2.43E 02 | -1.18E-03 | -6.84E-03 | -7.58E-03 |
| 177 | 1.93E 02 | 2.30E 02 | 4.35E-03 | -2.08E-02 | -6.31E-03 |
| 178 | 1.81E 02 | 2.52E 02 | -8.37E-04 | -7.07E-03 | -6.80E-03 |
| 179 | 2.08E 02 | 2.38E 02 | 4.95E-03 | -2.18E-02 | -5.66E-03 |
| 180 | 1.95E 02 | 2.60E 02 | -5.60E-04 | -7.00E-03 | -6.22E-03 |
| 181 | 2.25E 02 | 2.42E 02 | 5.46E-03 | -2.30E-02 | -4.63E-03 |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 137 | 1.98E 02 | -3.50E 03 | 6.68E 02 | 3.15E 02 | -3.61E 03 | 9.94E 00 |
| 138 | 1.11E 03 | -3.72E 03 | 1.37E 03 | 1.47E 03 | -4.08E 03 | 1.48E 01 |
| 139 | 2.01E 03 | -3.92E 03 | 2.02E 03 | 2.63E 03 | -4.54E 03 | 1.72E 01 |
| 140 | 2.01E 02 | -2.85E 03 | 4.24E 02 | 2.59E 02 | -2.91E 03 | 7.75E 00 |
| 141 | 1.21E 03 | -2.79E 03 | 1.23E 03 | 1.56E 03 | -3.14E 03 | 1.58E 01 |
| 142 | 2.17E 03 | -2.97E 03 | 1.91E 03 | 2.81E 03 | -3.61E 03 | 1.83E 01 |
| 143 | 4.33E 02 | -2.18E 03 | 2.04E 02 | 4.49E 02 | -2.20E 03 | 4.44E 00 |
| 144 | 1.34E 03 | -1.86E 03 | 9.56E 02 | 1.60E 03 | -2.12E 03 | 1.54E 01 |
| 145 | 2.38E 03 | -1.72E 03 | 1.79E 03 | 3.05E 03 | -2.39E 03 | 2.05E 01 |
| 146 | 6.93E 02 | -1.96E 03 | -1.16E 02 | 6.98E 02 | -1.97E 03 | -2.49E 00 |
| 147 | 1.57E 03 | -1.22E 03 | 5.71E 02 | 1.69E 03 | -1.33E 03 | 1.11E 01 |
| 148 | 2.58E 03 | -5.63E 02 | 1.55E 03 | 3.22E 03 | -1.20E 03 | 2.23E 01 |
| 149 | 1.01E 03 | -1.88E 03 | -4.02E 02 | 1.06E 03 | -1.94E 03 | -7.77E 00 |
| 150 | 1.74E 03 | -1.07E 03 | 1.90E 02 | 1.76E 03 | -1.08E 03 | 3.86E 00 |
| 151 | 2.27E 03 | 1.83E 02 | 8.32E 02 | 2.56E 03 | -1.08E 02 | 1.92E 01 |
| 152 | 9.54E 02 | -2.20E 03 | -4.00E 02 | 1.00E 03 | -2.25E 03 | -7.11E 00 |
| 153 | 2.13E 03 | -1.36E 03 | 1.50E 02 | 2.14E 03 | -1.36E 03 | 2.46E 00 |
| 154 | 2.68E 03 | -9.82E 02 | 2.26E 02 | 2.70E 03 | -9.96E 02 | 3.51E 00 |
| 155 | 1.24E 03 | -3.27E 03 | -5.88E 02 | 1.31E 03 | -3.34E 03 | -7.32E 00 |
| 156 | 2.45E 03 | -2.37E 03 | -3.20E 02 | 2.48E 03 | -2.39E 03 | -3.78E 00 |
| 157 | -3.31E 03 | -5.51E 03 | -5.26E 02 | -3.19E 03 | -5.63E 03 | -1.27E 01 |
| 158 | -3.00E 03 | -2.79E 03 | -5.24E 02 | -2.36E 03 | -3.43E 03 | 1.29E 02 |
| 159 | -3.18E 03 | -5.65E 03 | -8.94E 02 | -2.89E 03 | -5.94E 03 | -1.80E 01 |
| 160 | -2.27E 03 | -2.12E 03 | -8.57E 02 | -1.34E 03 | -3.06E 03 | 1.32E 02 |
| 161 | -2.75E 03 | -5.57E 03 | -8.20E 02 | -2.53E 03 | -5.79E 03 | -1.51E 01 |
| 162 | -2.38E 03 | -2.01E 03 | -6.98E 02 | -1.47E 03 | -2.92E 03 | 1.28E 02 |
| 163 | -2.69E 03 | -5.90E 03 | -9.35E 02 | -2.44E 03 | -6.16E 03 | -1.51E 01 |
| 164 | -2.52E 03 | -2.33E 03 | -9.36E 02 | -1.48E 03 | -3.36E 03 | 1.32E 02 |
| 165 | -2.47E 03 | -5.98E 03 | -8.93E 02 | -2.25E 03 | -6.19E 03 | -1.35E 01 |
| 166 | -2.18E 03 | -2.46E 03 | -1.10E 03 | -1.20E 03 | -3.43E 03 | -4.13E 01 |
| 167 | -2.25E 03 | -6.08E 03 | -8.84E 02 | -2.05E 03 | -6.27E 03 | -1.24E 01 |
| 168 | -1.92E 03 | -2.44E 03 | -9.90E 02 | -1.15E 03 | -3.20E 03 | -3.76E 01 |
| 169 | -2.04E 03 | -6.21E 03 | -8.90E 02 | -1.86E 03 | -6.39E 03 | -1.16E 01 |
| 170 | -1.78E 03 | -2.50E 03 | -9.58E 02 | -1.12E 03 | -3.16E 03 | -3.46E 01 |
| 171 | -1.92E 03 | -6.32E 03 | -8.51E 02 | -1.76E 03 | -6.48E 03 | -1.06E 01 |
| 172 | -1.65E 03 | -2.50E 03 | -9.04E 02 | -1.08E 03 | -3.08E 03 | -3.24E 01 |
| 173 | -1.81E 03 | -6.41E 03 | -8.00E 02 | -1.68E 03 | -6.55E 03 | -9.59E 00 |
| 174 | -1.55E 03 | -2.51E 03 | -8.40E 02 | -1.06E 03 | -3.00E 03 | -3.01E 01 |
| 175 | -1.72E 03 | -6.50E 03 | -7.40E 02 | -1.61E 03 | -6.61E 03 | -8.60E 00 |
| 176 | -1.45E 03 | -2.51E 03 | -7.74E 02 | -1.04E 03 | -2.91E 03 | -2.79E 01 |
| 177 | -1.64E 03 | -6.57E 03 | -6.79E 02 | -1.55E 03 | -6.67E 03 | -7.70E 00 |
| 178 | -1.35E 03 | -2.50E 03 | -6.90E 02 | -1.03E 03 | -2.83E 03 | -2.51E 01 |
| 179 | -1.57E 03 | -6.74E 03 | -6.11E 02 | -1.49E 03 | -6.82E 03 | -6.64E 00 |
| 180 | -1.24E 03 | -2.41E 03 | -6.29E 02 | -9.66E 02 | -2.69E 03 | -2.35E 01 |
| 181 | -1.56E 03 | -7.02E 03 | -5.12E 02 | -1.51E 03 | -7.07E 03 | -5.31E 00 |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 182 | 2.14E 02 | 2.61E 02 | 8.73E-04 | -1.08E-02 | -5.98E-03 |
| 183 | 2.08E 02 | 2.76E 02 | -9.88E-04 | -4.04E-03 | -6.59E-03 |
| 184 | 2.40E 02 | 2.51E 02 | 6.75E-03 | -2.44E-02 | -2.13E-03 |
| 185 | 2.31E 02 | 2.66E 02 | 3.23E-03 | -1.57E-02 | -4.08E-03 |
| 186 | 2.21E 02 | 2.81E 02 | -8.95E-04 | -4.68E-03 | -5.57E-03 |
| 187 | 2.54E 02 | 2.60E 02 | 7.43E-03 | -2.49E-02 | -1.01E-03 |
| 188 | 2.45E 02 | 2.75E 02 | 3.51E-03 | -1.51E-02 | -3.42E-03 |
| 189 | 2.36E 02 | 2.90E 02 | -4.62E-04 | -5.15E-03 | -4.36E-03 |
| 190 | 2.69E 02 | 2.70E 02 | 8.16E-03 | -2.54E-02 | -6.75E-04 |
| 191 | 2.59E 02 | 2.84E 02 | 3.95E-03 | -1.53E-02 | -2.42E-03 |
| 192 | 2.50E 02 | 2.99E 02 | -8.72E-05 | -5.03E-03 | -3.84E-03 |
| 193 | 2.83E 02 | 2.79E 02 | 8.70E-03 | -2.56E-02 | -3.24E-04 |
| 194 | 2.73E 02 | 2.93E 02 | 4.44E-03 | -1.55E-02 | -1.98E-03 |
| [illegible] | 2.64E 02 | 3.07E 02 | 2.84E-04 | -5.09E-03 | -3.12E-03 |
| [illegible] | 2.97E 02 | 2.89E 02 | 9.27E-03 | -2.60E-02 | -2.24E-04 |
| [illegible] | 2.88E 02 | 3.02E 02 | 4.88E-03 | -1.56E-02 | -1.74E-03 |
