

Large Scale Laboratory Testing in Support of Seismic Bridge Design and Retrofit



Frieder Seible, Ph.D., P.E.

Dean, Jacobs School of Engineering

Director, Powell Structural Research Laboratories

University of California, San Diego

OVERVIEW

- Seismic Bridge Performance and Retrofit Issues
- California Seismic Bridge Retrofit Program
- Research in Support of Seismic Assessment and Retrofit Technology Development
 - Large Scale Testing of Retrofit Concepts
 - New Materials for Seismic Bridge Retrofit
 - Seismic Response Modification
 - New Bridge Design
- Multi Hazards
- Conclusions

Bridge Failures, 71 San Fernando



Bridge Failures, 89 Loma Prieta



Bridge Failures, 94 Northridge



Caltrans Bridge Retrofit Program

Restrainers
Single Column Bents
Multi Column Bents
(Foundations)
Toll Bridges

Example: Single Column Bents

Column Jacketing



a) Research



b) Implementation

Column Jacket Retrofit



a) Steel Jacketing

b) Carbon Fiber Jacketing

c) Concrete Jacketing

Foundation Retrofit



a) Addition of Piles

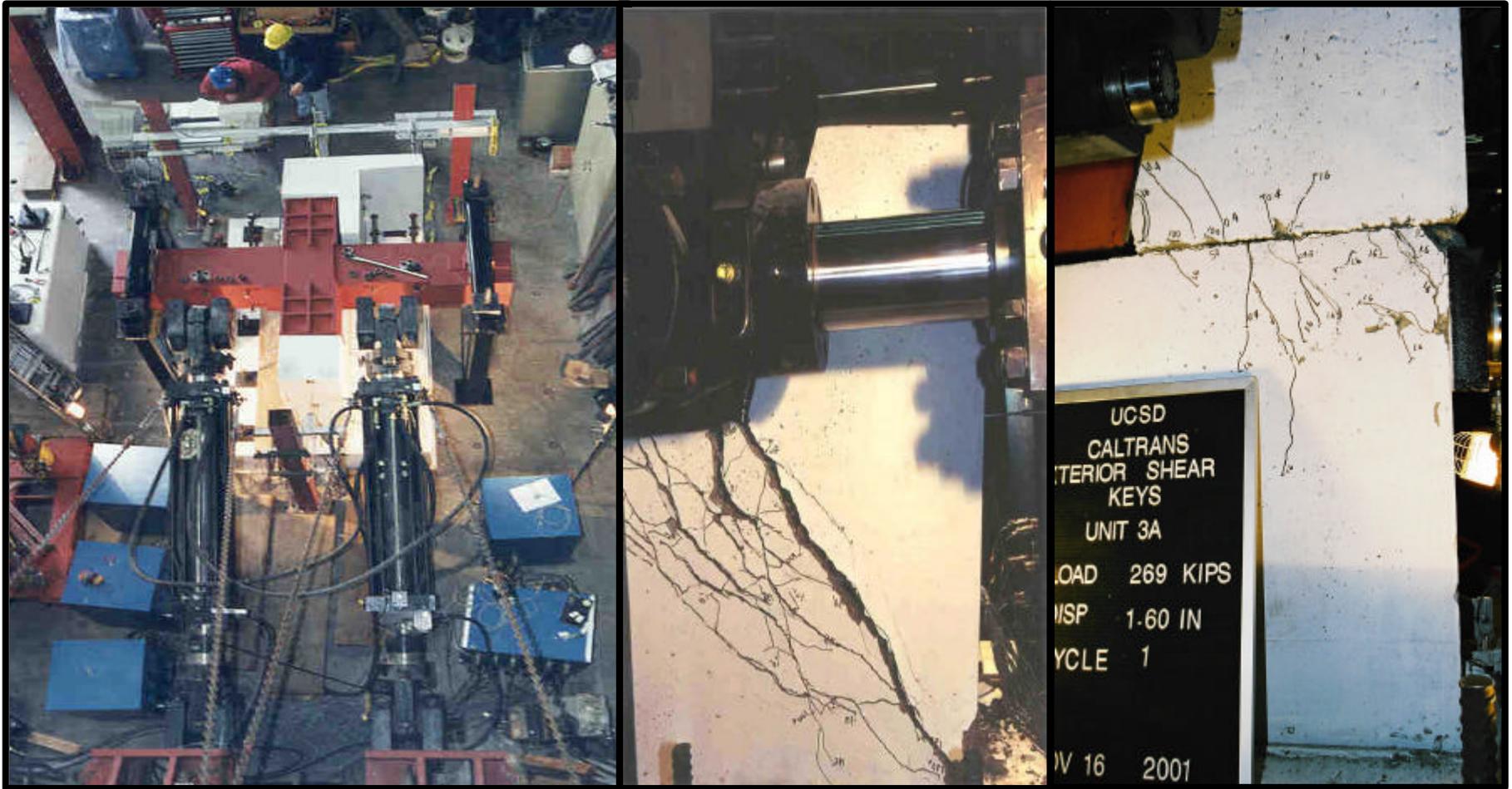


b) Reinforced Concrete Footing Overlay

Abutment Response, I-5/SR-14 Northridge 94



External Abutment Shear Key Testing



a) Test Setup

b) Shear Key Failure Modes

MAIN CAUSES FOR SEISMIC PERFORMANCE PROBLEMS IN BRIDGES

- Reinforcement Design and Detailing
 - Confinement
 - Force Transfer, Strength
 - Development Length
- Bridge Systems Response
 - SFSI
 - Stiffness/Capacity Unbalance
 - Dynamic Inelastic Systems Response

RESEARCH ON BRIDGE ASSESSMENT AND RETROFIT

- Analytical Simulations
 - Demand Assessment
 - Capacity/Performance Assessment
- Large Scale Experimental Testing
 - Component Tests
 - System Tests