| [illegible] | 2.78E 02 | 3.16E 02 | 6.14E-04 | -5.12E-03 | -2.71E-03 |
| [illegible] | 3.12E 02 | 2.98E 02 | 9.84E-03 | -2.63E-02 | -3.97E-04 |
| [illegible] | 3.02E 02 | 3.11E 02 | 5.28E-03 | -1.58E-02 | -1.85E-03 |
| [illegible] | 2.93E 02 | 3.25E 02 | 8.30E-04 | -5.13E-03 | -2.56E-03 |
| [illegible] | 3.26E 02 | 3.07E 02 | 1.05E-02 | -2.69E-02 | -1.15E-03 |
| [illegible] | 3.16E 02 | 3.21E 02 | 5.52E-03 | -1.59E-02 | -2.50E-03 |
| [illegible] | 3.07E 02 | 3.34E 02 | 8.74E-04 | -5.08E-03 | -2.62E-03 |
| [illegible] | 3.45E 02 | 3.15E 02 | 1.29E-02 | -2.99E-02 | -1.23E-04 |
| [illegible] | 3.38E 02 | 3.20E 02 | 9.48E-03 | -2.44E-02 | -4.21E-03 |
| [illegible] | 3.29E 02 | 3.31E 02 | 4.20E-03 | -1.37E-02 | -4.17E-03 |
| [illegible] | 3.21E 02 | 3.43E 02 | 6.18E-04 | -4.50E-03 | -2.93E-03 |
| [illegible] | 3.54E 02 | 3.21E 02 | 1.34E-02 | -3.06E-02 | -6.11E-04 |
| [illegible] | 3.42E 02 | 3.31E 02 | 7.21E-03 | -2.00E-02 | -7.46E-03 |
| [illegible] | 3.55E 02 | 3.30E 02 | 1.24E-02 | -2.93E-02 | -4.63E-03 |
| [illegible] | 3.67E 02 | 3.30E 02 | 1.51E-02 | -3.42E-02 | -1.09E-03 |
| [illegible] | 3.77E 02 | 3.35E 02 | 1.58E-02 | -3.66E-02 | 4.91E-03 |
| [illegible] | 3.35E 02 | 3.41E 02 | 1.96E-03 | -1.00E-02 | -4.89E-03 |
| [illegible] | 3.42E 02 | 3.41E 02 | 2.52E-03 | -1.26E-02 | -6.92E-03 |
| [illegible] | 3.52E 02 | 3.40E 02 | 8.29E-03 | -2.17E-02 | -1.08E-02 |
| [illegible] | 3.64E 02 | 3.41E 02 | 1.32E-02 | -3.08E-02 | -3.71E-03 |
| [illegible] | 3.75E 02 | 3.42E 02 | 1.44E-02 | -3.32E-02 | 3.85E-03 |
| [illegible] | 3.88E 02 | 3.43E 02 | 1.52E-02 | -3.45E-02 | 6.81E-03 |
| [illegible] | 3.30E 02 | 3.49E 02 | 1.18E-03 | -5.02E-03 | -3.26E-03 |
| [illegible] | 3.41E 02 | 3.49E 02 | 2.05E-03 | -6.35E-03 | -1.05E-03 |
| [illegible] | 3.52E 02 | 3.49E 02 | 2.14E-03 | -1.51E-02 | -1.50E-02 |
| [illegible] | 3.64E 02 | 3.49E 02 | 1.01E-02 | -2.82E-02 | -7.88E-03 |
| [illegible] | 3.76E 02 | 3.49E 02 | 1.25E-02 | -3.08E-02 | 2.88E-03 |
| [illegible] | 3.88E 02 | 3.50E 02 | 1.45E-02 | -3.16E-02 | 3.54E-03 |
| [illegible] | 4.01E 02 | 3.50E 02 | 1.72E-02 | -3.38E-02 | 2.16E-03 |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | |
|---|---|---|---|---|---|---|
| 182 | -1.31E 03 | -3.47E 03 | -6.10E 02 | -1.15E 03 | -3.63E 03 | -1 |
| 183 | -9.39E 02 | -1.47E 03 | -6.48E 02 | -5.03E 02 | -1.90E 03 | -3 |
| 184 | -1.31E 03 | -7.23E 03 | -2.73E 02 | -1.30E 03 | -7.24E 03 | -2 |
| 185 | -1.22E 03 | -4.73E 03 | -4.37E 02 | -1.17E 03 | -4.79E 03 | - |
| 186 | -9.95E 02 | -1.65E 03 | -5.52E 02 | -6.81E 02 | -1.97E 03 | - |
| 187 | -1.15E 03 | -7.22E 03 | -1.67E 02 | -1.14E 03 | -7.23E 03 | - |
| 188 | -1.04E 03 | -4.46E 03 | -3.74E 02 | -9.95E 02 | -4.50E 03 | - |
| 189 | -9.11E 02 | -1.73E 03 | -4.37E 02 | -7.22E 02 | -1.92E 03 | |
| 190 | -9.60E 02 | -7.20E 03 | -1.39E 02 | -9.57E 02 | -7.20E 03 | |
| 191 | -9.09E 02 | -4.41E 03 | -2.80E 02 | -8.87E 02 | -4.44E 03 | |
| 192 | -7.68E 02 | -1.63E 03 | -3.86E 02 | -6.21E 02 | -1.78E 03 | |
| 193 | -8.12E 02 | -7.15E 03 | -1.10E 02 | -8.10E 02 | -7.15E 03 | |
| 194 | -7.66E 02 | -4.37E 03 | -2.40E 02 | -7.50E 02 | -4.39E 03 | |
| 195 | -6.53E 02 | -1.60E 03 | -3.17E 02 | -5.56E 02 | -1.69E 03 | |
| 196 | -6.63E 02 | -7.14E 03 | -1.07E 02 | -6.62E 02 | -7.14E 03 | |
| 197 | -6.42E 02 | -4.34E 03 | -2.18E 02 | -6.29E 02 | -4.36E 03 | |
| 198 | -5.46E 02 | -1.56E 03 | -2.76E 02 | -4.76E 02 | -1.63E 03 | |
| 199 | -5.22E 02 | -7.16E 03 | -1.31E 02 | -5.20E 02 | -7.16E 03 | |
| 200 | -5.33E 02 | -4.34E 03 | -2.29E 02 | -5.19E 02 | -4.35E 03 | |
| 201 | -4.70E 02 | -1.54E 03 | -2.56E 02 | -4.12E 02 | -1.60E 03 | |
| 202 | -3.64E 02 | -7.25E 03 | -2.06E 02 | -3.58E 02 | -7.26E 03 | |
| 203 | -4.65E 02 | -4.35E 03 | -2.86E 02 | -4.44E 02 | -4.37E 03 | |
| 204 | -4.36E 02 | -1.53E 03 | -2.51E 02 | -3.81E 02 | -1.58E 03 | |
| 205 | 1.46E 01 | -7.98E 03 | -8.04E 01 | 1.54E 01 | -7.98E 03 | |
| 206 | -3.73E 02 | -6.64E 03 | -4.72E 02 | -3.37E 02 | -6.67E 0 | |
| 207 | -5.73E 02 | -3.88E 03 | -4.13E 02 | -5.22E 02 | -3.93E 0 | |
| 208 | -4.15E 02 | -1.39E 03 | -2.64E 02 | -3.49E 02 | -1.46E 0 | |
| 209 | 7.67E 01 | -8.15E 03 | -1.21E 02 | 7.85E 01 | -8.15E 0 | |
| 210 | -4.74E 02 | -5.54E 03 | -7.24E 02 | -3.73E 02 | -5.64E 0 | |
| 211 | -7.79E 01 | -7.89E 03 | -4.74E 02 | -4.93E 01 | -7.92E 0 | |
| 212 | 1.19E 02 | -9.11E 03 | -1.25E 02 | 1.21E 02 | -9.12E | |
| 213 | 2.21E 01 | -9.78E 03 | 4.56E 02 | 4.32E 01 | -9.80E | |
| 214 | -7.57E 02 | -3.01E 03 | -4.51E 02 | -6.70E 02 | -3.10E | |
| 215 | -9.26E 02 | -3.77E 03 | -6.36E 02 | -7.91E 02 | -3.91E | |
| 216 | -3.21E 02 | -5.93E 03 | -9.99E 02 | -1.48E 02 | -6.11E | |
| 217 | 1.05E 01 | -8.19E 03 | -3.38E 02 | 2.44E 01 | -8.21E | |
| 218 | 8.60E 01 | -8.80E 03 | 3.63E 02 | 1.01E 02 | -8.81E | |
| 219 | 1.69E 02 | -9.10E 03 | 6.35E 02 | 2.13E 02 | -9.14E | |
| 220 | -2.89E 02 | -1.47E 03 | -2.90E 02 | -2.22E 02 | -1.54E | |
| 221 | -1.67E 02 | -1.79E 03 | -8.12E 01 | -1.63E 02 | -1.80E | |
| 222 | -1.30E 03 | -4.57E 03 | -1.35E 03 | -8.16E 02 | -5.06E | |
| 223 | -5.14E 02 | -7.68E 03 | -7.06E 02 | -4.45E 02 | -7.74E | |
| 224 | -9.49E 01 | -8.17E 03 | 2.74E 02 | -8.56E 01 | -8.1 | |
| 225 | 4.88E 02 | -8.14E 03 | 3.31E 02 | 5.01E 02 | -8.1 | |
| 226 | 1.11E 03 | -8.46E 03 | 1.97E 02 | 1.11E 03 | -8. | |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 227 | 3.65E 02 | 3.56E 02 | 1.70E-04 | -3.37E-02 | -2.00E-02 |
| | STRIP AXIAL FORCE= 1.351E 03 | | MOMENT= 7.010E-02 | | |
| | SKIN MEMBRANE STRESS= 0.166E 06 | | | | |
| 228 | 3.76E 02 | 3.56E 02 | 2.34E-04 | -2.50E-02 | -5.80E-03 |
| | STRIP AXIAL FORCE= 1.862E 03 | | MOMENT= -1.548E-03 | | |
| 229 | 3.88E 02 | 3.57E 02 | 5.17E-04 | -2.62E-02 | -1.38E-03 |
| | STRIP AXIAL FORCE= 4.113E 03 | | MOMENT= 1.109E-02 | | |
| 230 | 4.00E 02 | 3.57E 02 | 6.67E-04 | -2.61E-02 | 1.02E-03 |
| | STRIP AXIAL FORCE= 5.299E 03 | | MOMENT= 1.619E-02 | | |
| 231 | 4.12E 02 | 3.58E 02 | 9.74E-03 | -2.67E-02 | 4.01E-03 |
| 232 | 3.65E 02 | 3.61E 02 | 4.46E-04 | -2.86E-02 | -1.15E-02 |
| | STRIP AXIAL FORCE= 3.543E 03 | | MOMENT= 3.475E-03 | | |
| | SKIN MEMBRANE STRESS= 0.142E 06 | | | | |
| 233 | 3.77E 02 | 3.61E 02 | 2.31E-04 | -2.30E-02 | -8.40E-03 |
| | STRIP AXIAL FORCE= 1.837E 03 | | MOMENT= 2.002E-03 | | |
| 234 | 3.89E 02 | 3.61E 02 | 2.38E-04 | -2.31E-02 | -3.74E-03 |
| | STRIP AXIAL FORCE= 1.888E 03 | | MOMENT= 2.176E-03 | | |
| 235 | 4.00E 02 | 3.61E 02 | 2.62E-04 | -2.33E-02 | 1.70E-04 |
| | STRIP AXIAL FORCE= 2.081E 03 | | MOMENT= 1.594E-04 | | |
| 236 | 4.09E 02 | 3.61E 02 | 7.79E-03 | -2.42E-02 | 3.69E-03 |
| 237 | 3.65E 02 | 3.66E 02 | 4.23E-04 | -2.29E-02 | -6.94E-03 |
| | STRIP AXIAL FORCE= 3.364E 03 | | MOMENT= -9.450E-04 | | |
| | SKIN MEMBRANE STRESS= 0.117E 06 | | | | |
| 238 | 3.77E 02 | 3.66E 02 | 3.15E-04 | -2.06E-02 | -7.28E-03 |
| | STRIP AXIAL FORCE= 2.504E 03 | | MOMENT= -7.034E-04 | | |
| 239 | 3.89E 02 | 3.66E 02 | 2.83E-04 | -2.01E-02 | -3.63E-03 |
| | STRIP AXIAL FORCE= 2.253E 03 | | MOMENT= 5.728E-04 | | |
| 240 | 4.00E 02 | 3.66E 02 | 2.99E-04 | -2.07E-02 | -6.08E-04 |
| | STRIP AXIAL FORCE= 2.380E 03 | | MOMENT= 5.682E-04 | | |
| 241 | 4.09E 02 | 3.66E 02 | 6.44E-03 | -2.10E-02 | 2.50E-03 |
| 242 | 4.19E 02 | 3.65E 02 | 7.48E-03 | -2.27E-02 | 3.57E-03 |
| 243 | 3.65E 02 | 3.70E 02 | 6.18E-04 | -1.94E-02 | -4.75E-03 |
| | STRIP AXIAL FORCE= 4.915E 03 | | MOMENT= -5.001E-03 | | |
| | SKIN MEMBRANE STRESS= 0.995E 05 | | | | |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 227 | -3.98E 03 | -9.38E 03 | -1.62E 03 | -3.53E 03 | -9.83E 03 | -1.55E 01 |
| 228 | -2.93E 03 | -6.96E 03 | -4.59E 02 | -2.88E 03 | -7.01E 03 | -6.42E 00 |
| 229 | -3.01E 03 | -7.29E 03 | -9.75E 01 | -3.01E 03 | -7.29E 03 | -1.30E 00 |
| 230 | -2.95E 03 | -7.22E 03 | 8.88E 01 | -2.94E 03 | -7.22E 03 | 1.19E 00 |
| 231 | -5.31E 02 | -7.16E 03 | 3.74E 02 | -5.10E 02 | -7.18E 03 | 3.22E 00 |
| 232 | -3.41E 03 | -8.19E 03 | -9.69E 02 | -3.22E 03 | -8.38E 03 | -1.10E 01 |
| 233 | -2.78E 03 | -6.59E 03 | -6.97E 02 | -2.65E 03 | -6.72E 03 | -1.00E 01 |
| 234 | -2.79E 03 | -6.64E 03 | -2.98E 02 | -2.77E 03 | -6.66E 03 | -4.41E 00 |
| 235 | -2.81E 03 | -6.70E 03 | 3.62E 01 | -2.81E 03 | -6.70E 03 | 5.33E-01 |
| 236 | -8.28E 02 | -6.64E 03 | 3.45E 02 | -8.07E 02 | -6.66E 03 | 3.39E 00 |
| 237 | -2.82E 03 | -6.81E 03 | -6.08E 02 | -2.73E 03 | -6.90E 03 | -8.46E 00 |
| 238 | -2.56E 03 | -6.14E 03 | -6.30E 02 | -2.45E 03 | -6.24E 03 | -9.70E 00 |
| 239 | -2.50E 03 | -5.99E 03 | -3.04E 02 | -2.48E 03 | -6.02E 03 | -4.94E 00 |
| 240 | -2.58E 03 | -6.18E 03 | -3.59E 01 | -2.58E 03 | -6.18E 03 | -5.71E-01 |
| 241 | -8.27E 02 | -5.83E 03 | 2.36E 02 | -8.16E 02 | -5.84E 03 | 2.69E 00 |
| 242 | -7.19E 02 | -6.27E 03 | 3.31E 02 | -6.99E 02 | -6.29E 03 | 3.40E 00 |
| 243 | -2.39E 03 | -5.94E 03 | -4.22E 02 | -2.34E 03 | -5.99E 03 | -6.68E 00 |

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NO.        X          Y        EPSILON-X  EPSILON-Y   GAMA-XY

244      3.77E 02   3.70E 02   4.66E-04  -1.84E-02  -5.51E-03
       STRIP AXIAL FORCE=  3.707E 03   MOMENT= -1.461E-03

245      3.89E 02   3.70E 02   3.84E-04  -1.79E-02  -2.94E-03
       STRIP AXIAL FORCE=  3.055E 03   MOMENT= -1.398E-03

246      4.00E 02   3.70E 02   3.88E-04  -1.82E-02  -3.62E-04
       STRIP AXIAL FORCE=  3.085E 03   MOMENT= -2.208E-03

247      4.12E 02   3.70E 02   5.93E-03  -2.00E-02   1.54E-03
248      4.23E 02   3.70E 02   6.33E-03  -1.98E-02   2.69E-03
249      3.65E 02   3.74E 02   6.73E-04  -1.59E-02  -2.52E-03
       STRIP AXIAL FORCE=  5.346E 03   MOMENT=  1.840E-03
         SKIN MEMBRANE STRESS=  0.864E 05

250      3.65E 02   3.78E 02   5.86E-04  -1.35E-02  -1.56E-03
       STRIP AXIAL FORCE=  4.656E 03   MOMENT=  1.313E-03
         SKIN MEMBRANE STRESS=  0.747E 05

251      3.77E 02   3.74E 02   5.52E-04  -1.55E-02  -3.88E-03
       STRIP AXIAL FORCE=  4.386E 03   MOMENT=  4.839E-05

252      3.77E 02   3.78E 02   5.03E-04  -1.35E-02  -2.63E-03
       STRIP AXIAL FORCE=  4.000E 03   MOMENT=  1.581E-03

253      3.89E 02   3.74E 02   4.64E-04  -1.51E-02  -2.31E-03