LARGE SCALE EXPERIMENTAL TESTING

- Controlled laboratory environment for quality data
- Large or full-scale to exhibit representative damage patterns and failure modes
- Performed under realistic earthquake simulations, test protocols which represent actual demands

EXAMPLES OF SEISMIC BRIDGE PERFORMANCE AND RETROFIT RESEARCH

1. San Francisco Double Deck Viaduct
2. Seismic Response Modification
3. SFOBB East Span Replacement

SAN FRANCISCO DOUBLE DECK VIADUCT

- Column Capacities
- Joint Shear Force Transfer
- Cap Beam Capacities
- Longitudinal Seismic Response



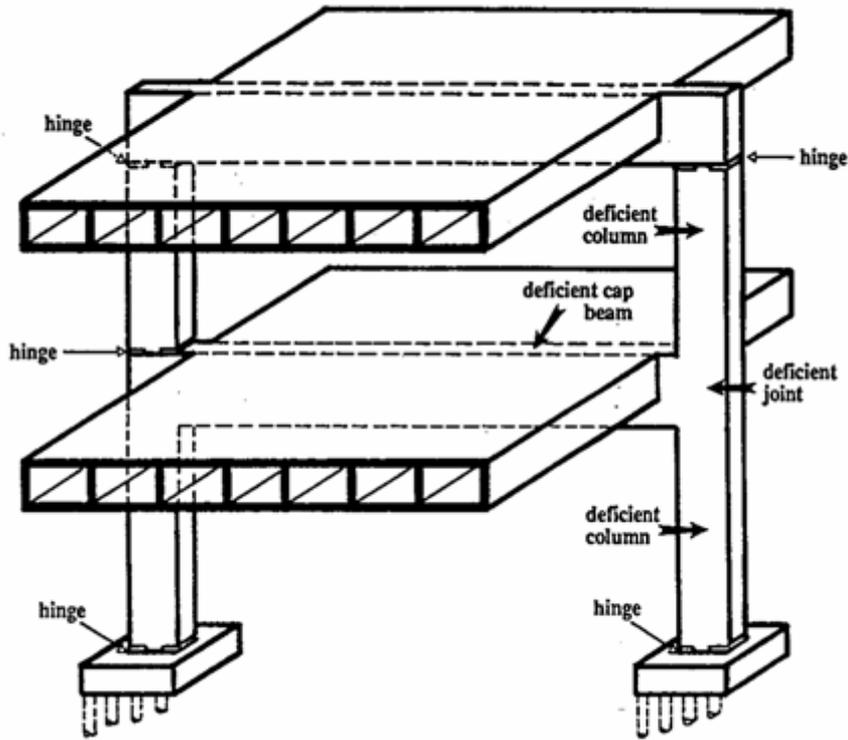