       STRIP AXIAL FORCE=  3.684E 03   MOMENT= -2.195E-05

254      3.89E 02   3.78E 02   4.08E-04  -1.33E-02  -1.62E-03
       STRIP AXIAL FORCE=  3.246E 03   MOMENT=  1.266E-03

255      4.00E 02   3.74E 02   4.57E-04  -1.56E-02  -4.24E-04
       STRIP AXIAL FORCE=  3.634E 03   MOMENT=  1.153E-03

256      4.00E 02   3.78E 02   4.11E-04  -1.37E-02  -1.21E-04
       STRIP AXIAL FORCE=  3.263E 03   MOMENT=  8.697E-04

257      4.11E 02   3.74E 02   5.12E-03  -1.69E-02   6.73E-04
258      4.11E 02   3.78E 02   4.12E-03  -1.45E-02   3.44E-04
259      4.24E 02   3.74E 02   5.35E-03  -1.67E-02   2.13E-03
260      4.24E 02   3.78E 02   4.95E-03  -1.60E-02   1.84E-03
261      4.34E 02   3.74E 02   6.15E-03  -1.81E-02   3.52E-03
262      4.35E 02   3.78E 02   5.47E-03  -1.53E-02   1.55E-03
263      3.65E 02   3.82E 02   5.04E-04  -1.03E-02  -8.53E-04
       STRIP AXIAL FORCE=  4.003E 03   MOMENT=  6.026E-04
         SKIN MEMBRANE STRESS=  0.633E 05
```

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 244 | -2.30E 03 | -5.64E 03 | -4.89E 02 | -2.23E 03 | -5.71E 03 | -8.16E 00 |
| 245 | -2.27E 03 | -5.51E 03 | -2.56E 02 | -2.25E 03 | -5.53E 03 | -4.49E 00 |
| 246 | -2.31E 03 | -5.61E 03 | -2.94E 01 | -2.31E 03 | -5.61E 03 | -5.10E-01 |
| 247 | -8.69E 02 | -5.66E 03 | 1.43E 02 | -8.65E 02 | -5.67E 03 | 1.70E 00 |
| 248 | -6.93E 02 | -5.52E 03 | 2.52E 02 | -6.80E 02 | -5.53E 03 | 2.98E 00 |
| 249 | -2.07E 03 | -5.28E 03 | -2.47E 02 | -2.06E 03 | -5.30E 03 | -4.38E 00 |
| 250 | -1.79E 03 | -4.58E 03 | -1.56E 02 | -1.79E 03 | -4.58E 03 | -3.20E 00 |
| 251 | -2.06E 03 | -5.16E 03 | -3.79E 02 | -2.02E 03 | -5.21E 03 | -6.86E 00 |
| 252 | -1.83E 03 | -4.60E 03 | -2.68E 02 | -1.81E 03 | -4.62E 03 | -5.49E 00 |
| 253 | -2.04E 03 | -5.04E 03 | -2.16E 02 | -2.02E 03 | -5.06E 03 | -4.08E 00 |
| 254 | -1.83E 03 | -4.52E 03 | -1.56E 02 | -1.82E 03 | -4.53E 03 | -3.31E 00 |
| 255 | -2.10E 03 | -5.20E 03 | -3.04E 01 | -2.10E 03 | -5.20E 03 | -5.63E-01 |
| 256 | -1.89E 03 | -4.68E 03 | -3.19E 00 | -1.89E 03 | -4.68E 03 | -6.57E-02 |
| 257 | -7.29E 02 | -4.96E 03 | 6.86E 01 | -7.28E 02 | -4.96E 03 | 9.29E-01 |
| 258 | -7.24E 02 | -4.30E 03 | 2.89E 01 | -7.23E 02 | -4.30E 03 | 4.64E-01 |
| 259 | -6.13E 02 | -4.83E 03 | 2.12E 02 | -6.02E 02 | -4.85E 03 | 2.87E 00 |
| 260 | -6.38E 02 | -4.68E 03 | 1.88E 02 | -6.29E 02 | -4.69E 03 | 2.66E 00 |
| 261 | -5.18E 02 | -5.18E 03 | 3.50E 02 | -4.92E 02 | -5.21E 03 | 4.27E 00 |
| 262 | -3.19E 02 | -4.36E 03 | 1.40E 02 | -3.14E 02 | -4.37E 03 | 1.98E 00 |
| 263 | -1.52E 03 | -3.92E 03 | -9.20E 01 | -1.52E 03 | -3.93E 03 | -2.19E 00 |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 264 | 3.65E 02 | 3.85E 02 | 4.72E-04 | -8.63E-03 | -6.92E-04 |
| | STRIP AXIAL FORCE= 3.755E 03 | | MOMENT= -3.072E-04 | | |
| | SKIN MEMBRANE STRESS= 0.537E 05 | | | | |
| 265 | 3.77E 02 | 3.82E 02 | 4.79E-04 | -1.06E-02 | -1.48E-03 |
| | STRIP AXIAL FORCE= 3.806E 03 | | MOMENT= 5.489E-04 | | |
| 266 | 3.77E 02 | 3.85E 02 | 4.47E-04 | -8.91E-03 | -9.33E-04 |
| | STRIP AXIAL FORCE= 3.550E 03 | | MOMENT= 5.122E-04 | | |
| 267 | 3.89E 02 | 3.82E 02 | 4.26E-04 | -1.05E-02 | -9.80E-04 |
| | STRIP AXIAL FORCE= 3.387E 03 | | MOMENT= 6.216E-04 | | |
| 268 | 3.89E 02 | 3.86E 02 | 3.94E-04 | -8.87E-03 | -5.23E-04 |
| | STRIP AXIAL FORCE= 3.129E 03 | | MOMENT= 6.467E-04 | | |
| 269 | 4.00E 02 | 3.82E 02 | 4.16E-04 | -1.09E-02 | -2.24E-05 |
| | STRIP AXIAL FORCE= 3.307E 03 | | MOMENT= 1.833E-05 | | |
| 270 | 4.00E 02 | 3.86E 02 | 4.11E-04 | -9.33E-03 | 2.02E-04 |
| | STRIP AXIAL FORCE= 3.269E 03 | | MOMENT= -8.010E-05 | | |
| 271 | 4.11E 02 | 3.82E 02 | 3.70E-03 | -1.18E-02 | 7.49E-04 |
| 272 | 4.11E 02 | 3.86E 02 | 3.34E-03 | -1.03E-02 | 1.09E-03 |
| 273 | 4.23E 02 | 3.82E 02 | 4.11E-03 | -1.29E-02 | 8.96E-04 |
| 274 | 4.23E 02 | 3.86E 02 | 3.32E-03 | -1.08E-02 | 6.88E-04 |
| 275 | 4.34E 02 | 3.82E 02 | 4.03E-03 | -1.22E-02 | 1.59E-03 |
| 276 | 4.37E 02 | 3.86E 02 | 3.66E-03 | -1.10E-02 | 1.44E-03 |
| 277 | 4.44E 02 | 3.80E 02 | 4.69E-03 | -1.36E-02 | 2.28E-03 |
| 278 | 4.47E 02 | 3.86E 02 | 4.39E-03 | -1.08E-02 | 3.64E-04 |
| 279 | 3.65E 02 | 3.90E 02 | 4.35E-04 | -5.43E-03 | -2.70E-04 |
| | STRIP AXIAL FORCE= 3.461E 03 | | MOMENT= 2.317E-04 | | |
| | SKIN MEMBRANE STRESS= 0.408E 05 | | | | |
| 280 | 3.65E 02 | 3.95E 02 | 3.54E-04 | -3.46E-03 | -7.45E-05 |
| | STRIP AXIAL FORCE= 2.815E 03 | | MOMENT= 1.251E-03 | | |
| | SKIN MEMBRANE STRESS= 0.268E 05 | | | | |
| 281 | 3.77E 02 | 3.90E 02 | 4.16E-04 | -5.73E-03 | -3.03E-04 |
| | STRIP AXIAL FORCE= 3.304E 03 | | MOMENT= 1.868E-04 | | |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 264 | -1.29E 03 | -3.37E 03 | -7.57E 01 | -1.29E 03 | -3.38E 03 | -2.08E 00 |
| 265 | -1.56E 03 | -4.01E 03 | -1.65E 02 | -1.55E 03 | -4.02E 03 | -3.84E 00 |
| 266 | -1.35E 03 | -3.48E 03 | -1.10E 02 | -1.34E 03 | -3.49E 03 | -2.94E 00 |
| 267 | -1.57E 03 | -3.97E 03 | -1.04E 02 | -1.56E 03 | -3.97E 03 | -2.47E 00 |
| 268 | -1.36E 03 | -3.48E 03 | -5.75E 01 | -1.36E 03 | -3.48E 03 | -1.56E 00 |
| 269 | -1.65E 03 | -4.15E 03 | 5.11E 00 | -1.65E 03 | -4.15E 03 | 1.17E-01 |
| 270 | -1.44E 03 | -3.66E 03 | 2.44E 01 | -1.44E 03 | -3.66E 03 | 6.26E-01 |
| 271 | -5.11E 02 | -3.69E 03 | 7.82E 01 | -5.09E 02 | -3.69E 03 | 1.41E 00 |
| 272 | -3.79E 02 | -3.23E 03 | 1.23E 02 | -3.74E 02 | -3.23E 03 | 2.47E 00 |
| 273 | -5.15E 02 | -4.03E 03 | 8.84E 01 | -5.13E 02 | -4.04E 03 | 1.44E 00 |
| 274 | -4.81E 02 | -3.45E 03 | 6.52E 01 | -4.80E 02 | -3.45E 03 | 1.26E 00 |
| 275 | -4.34E 02 | -3.78E 03 | 1.69E 02 | -4.25E 02 | -3.79E 03 | 2.88E 00 |
| 276 | -3.83E 02 | -3.51E 03 | 1.63E 02 | -3.74E 02 | -3.52E 03 | 2.97E 00 |
| 277 | -3.98E 02 | -4.18E 03 | 2.52E 02 | -3.81E 02 | -4.19E 03 | 3.80E 00 |
| 278 | -2.28E 01 | -3.30E 03 | 2.71E 01 | -2.26E 01 | -3.30E 03 | 4.74E-01 |
| 279 | -9.79E 02 | -2.73E 03 | -3.67E 01 | -9.78E 02 | -2.73E 03 | -1.20E 00 |
| 280 | -6.45E 02 | -1.92E 03 | -8.38E 00 | -6.45E 02 | -1.92E 03 | -3.77E-01 |
| 281 | -1.05E 03 | -2.86E 03 | -4.92E 01 | -1.05E 03 | -2.87E 03 | -1.55E 00 |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 282 | 3.77E 02 | 3.95E 02 | 3.68E-04 | -3.73E-03 | 3.28E-05 |
| | STRIP AXIAL FORCE= 2.925E 03 | | MOMENT= 6.475E-04 | | |
| 283 | 3.89E 02 | 3.90E 02 | 3.74E-04 | -5.73E-03 | -1.48E-04 |
| | STRIP AXIAL FORCE= 2.972E 03 | | MOMENT= 3.542E-04 | | |
| 284 | 3.89E 02 | 3.96E 02 | 3.30E-04 | -3.73E-03 | 1.33E-04 |
| | STRIP AXIAL FORCE= 2.623E 03 | | MOMENT= 5.815E-04 | | |
| 285 | 4.00E 02 | 3.90E 02 | 4.06E-04 | -6.15E-03 | 2.03E-05 |
| | STRIP AXIAL FORCE= 3.229E 03 | | MOMENT= 7.174E-05 | | |
| 286 | 4.00E 02 | 3.96E 02 | 3.49E-04 | -4.03E-03 | -1.43E-04 |
| | STRIP AXIAL FORCE= 2.774E 03 | | MOMENT= 1.056E-03 | | |
| 287 | 4.11E 02 | 3.90E 02 | 2.56E-03 | -7.09E-03 | 2.99E-04 |
| 288 | 4.11E 02 | 3.96E 02 | 1.84E-03 | -4.78E-03 | -3.99E-05 |
| 289 | 4.23E 02 | 3.91E 02 | 2.73E-03 | -7.55E-03 | 6.33E-04 |
| 290 | 4.23E 02 | 3.96E 02 | 2.24E-03 | -5.32E-03 | 5.79E-04 |
| 291 | 4.35E 02 | 3.91E 02 | 2.88E-03 | -7.77E-03 | 6.05E-04 |
| 292 | 4.35E 02 | 3.96E 02 | 2.31E-03 | -5.35E-03 | 3.09E-04 |
| 293 | 4.45E 02 | 3.91E 02 | 2.84E-03 | -7.20E-03 | 1.92E-04 |
| 294 | 4.48E 02 | 3.96E 02 | 2.48E-03 | -5.61E-03 | 1.64E-04 |
| 295 | 4.58E 02 | 3.91E 02 | 3.64E-03 | -8.49E-03 | 1.45E-03 |
| 296 | 4.60E 02 | 3.96E 02 | 2.80E-03 | -5.51E-03 | -1.31E-04 |
| 297 | 3.65E 02 | 4.01E 02 | 2.07E-04 | -1.40E-03 | -3.04E-04 |
| | STRIP AXIAL FORCE= 1.645E 03 | | MOMENT= 4.480E-04 | | |
| | SKIN MEMBRANE STRESS= 0.134E 05 | | | | |
| 298 | 3.77E 02 | 4.01E 02 | 2.74E-04 | -1.67E-03 | 9.56E-05 |
| | STRIP AXIAL FORCE= 2.174E 03 | | MOMENT= 2.991E-04 | | |
| 299 | 3.89E 02 | 4.01E 02 | 2.87E-04 | -1.63E-03 | 1.89E-04 |
| | STRIP AXIAL FORCE= 2.282E 03 | | MOMENT= -6.098E-04 | | |
| 300 | 4.00E 02 | 4.01E 02 | 3.19E-04 | -1.82E-03 | -1.02E-04 |
| | STRIP AXIAL FORCE= 2.534E 03 | | MOMENT= -1.305E-03 | | |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 282 | -7.02E 02 | -2.06E 03 | 8.71E-01 | -7.02E 02 | -2.06E 03 | 3.67E-02 |
| 283 | -1.07E 03 | -2.86E 03 | -2.44E 01 | -1.07E 03 | -2.86E 03 | -7.81E-01 |
| 284 | -7.24E 02 | -2.07E 03 | 2.11E 01 | -7.24E 02 | -2.07E 03 | 8.99E-01 |
| 285 | -1.15E 03 | -3.08E 03 | 1.62E 00 | -1.15E 03 | -3.08E 03 | 4.79E-02 |
| 286 | -7.90E 02 | -2.24E 03 | -2.76E 01 | -7.90E 02 | -2.24E 03 | -1.09E 00 |
| 287 | -2.16E 02 | -2.60E 03 | 4.18E 01 | -2.15E 02 | -2.60E 03 | 1.01E 00 |
| 288 | -9.62E 01 | -1.87E 03 | -5.69E 00 | -9.62E 01 | -1.87E 03 | -1.84E-01 |
| 289 | -2.20E 02 | -2.78E 03 | 9.06E 01 | -2.17E 02 | -2.78E 03 | 2.02E 00 |
| 290 | 7.59E 00 | -2.05E 03 | 8.81E 01 | 1.14E 01 | -2.05E 03 | 2.45E 00 |
| 291 | -1.85E 02 | -2.87E 03 | 8.06E 01 | -1.82E 02 | -2.87E 03 | 1.72E 00 |
| 292 | 6.76E 01 | -2.04E 03 | 3.78E 01 | 6.83E 01 | -2.04E 03 | 1.02E 00 |
| 293 | -8.29E 01 | -2.58E 03 | 1.73E 01 | -8.28E 01 | -2.58E 03 | 3.96E-01 |
| 294 | 9.63E 01 | -2.14E 03 | 2.50E 01 | 9.66E 01 | -2.14E 03 | 6.42E-01 |
| 295 | 4.87E 01 | -2.98E 03 | 2.02E 02 | 6.21E 01 | -2.99E 03 | 3.80E 00 |
| 296 | 2.86E 02 | -2.03E 03 | -3.47E 01 | 2.86E 02 | -2.03E 03 | -8.58E-01 |
| 297 | -3.22E 02 | -1.09E 03 | -6.06E 01 | -3.17E 02 | -1.10E 03 | -4.48E 00 |
| 298 | -3.57E 02 | -1.27E 03 | 2.16E 01 | -3.56E 02 | -1.27E 03 | 1.35E 00 |
| 299 | -3.33E 02 | -1.24E 03 | 4.16E 01 | -3.31E 02 | -1.24E 03 | 2.63E 00 |
| 300 | -3.76E 02 | -1.39E 03 | -2.72E 01 | -3.76E 02 | -1.39E 03 | -1.54E 00 |

| ELEMENT NO. | X | Y | EPSILON-X | EPSILON-Y | GAMA-XY |
|---|---|---|---|---|---|
| 301 | 4.11E 02 | 4.01E 02 | 1.35E-03 | -2.35E-03 | -8.60E-05 |
| 302 | 4.23E 02 | 4.01E 02 | 1.43E-03 | -2.65E-03 | 2.85E-04 |
| 303 | 4.35E 02 | 4.01E 02 | 1.44E-03 | -2.59E-03 | 3.35E-04 |
| 304 | 4.48E 02 | 4.01E 02 | 1.42E-03 | -2.66E-03 | -5.86E-05 |
| 305 | 4.62E 02 | 4.02E 02 | 1.32E-03 | -2.43E-03 | 6.89E-05 |
| 306 | 4.71E 02 | 4.00E 02 | 1.90E-03 | -3.44E-03 | 7.76E-04 |
| 307 | 3.34E 02 | 3.57E 02 | -1.04E-03 | -1.68E-03 | -4.08E-03 |
| 308 | 3.42E 02 | 3.57E 02 | 8.72E-05 | -3.35E-03 | -3.06E-03 |
| 309 | 3.53E 02 | 3.57E 02 | 5.62E-04 | -4.24E-03 | 1.02E-03 |