Joint Failures, Loma Prieta, 1989



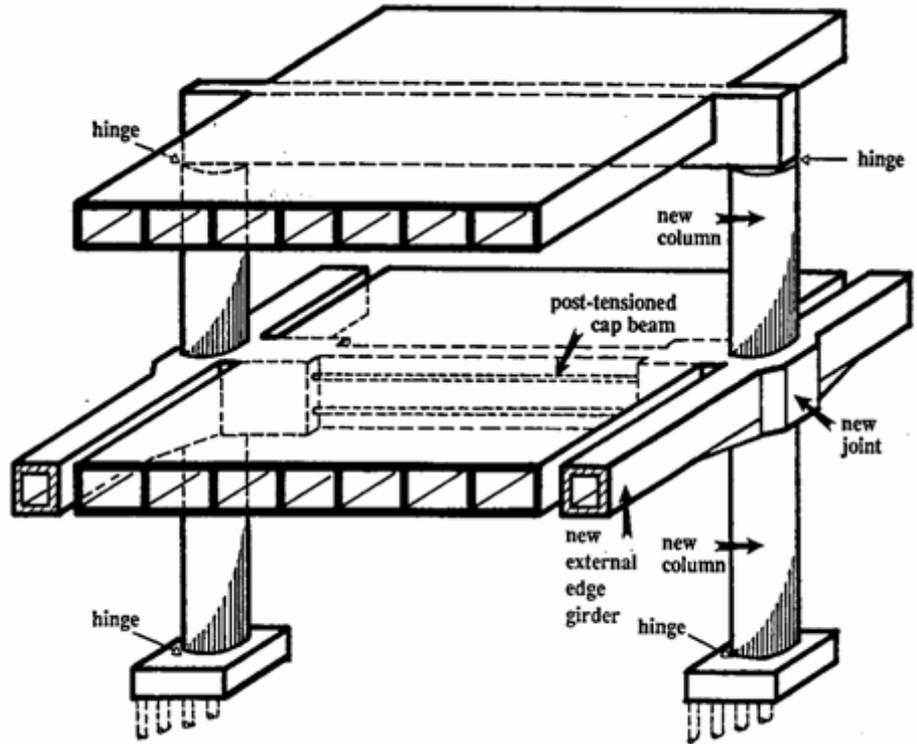
a) I-280 Viaduct



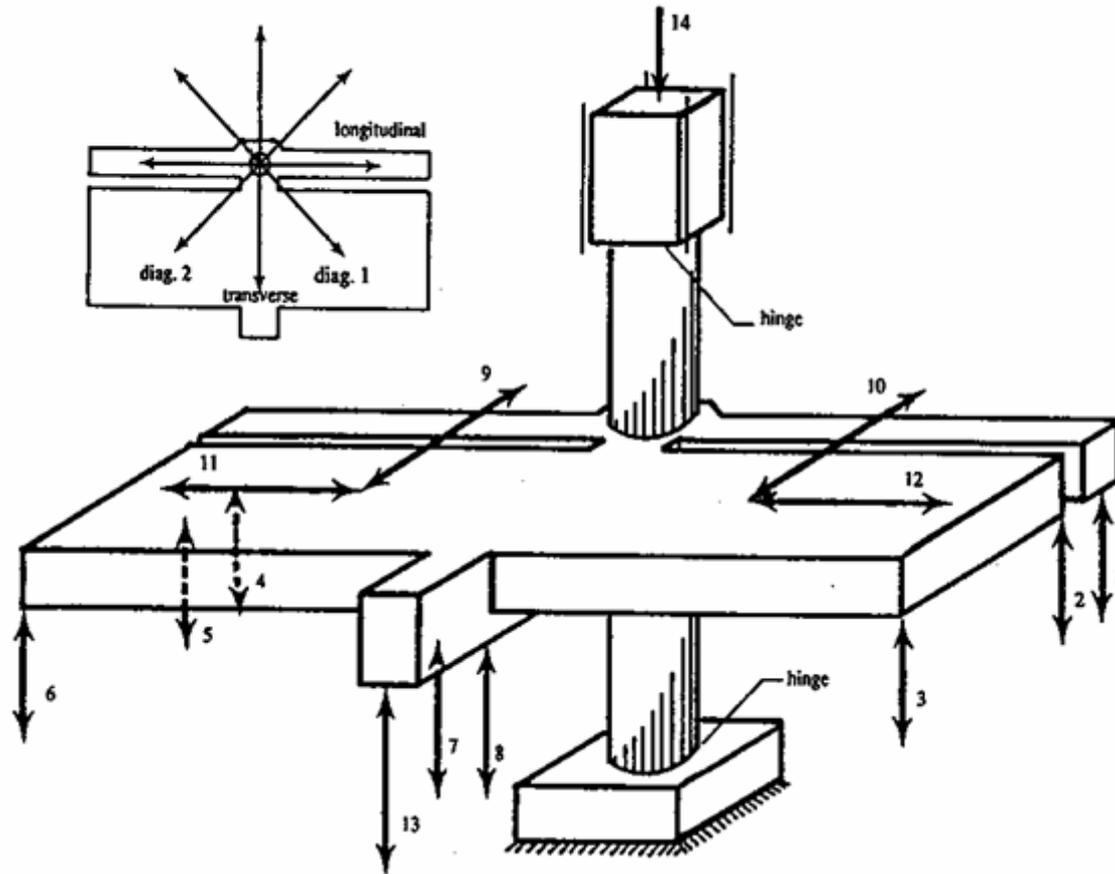
b) I-880 Cypress Viaduct



As-Built Double Deck Viaduct



Retrofit Scheme for Double Deck Viaduct



Proof test Setup with 14 Servo-Controlled Actuators

Half-Scale Proof-Test Model



Large Scale Test on Retrofitted Joint Region



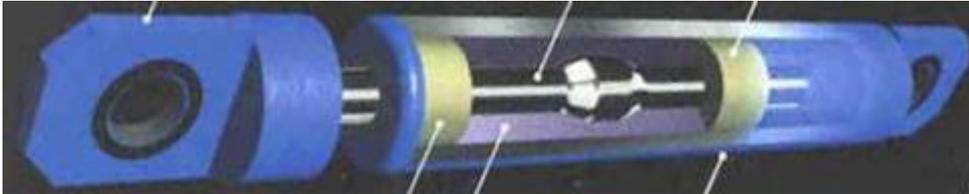
SF DOUBLE DECK VIADUCT RETROFIT



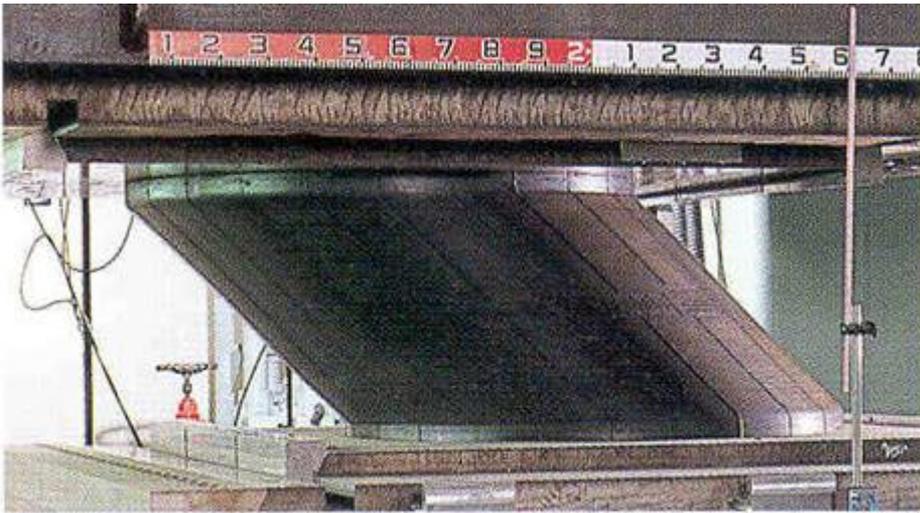
SEISMIC RESPONSE MODIFICATION

- SRMDs (Isolation Bearings, Dampers, Lock-up Devices)
- Displacement/Deformation Control
- Force Limiting Mechanisms