| 310 | 3.37E 02 | 3.62E 02 | -1.42E-03 | -2.45E-04 | -4.80E-03 |
| 311 | 3.45E 02 | 3.62E 02 | -8.57E-04 | -1.69E-03 | -2.53E-03 |
| 312 | 3.46E 02 | 3.67E 02 | -1.85E-03 | 3.24E-04 | -2.35E-03 |
| 313 | 3.55E 02 | 3.62E 02 | -1.44E-04 | -2.58E-03 | 6.45E-04 |
| 314 | 3.55E 02 | 3.67E 02 | -9.80E-04 | -6.95E-04 | 3.42E-04 |
| 315 | 3.65E 02 | 4.07E 02 | 5.60E-05 | -3.30E-04 | -2.15E-04 |
| 316 | 3.77E 02 | 4.07E 02 | 3.31E-05 | -4.32E-04 | 3.53E-05 |
| 317 | 3.89E 02 | 4.07E 02 | 4.10E-05 | -4.03E-04 | 2.45E-05 |
| 318 | 4.00E 02 | 4.07E 02 | 4.78E-05 | -4.13E-04 | -1.99E-05 |
| 319 | 4.11E 02 | 4.07E 02 | 5.46E-05 | -4.03E-04 | -3.82E-06 |
| 320 | 4.23E 02 | 4.07E 02 | 1.06E-04 | -4.30E-04 | 1.02E-04 |
| 321 | 4.35E 02 | 4.07E 02 | 1.86E-04 | -4.61E-04 | 5.66E-05 |
| 322 | 4.48E 02 | 4.07E 02 | 2.68E-04 | -4.97E-04 | 1.03E-04 |
| 323 | 4.62E 02 | 4.07E 02 | 2.83E-04 | -5.17E-04 | -2.16E-04 |
| 324 | 4.80E 02 | 4.07E 02 | 4.65E-04 | -5.30E-04 | 4.19E-04 |

| ELEMENT NO. | SIGMA-X | SIGMA-Y | TAU-XY | SIGMA-1 | SIGMA-2 | ANG |
|---|---|---|---|---|---|---|
| 301 | 2.01E 02 | -1.10E 03 | -1.73E 01 | 2.01E 02 | -1.10E 03 | -7.62E-01 |
| 302 | 1.85E 02 | -1.26E 03 | 5.08E 01 | 1.86E 02 | -1.26E 03 | 2.02E 00 |
| 303 | 2.16E 02 | -1.22E 03 | 5.93E 01 | 2.18E 02 | -1.22E 03 | 2.36E 00 |
| 304 | 1.92E 02 | -1.28E 03 | -1.59E 01 | 1.93E 02 | -1.28E 03 | -6.18E-01 |
| 305 | 1.88E 02 | -1.12E 03 | 1.55E 01 | 1.88E 02 | -1.12E 03 | 6.79E-01 |
| 306 | 2.83E 02 | -1.48E 03 | 1.43E 02 | 2.95E 02 | -1.49E 03 | 4.63E 00 |
| 307 | -6.03E 02 | -7.36E 02 | -3.99E 02 | -2.65E 02 | -1.07E 03 | -4.03E 01 |
| 308 | -4.53E 02 | -1.14E 03 | -2.90E 02 | -3.47E 02 | -1.25E 03 | -2.01E 01 |
| 309 | -4.25E 02 | -1.36E 03 | 1.23E 02 | -4.09E 02 | -1.37E 03 | 7.40E 00 |
| 310 | -5.36E 02 | -2.97E 02 | -4.86E 02 | 8.40E 01 | -9.16E 02 | 1.28E 02 |
| 311 | -5.42E 02 | -7.42E 02 | -2.43E 02 | -3.79E 02 | -9.04E 02 | -3.38E 01 |
| 312 | -6.23E 02 | -1.85E 02 | -2.54E 02 | -6.91E 01 | -7.40E 02 | 1.15E 02 |
| 313 | -4.17E 02 | -8.95E 02 | 1.10E 02 | -3.93E 02 | -9.19E 02 | 1.23E 01 |
| 314 | -3.89E 02 | -3.48E 02 | 8.56E 01 | -2.81E 02 | -4.57E 02 | 5.17E 01 |
| 315 | -9.10E 01 | -3.26E 02 | -6.54E 01 | -7.40E 01 | -3.43E 02 | -1.46E 01 |
| 316 | -1.62E 02 | -4.45E 02 | 1.07E 01 | -1.61E 02 | -4.45E 02 | 2.17E 00 |
| 317 | -1.40E 02 | -4.10E 02 | 7.46E 00 | -1.40E 02 | -4.11E 02 | 1.58E 00 |
| 318 | -1.38E 02 | -4.19E 02 | -6.06E 00 | -1.38E 02 | -4.19E 02 | -1.23E 00 |
| 319 | -1.26E 02 | -4.06E 02 | -1.16E 00 | -1.26E 02 | -4.06E 02 | -2.39E-01 |
| 320 | -8.31E 01 | -4.11E 02 | 3.11E 01 | -8.02E 01 | -4.14E 02 | 5.38E 00 |
| 321 | -1.21E 01 | -4.07E 02 | 1.73E 01 | -1.13E 01 | -4.08E 02 | 2.50E 00 |
| 322 | 5.84E 01 | -4.10E 02 | 3.14E 01 | 6.05E 01 | -4.12E 02 | 3.82E 00 |
| 323 | 6.60E 01 | -4.25E 02 | -6.62E 01 | 7.48E 01 | -4.33E 02 | -7.55E 00 |
| 324 | 2.41E 02 | -3.35E 02 | 1.21E 02 | 2.65E 02 | -3.59E 02 | 1.14E 01 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCE |
|---|---|---|---|---|---|
| 1 | 0.0 | 0.0 | 38 | -1.51E-01 | -5.60E-01 |
| 2 | 0.0 | -2.34E-01 | 39 | -1.97E-01 | -6.51E-01 |
| 3 | 0.0 | -4.33E-01 | 40 | -3.25E-01 | -8.82E-01 |
| 4 | 0.0 | -5.08E-01 | 41 | -5.44E-01 | -1.25E 00 |
| 5 | 0.0 | -6.59E-01 | 42 | -6.22E-01 | -1.32E 00 |
| 6 | 0.0 | 0.0 | 43 | 0.0 | 0.0 |
| 7 | 0.0 | 0.0 | 44 | -4.24E-02 | -2.70E-01 |
| 8 | 0.0 | 0.0 | 45 | -1.60E-01 | -5.73E-01 |
| 9 | -2.48E-02 | -2.39E-01 | 46 | -2.66E-01 | -7.74E-01 |
| 10 | -4.88E-02 | -4.41E-01 | 47 | -3.86E-01 | -9.75E-01 |
| 11 | -7.56E-02 | -5.15E-01 | 48 | -6.30E-01 | -1.36E 00 |
| 12 | -1.29E-01 | -6.78E-01 | 49 | -7.00E-01 | -1.44E 00 |
| 13 | -1.88E-01 | -7.77E-01 | 50 | 0.0 | 0.0 |
| 14 | 0.0 | 0.0 | 51 | 0.0 | 0.0 |
| 15 | 0.0 | 0.0 | 52 | 0.0 | 0.0 |
| 16 | -4.20E-02 | -2.49E-01 | 53 | -5.11E-02 | -2.92E-01 |
| 17 | -8.98E-02 | -4.72E-01 | 54 | -1.67E-01 | -5.77E-01 |
| 18 | -1.30E-01 | -5.74E-01 | 55 | -2.92E-01 | -8.17E-01 |
| 19 | -2.93E-01 | -9.06E-01 | 56 | -4.33E-01 | -1.05E 00 |
| 20 | -2.97E-01 | -9.62E-01 | 57 | -7.00E-01 | -1.47E 00 |
| 21 | 0.0 | 0.0 | 58 | -7.75E-01 | -1.56E 00 |
| 22 | 0.0 | 0.0 | 59 | 0.0 | 0.0 |
| 23 | -4.97E-02 | -2.59E-01 | 60 | 0.0 | 0.0 |
| 24 | -1.14E-01 | -5.02E-01 | 61 | 0.0 | 0.0 |
| 25 | -2.04E-01 | -6.92E-01 | 62 | -6.19E-02 | -2.94E-01 |
| 26 | -3.70E-01 | -9.99E-01 | 63 | -1.72E-01 | -5.81E-01 |
| 27 | -3.76E-01 | -1.04E 00 | 64 | -3.12E-01 | -8.52E-01 |
| 28 | 0.0 | 0.0 | 65 | -4.76E-01 | -1.13E 00 |
| 29 | 0.0 | 0.0 | 66 | -7.64E-01 | -1.58E 00 |
| 30 | -4.94E-02 | -2.70E-01 | 67 | -8.44E-01 | -1.68E 00 |
| 31 | -1.36E-01 | -5.35E-01 | 68 | 0.0 | 0.0 |
| 32 | -2.50E-01 | -7.60E-01 | 69 | 0.0 | 0.0 |
| 33 | -4.44E-01 | -1.11E 00 | 70 | 0.0 | 0.0 |
| 34 | -5.03E-01 | -1.16E 00 | 71 | -7.02E-02 | -2.93E-01 |
| 35 | 0.0 | 0.0 | 72 | -1.75E-01 | -5.68E-01 |
| 36 | 0.0 | 0.0 | 73 | -3.29E-01 | -8.82E-01 |
| 37 | -4.51E-02 | -2.75E-01 | 74 | -5.15E-01 | -1.19E 00 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 75 | -8.23E-01 | -1.68E 00 | 112 | -1.06E 00 | -2.12E 00 |