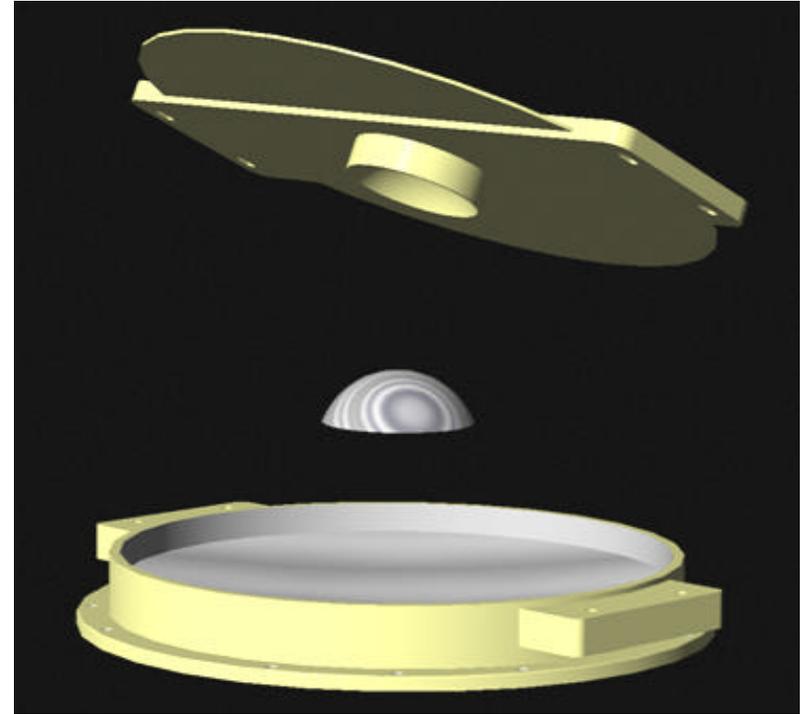
Various SRMD Examples



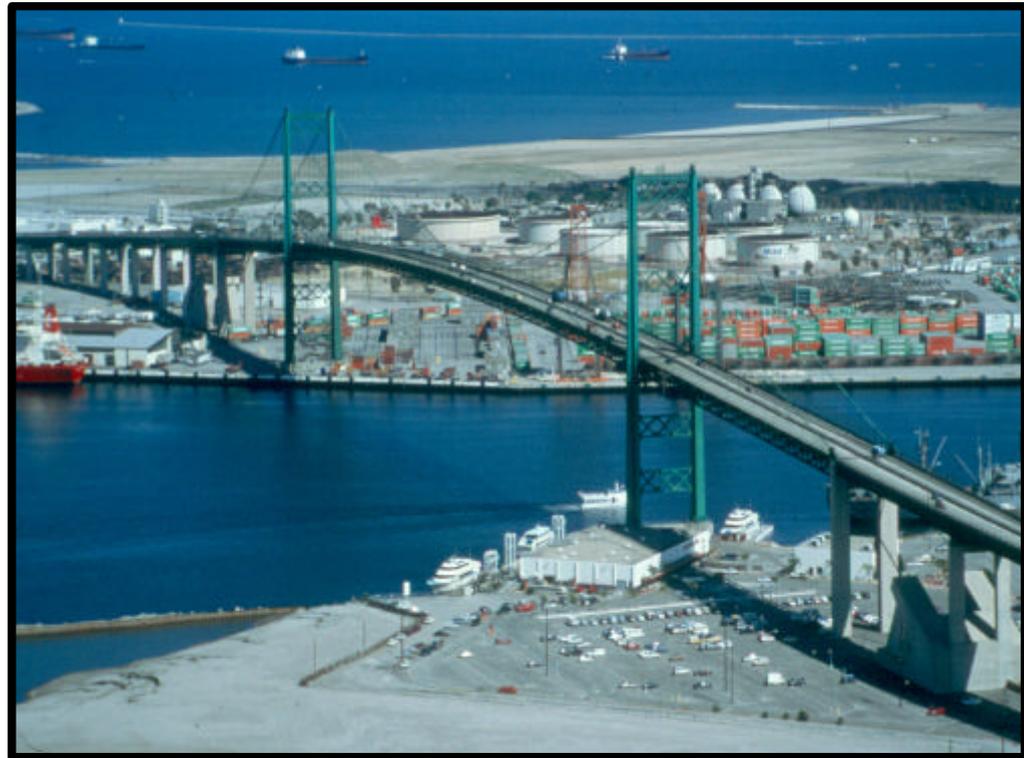
Dampers



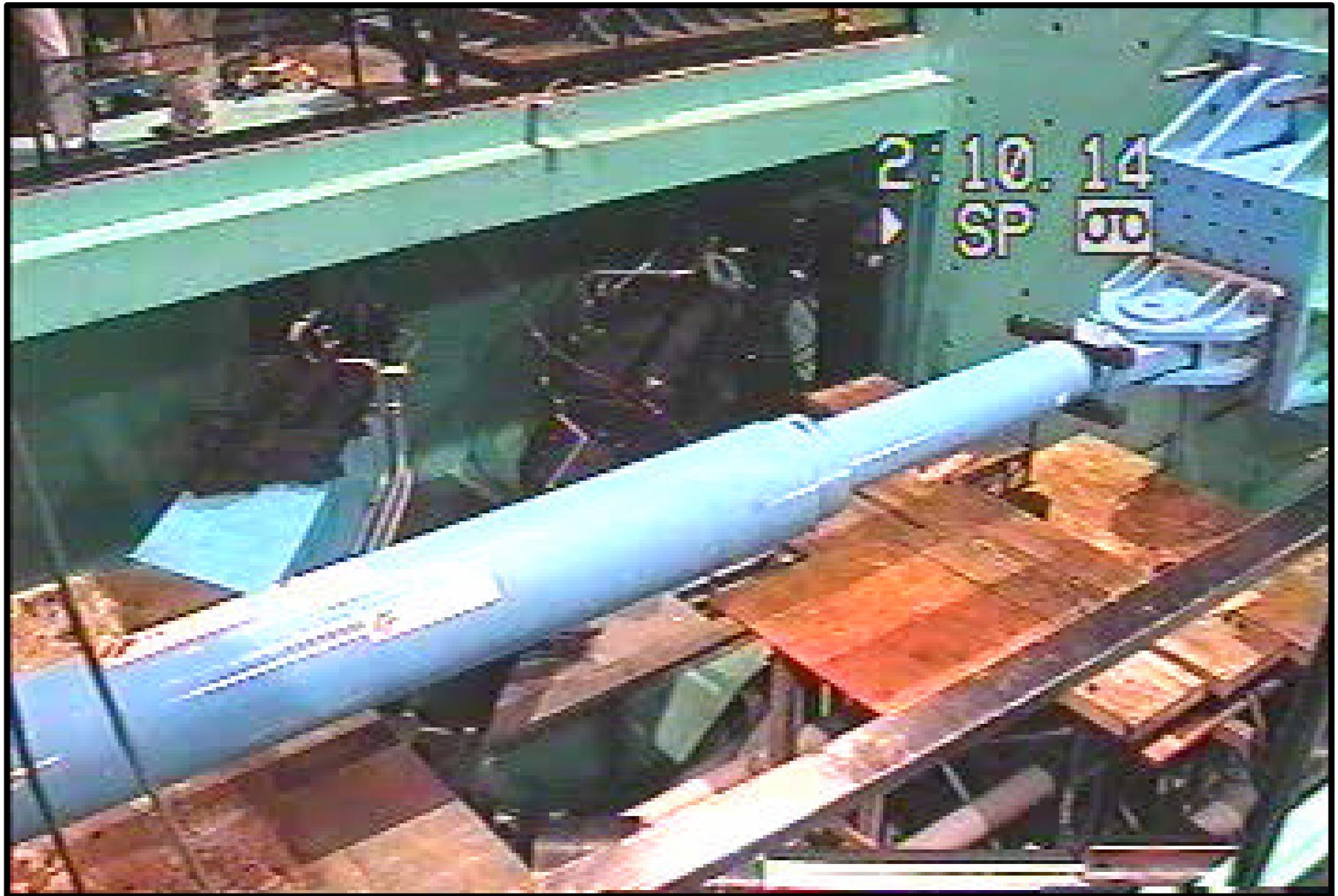
Elastomeric Bearings



Friction Pendulum Bearings







BENICIA-MARTINEZ BRIDGE

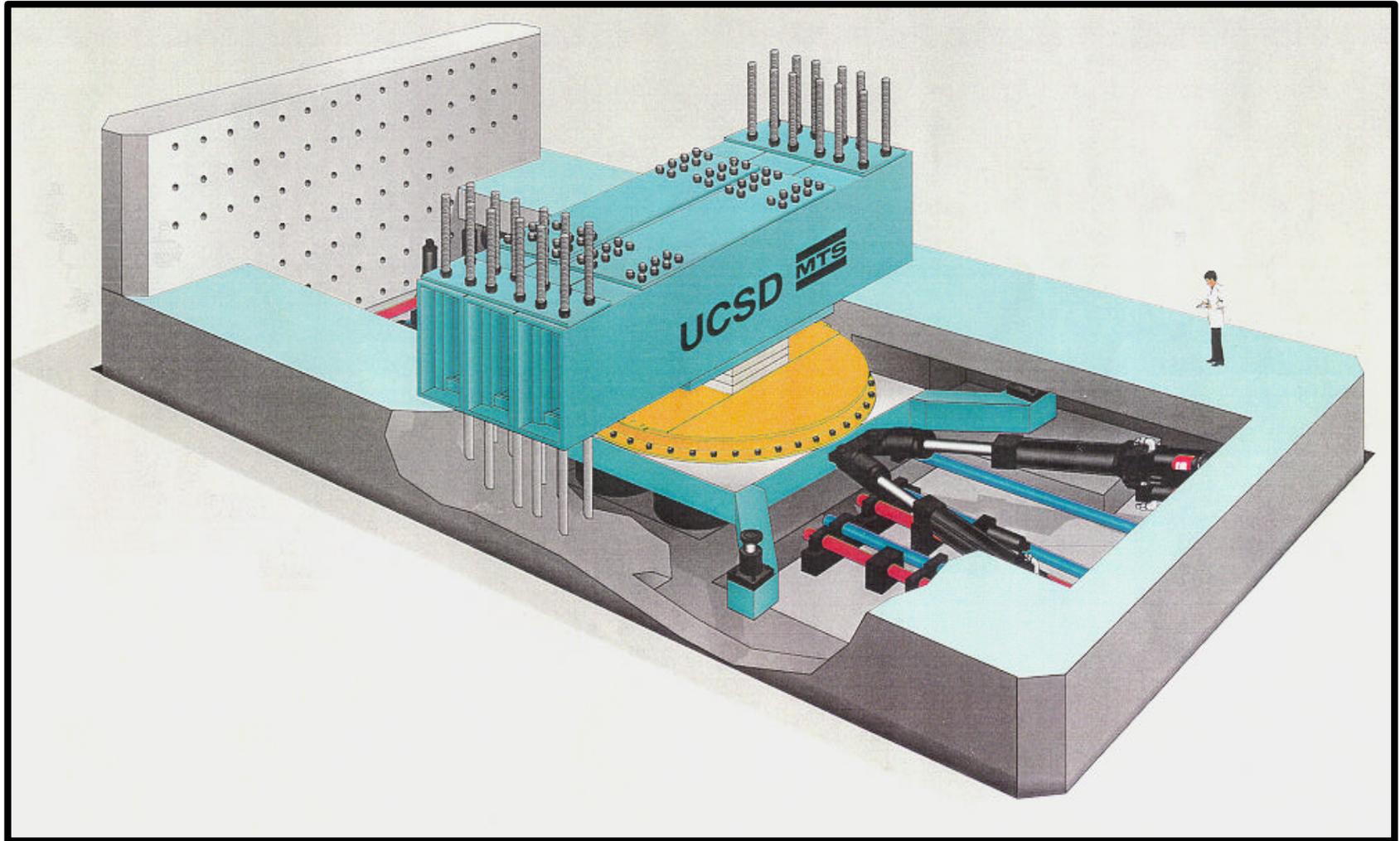








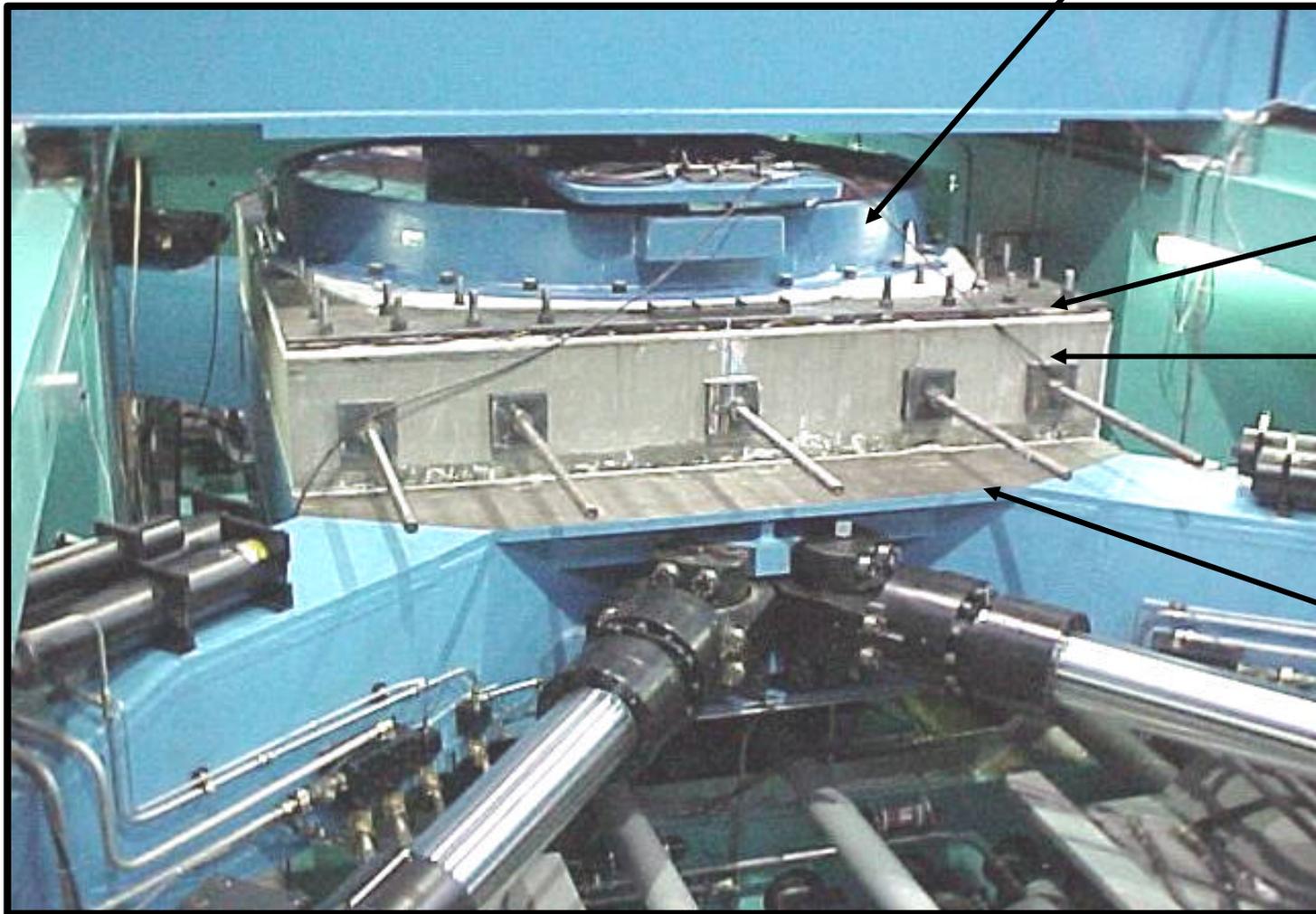
Schematic of SRMD Test System



SRMD Technical Specifications

	<i>Vertical</i>	<i>Longitudinal</i>	<i>Transverse</i>
Force	53,400 kN (12,000 kips)	8,900 kN (2,000 kips)	4,450 kN (1,000 kips)
Displacement	± 0.127 m (5 in.)	± 1.22 m (48 in.)	± 0.61 m (24 in.)
Velocity	± 254 mm/s (10 in./s)	± 1778 mm/s (70 in./sec)	± 762 mm/s (30 in./sec)
Clearance	Up to 1.52 m (5 ft)		~ 4 m (13 ft)
Relative rotation	± 2°	± 2°	± 2°

Bearing Specimen (Type 1)