| 76 | -9.08E-01 | -1.79E 00 | 113 | -1.11E 00 | -2.16E 00 |
| 77 | 0.0 | 0.0 | 114 | 0.0 | 0.0 |
| 78 | 0.0 | 0.0 | 115 | 0.0 | 0.0 |
| 79 | 0.0 | 0.0 | 116 | -9.50E-02 | -2.73E-01 |
| 80 | -7.78E-02 | -2.93E-01 | 117 | -2.10E-01 | -5.47E-01 |
| 81 | -1.88E-01 | -5.78E-01 | 118 | -4.12E-01 | -9.63E-01 |
| 82 | -3.53E-01 | -9.16E-01 | 119 | -6.52E-01 | -1.39E 00 |
| 83 | -5.50E-01 | -1.25E 00 | 120 | -9.24E-01 | -1.88E 00 |
| 84 | -8.77E-01 | -1.78E 00 | 121 | -1.11E 00 | -2.16E 00 |
| 85 | -9.67E-01 | -1.90E 00 | 122 | -1.16E 00 | -2.24E 00 |
| 86 | 0.0 | 0.0 | 123 | 0.0 | 0.0 |
| 87 | 0.0 | 0.0 | 124 | 0.0 | 0.0 |
| 88 | 0.0 | 0.0 | 125 | -9.67E-02 | -2.65E-01 |
| 89 | -8.40E-02 | -2.92E-01 | 126 | -2.08E-01 | -5.26E-01 |
| 90 | -1.98E-01 | -5.80E-01 | 127 | -3.66E-01 | -8.61E-01 |
| 91 | -3.72E-01 | -9.38E-01 | 128 | -5.53E-01 | -1.20E 00 |
| 92 | -5.81E-01 | -1.30E 00 | 129 | -6.83E-01 | -1.42E 00 |
| 93 | -9.27E-01 | -1.86E 00 | 130 | -9.65E-01 | -1.92E 00 |
| 94 | -1.02E 00 | -2.00E 00 | 131 | -1.15E 00 | -2.21E 00 |
| 95 | 0.0 | 0.0 | 132 | -1.21E 00 | -2.29E 00 |
| 96 | 0.0 | 0.0 | 133 | 0.0 | 0.0 |
| 97 | 0.0 | 0.0 | 134 | -9.83E-02 | -2.62E-01 |
| 98 | -8.88E-02 | -2.88E-01 | 135 | -2.13E-01 | -5.27E-01 |
| 99 | -2.06E-01 | -5.75E-01 | 136 | -3.82E-01 | -8.74E-01 |
| 100 | -3.88E-01 | -9.49E-01 | 137 | -5.77E-01 | -1.22E 00 |
| 101 | -6.05E-01 | -1.33E 00 | 138 | -7.13E-01 | -1.45E 00 |
| 102 | -9.71E-01 | -1.95E 00 | 139 | -9.97E-01 | -1.95E 00 |
| 103 | -1.06E 00 | -2.08E 00 | 140 | -1.18E 00 | -2.25E 00 |
| 104 | 0.0 | 0.0 | 141 | -1.25E 00 | -2.33E 00 |
| 105 | 0.0 | 0.0 | 142 | 0.0 | 0.0 |
| 106 | 0.0 | 0.0 | 143 | -9.91E-02 | -2.59E-01 |
| 107 | -9.25E-02 | -2.81E-01 | 144 | -2.17E-01 | -5.24E-01 |
| 108 | -2.09E-01 | -5.64E-01 | 145 | -3.95E-01 | -8.81E-01 |
| 109 | -4.01E-01 | -9.57E-01 | 146 | -5.98E-01 | -1.24E 00 |
| 110 | -6.22E-01 | -1.35E 00 | 147 | -7.39E-01 | -1.47E 00 |
| 111 | -8.78E-01 | -1.81E 00 | 148 | -1.03E 00 | -1.97E 00 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 149 | -1.22E 00 | -2.27E 00 | 186 | -1.04E 00 | -1.94E 00 |
| 150 | -1.28E 00 | -2.36E 00 | 187 | -1.25E 00 | -2.21E 00 |
| 151 | 0.0 | 0.0 | 188 | -1.36E 00 | -2.35E 00 |
| 152 | -9.89E-02 | -2.54E-01 | 189 | -1.42E 00 | -2.40E 00 |
| 153 | -2.18E-01 | -5.19E-01 | 190 | -1.41E 00 | -2.39E 00 |
| 154 | -4.04E-01 | -8.84E-01 | 191 | -7.09E-02 | -2.84E-01 |
| 155 | -6.16E-01 | -1.25E 00 | 192 | -6.02E-02 | -2.40E-01 |
| 156 | -7.61E-01 | -1.49E 00 | 193 | -6.83E-02 | -3.15E-01 |
| 157 | -1.05E 00 | -1.99E 00 | 194 | -6.50E-02 | -3.12E-01 |
| 158 | -1.25E 00 | -2.29E 00 | 195 | -1.23E 00 | -2.18E 00 |
| 159 | -1.32E 00 | -2.38E 00 | 196 | -1.34E 00 | -2.30E 00 |
| 160 | 0.0 | 0.0 | 197 | -1.37E 00 | -2.35E 00 |
| 161 | -9.76E-02 | -2.47E-01 | 198 | -7.37E-02 | -3.20E-01 |
| 162 | -2.16E-01 | -5.11E-01 | 199 | -7.87E-02 | -3.27E-01 |
| 163 | -4.08E-01 | -8.84E-01 | 200 | -8.36E-02 | -3.27E-01 |
| 164 | -6.28E-01 | -1.26E 00 | 201 | 0.0 | 0.0 |
| 165 | -7.80E-01 | -1.50E 00 | 202 | -9.33E-02 | -2.23E-01 |
| 166 | -1.07E 00 | -2.00E 00 | 203 | -2.09E-01 | -4.72E-01 |
| 167 | -1.27E 00 | -2.30E 00 | 204 | -3.98E-01 | -8.58E-01 |
| 168 | -1.35E 00 | -2.39E 00 | 205 | -6.33E-01 | -1.28E 00 |
| 169 | 0.0 | 0.0 | 206 | -8.07E-01 | -1.55E 00 |
| 170 | -9.55E-02 | -2.39E-01 | 207 | -1.11E 00 | -2.06E 00 |
| 171 | -2.12E-01 | -4.98E-01 | 208 | -1.25E 00 | -2.28E 00 |
| 172 | -4.07E-01 | -8.79E-01 | 209 | -1.40E 00 | -2.51E 00 |
| 173 | -6.34E-01 | -1.27E 00 | 210 | -4.16E-01 | -1.47E 00 |
| 174 | -1.29E 00 | -2.25E 00 | 211 | -4.58E-01 | -1.55E 00 |
| 175 | -1.34E 00 | -2.32E 00 | 212 | -4.93E-01 | -1.56E 00 |
| 176 | -7.94E-01 | -1.52E 00 | 213 | -4.94E-01 | -1.49E 00 |
| 177 | -1.09E 00 | -2.02E 00 | 214 | -5.04E-01 | -1.46E 00 |
| 178 | -1.31E 00 | -2.31E 00 | 215 | -5.34E-01 | -1.52E 00 |
| 179 | -1.38E 00 | -2.40E 00 | 216 | -4.77E-01 | -1.29E 00 |
| 180 | 0.0 | 0.0 | 217 | -4.94E-01 | -1.31E 00 |
| 181 | -9.35E-02 | -2.30E-01 | 218 | -4.28E-01 | -1.07E 00 |
| 182 | -2.06E-01 | -4.79E-01 | 219 | -4.50E-01 | -1.09E 00 |
| 183 | -4.00E-01 | -8.68E-01 | 220 | -2.85E-01 | -6.26E-01 |
| 184 | -6.34E-01 | -1.28E 00 | 221 | -9.27E-02 | -2.31E-01 |
| 185 | -8.05E-01 | -1.53E 00 | 222 | 0.0 | 0.0 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 223 | -9.52E-02 | -2.15E-01 | 260 | -4.18E-01 | -9.72E-01 |
| 224 | -2.14E-01 | -4.59E-01 | 261 | -4.42E-01 | -9.92E-01 |
| 225 | -3.96E-01 | -8.34E-01 | 262 | -2.80E-01 | -5.67E-01 |
| 226 | -6.28E-01 | -1.27E 00 | 263 | -9.33E-02 | -2.33E-01 |
| 227 | -7.97E-01 | -1.55E 00 | 264 | 0.0 | 0.0 |
| 228 | -9.51E-01 | -1.87E 00 | 265 | -1.08E-01 | -1.97E-01 |
| 229 | -1.11E 00 | -2.14E 00 | 266 | -2.37E-01 | -4.20E-01 |
| 230 | -1.31E 00 | -2.43E 00 | 267 | -4.05E-01 | -7.41E-01 |
| 231 | -4.10E-01 | -1.51E 00 | 268 | -6.32E-01 | -1.15E 00 |
| 232 | -4.54E-01 | -1.51E 00 | 269 | -8.11E-01 | -1.43E 00 |
| 233 | -4.87E-01 | -1.50E 00 | 270 | 0.0 | 0.0 |
| 234 | -4.86E-01 | -1.42E 00 | 271 | 0.0 | 0.0 |