Adapting Plate

Concrete
Spacer
Block

Platen



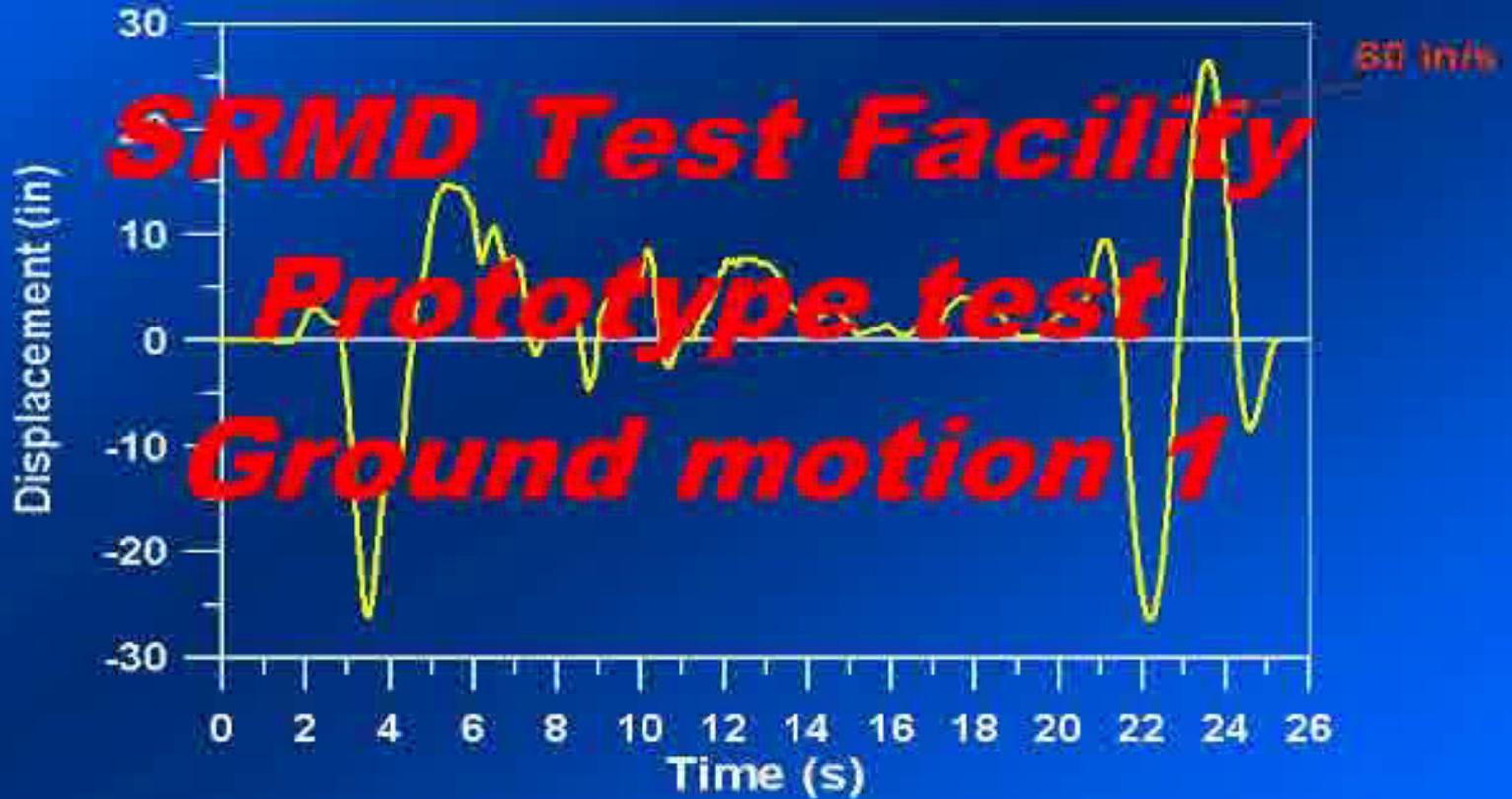
SRMD

Caltrans Seismic response Modification Device Test facility



FPS Device Type 3

Ground Motion 1



Isolation Bearing Test: Friction Pendulum Bearing



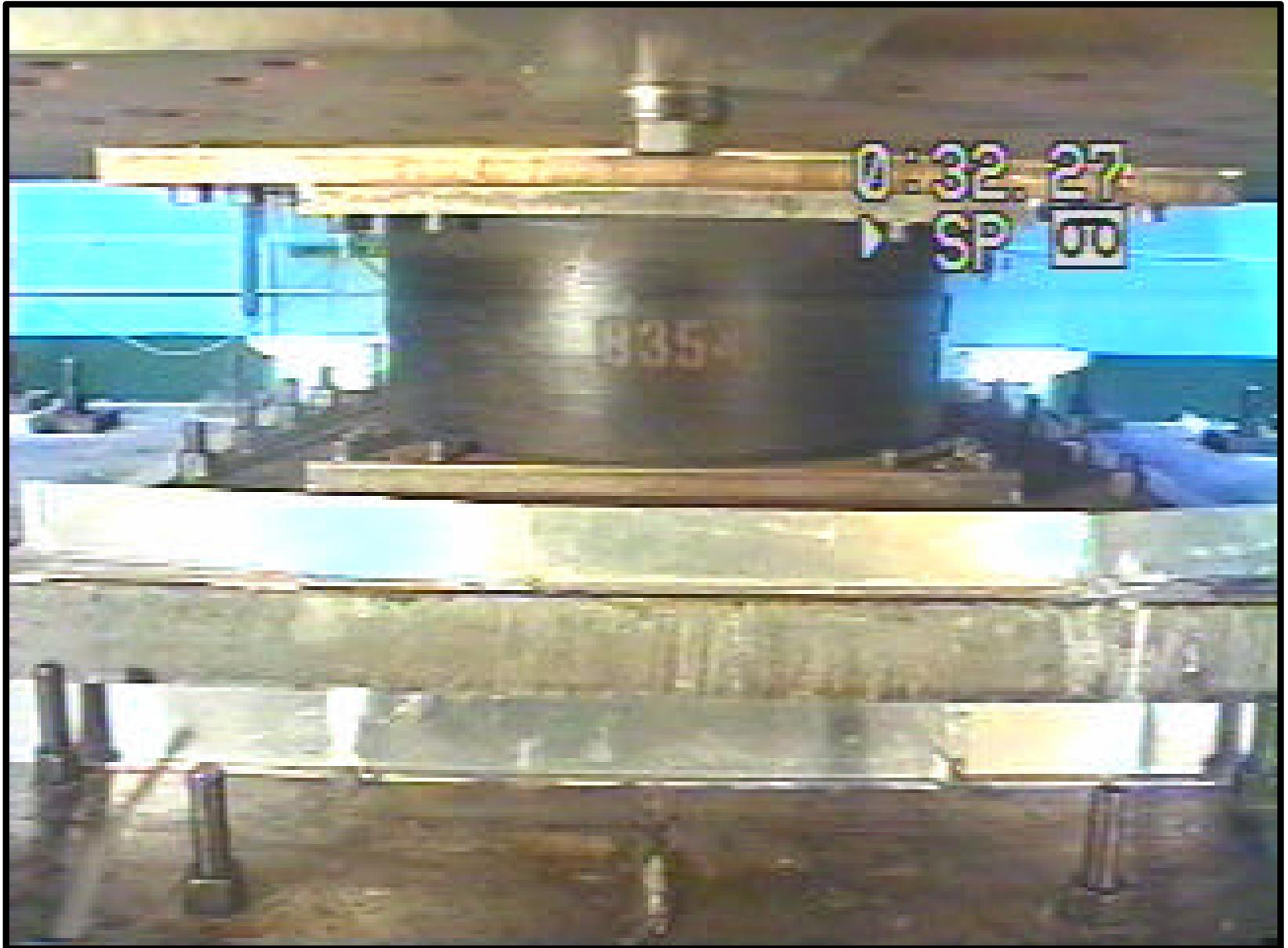
$P_z = 6000$ kips

$D_x = \pm 29$ inches

Vel = 60 in./sec.