| 235 | -4.97E-01 | -1.39E 00 | 272 | -1.02E 00 | -1.79E 00 |
| 236 | -5.28E-01 | -1.45E 00 | 273 | -4.07E-01 | -1.33E 00 |
| 237 | -4.72E-01 | -1.23E 00 | 274 | -4.51E-01 | -1.36E 00 |
| 238 | -4.89E-01 | -1.26E 00 | 275 | -4.81E-01 | -1.35E 00 |
| 239 | -4.23E-01 | -1.02E 00 | 276 | -4.76E-01 | -1.28E 00 |
| 240 | -4.46E-01 | -1.04E 00 | 277 | -4.86E-01 | -1.25E 00 |
| 241 | -2.83E-01 | -6.01E-01 | 278 | -5.19E-01 | -1.31E 00 |
| 242 | -9.27E-02 | -2.35E-01 | 279 | -4.62E-01 | -1.11E 00 |
| 243 | 0.0 | 0.0 | 280 | -4.80E-01 | -1.13E 00 |
| 244 | -9.98E-02 | -2.07E-01 | 281 | -4.14E-01 | -9.17E-01 |
| 245 | -2.23E-01 | -4.42E-01 | 282 | -4.39E-01 | -9.37E-01 |
| 246 | -3.97E-01 | -7.94E-01 | 283 | -2.76E-01 | -5.31E-01 |
| 247 | -6.26E-01 | -1.23E 00 | 284 | -9.30E-02 | -2.29E-01 |
| 248 | -7.97E-01 | -1.51E 00 | 285 | 0.0 | 0.0 |
| 249 | -8.67E-01 | -1.74E 00 | 286 | -1.21E-01 | -1.88E-01 |
| 250 | -9.49E-01 | -1.84E 00 | 287 | -2.58E-01 | -3.93E-01 |
| 251 | -1.18E 00 | -2.13E 00 | 288 | -4.19E-01 | -6.82E-01 |
| 252 | -4.08E-01 | -1.45E 00 | 289 | -6.49E-01 | -1.06E 00 |
| 253 | -4.52E-01 | -1.47E 00 | 290 | -8.20E-01 | -1.30E 00 |
| 254 | -4.84E-01 | -1.45E 00 | 291 | -8.81E-01 | -1.44E 00 |
| 255 | -4.81E-01 | -1.36E 00 | 292 | 0.0 | 0.0 |
| 256 | -4.91E-01 | -1.33E 00 | 293 | 0.0 | 0.0 |
| 257 | -5.23E-01 | -1.39E 00 | 294 | -4.07E-01 | -1.17E 00 |
| 258 | -4.66E-01 | -1.17E 00 | 295 | -4.49E-01 | -1.21E 00 |
| 259 | -4.84E-01 | -1.20E 00 | 296 | -4.78E-01 | -1.23E 00 |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 297 | -4.72E-01 | -1.18E 00 | 334 | 0.0 | 0.0 |
| 298 | -4.81E-01 | -1.16E 00 | 335 | 0.0 | 0.0 |
| 299 | -5.15E-01 | -1.22E 00 | 336 | 0.0 | 0.0 |
| 300 | -4.57E-01 | -1.04E 00 | 337 | 0.0 | 0.0 |
| 301 | -4.75E-01 | -1.07E 00 | 338 | 0.0 | 0.0 |
| 302 | -4.10E-01 | -8.66E-01 | 339 | -3.56E-01 | -8.85E-01 |
| 303 | -4.36E-01 | -8.90E-01 | 340 | -3.54E-01 | -8.31E-01 |
| 304 | -2.72E-01 | -5.05E-01 | 341 | -4.22E-01 | -9.40E-01 |
| 305 | -9.26E-02 | -2.26E-01 | 342 | -3.74E-01 | -8.37E-01 |
| 306 | 0.0 | 0.0 | 343 | -4.15E-01 | -8.80E-01 |
| 307 | -1.42E-01 | -1.80E-01 | 344 | -3.56E-01 | -7.17E-01 |
| 308 | -2.84E-01 | -3.64E-01 | 345 | -3.96E-01 | -7.46E-01 |
| 309 | -4.37E-01 | -6.18E-01 | 346 | -2.44E-01 | -4.33E-01 |
| 310 | -6.52E-01 | -9.70E-01 | 347 | -9.36E-02 | -2.04E-01 |
| 311 | -7.69E-01 | -1.18E 00 | 348 | 0.0 | 0.0 |
| 312 | 0.0 | 0.0 | 349 | -2.27E-01 | -1.64E-01 |
| 313 | 0.0 | 0.0 | 350 | -3.36E-01 | -3.01E-01 |
| 314 | 0.0 | 0.0 | 351 | -4.64E-01 | -4.94E-01 |
| 315 | 0.0 | 0.0 | 352 | -6.33E-01 | -7.76E-01 |
| 316 | -4.04E-01 | -1.09E 00 | 353 | -7.24E-01 | -9.26E-01 |
| 317 | -3.88E-01 | -1.02E 00 | 354 | -3.72E-01 | -7.57E-01 |
| 318 | -4.13E-01 | -1.04E 00 | 355 | -3.09E-01 | -6.24E-01 |
| 319 | -4.30E-01 | -1.05E 00 | 356 | -3.76E-01 | -7.31E-01 |
| 320 | -4.77E-01 | -1.11E 00 | 357 | -3.24E-01 | -6.16E-01 |
| 321 | -4.19E-01 | -9.51E-01 | 358 | -3.73E-01 | -6.45E-01 |
| 322 | -4.40E-01 | -9.83E-01 | 359 | -2.27E-01 | -3.83E-01 |
| 323 | -3.86E-01 | -8.05E-01 | | | |
| 324 | -4.20E-01 | -8.34E-01 | | | |
| 325 | -2.58E-01 | -4.77E-01 | | | |
| 326 | -9.35E-02 | -2.19E-01 | | | |
| 327 | 0.0 | 0.0 | | | |
| 328 | -1.72E-01 | -1.75E-01 | | | |
| 329 | -3.16E-01 | -3.30E-01 | | | |
| 330 | -4.51E-01 | -5.55E-01 | | | |
| 331 | -6.41E-01 | -8.78E-01 | | | |
| 332 | -7.43E-01 | -1.06E 00 | | | |
| 333 | 0.0 | 0.0 | | | |

| NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT | NODAL POINT | X DISPLCEMNT | Y DISPLCEMNT |
|---|---|---|---|---|---|
| 360 | -9.26E-02 | -1.85E-01 | 386 | 0.0 | 0.0 |
| 361 | -1.17E-01 | -8.82E-02 | 387 | -2.59E-01 | -1.96E-01 |
| 362 | -2.57E-01 | -1.49E-01 | 388 | -3.19E-01 | -2.10E-01 |
| 363 | -3.66E-01 | -2.74E-01 | 389 | -3.96E-01 | -2.60E-01 |
| 364 | -4.76E-01 | -4.23E-01 | 390 | -4.87E-01 | -3.48E-01 |
| 365 | -6.28E-01 | -6.66E-01 | 391 | -6.03E-01 | -4.83E-01 |
| 366 | -7.01E-01 | -7.89E-01 | 392 | -6.28E-01 | -5.36E-01 |
| 367 | -3.45E-01 | -6.13E-01 | 393 | 0.0 | 0.0 |
| 368 | -2.87E-01 | -4.82E-01 | 394 | 0.0 | 0.0 |
| 369 | -3.41E-01 | -5.15E-01 | 395 | 0.0 | 0.0 |
| 370 | -2.09E-01 | -3.24E-01 | 396 | 0.0 | 0.0 |
| 371 | -8.82E-02 | -1.60E-01 | 397 | 0.0 | 0.0 |
| 372 | 0.0 | 0.0 | 398 | 0.0 | 0.0 |
| 373 | 0.0 | 0.0 | 399 | 0.0 | 0.0 |
| 374 | -1.99E-01 | -1.51E-01 | 400 | -3.00E-01 | -2.27E-01 |
| 375 | -2.89E-01 | -1.73E-01 | 401 | -3.39E-01 | -2.55E-01 |
| 376 | -3.87E-01 | -2.54E-01 | 402 | -3.91E-01 | -2.92E-01 |
| 377 | -4.87E-01 | -3.72E-01 | 403 | -4.73E-01 | -3.57E-01 |
| 378 | -6.21E-01 | -5.60E-01 | 404 | -5.70E-01 | -4.47E-01 |
| 379 | -6.76E-01 | -6.50E-01 | 405 | -5.97E-01 | -4.66E-01 |
| 380 | -3.26E-01 | -3.94E-01 | 406 | -3.11E-01 | -2.35E-01 |
| 381 | -1.93E-01 | -2.41E-01 | 407 | -3.37E-01 | -3.29E-01 |
| 382 | -8.78E-02 | -1.30E-01 | 408 | -3.79E-01 | -3.39E-01 |
| 383 | 0.0 | 0.0 | 409 | -4.28E-01 | -4.12E-01 |
| 384 | 0.0 | 0.0 | 410 | -4.44E-01 | -4.40E-01 |
| 385 | 0.0 | 0.0 | 411 | -2.86E-01 | -5.55E-01 |
| | | | 412 | -0.21 | -0.71 |
| | | | 413 | -0.31 | -0.40 |