CORONADO BRIDGE





The San Francisco – Oakland Bay Area



SFOBB – Existing Bridge



© 1999 Barrie Rokeach

October 17, 1989 – 5:04 PM

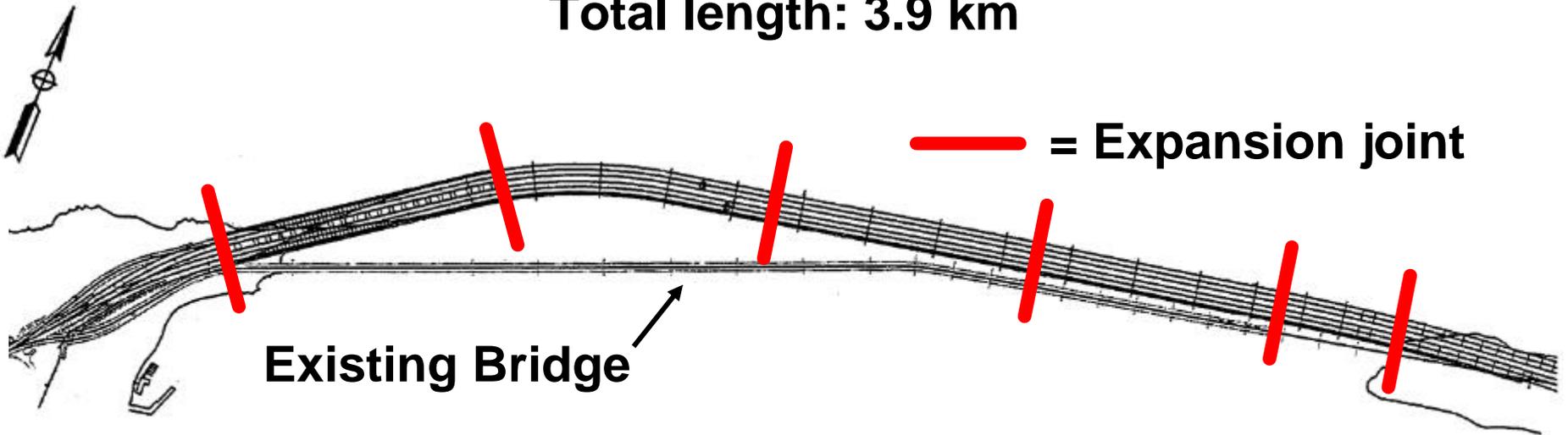
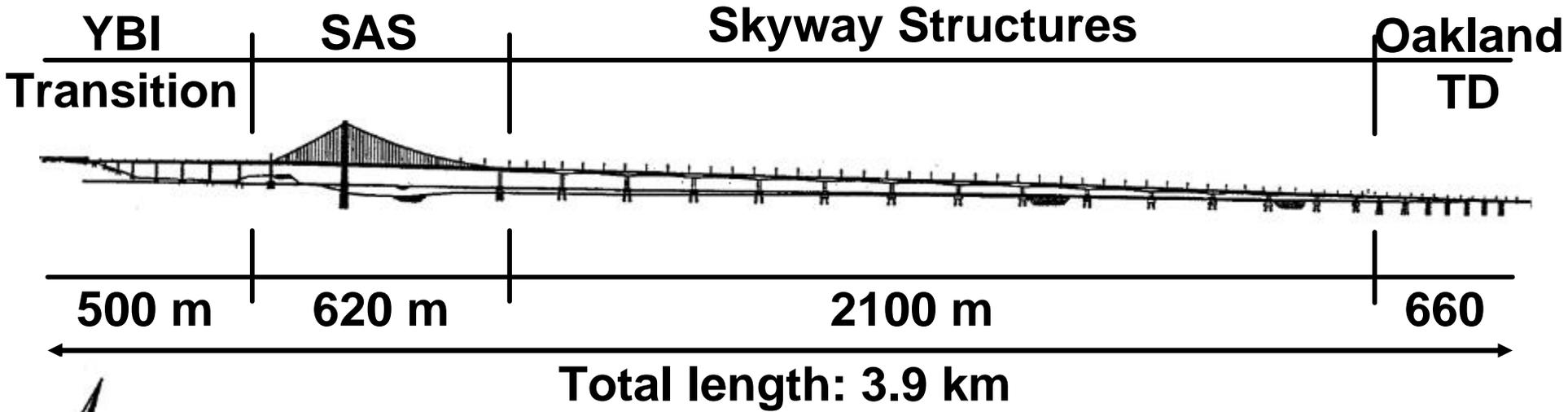
**Partial collapse of
deck roadway above
Pier E9 during the
Loma Prieta EQ**

**1 casualty
One month bridge closure
Million \$\$\$ in losses**

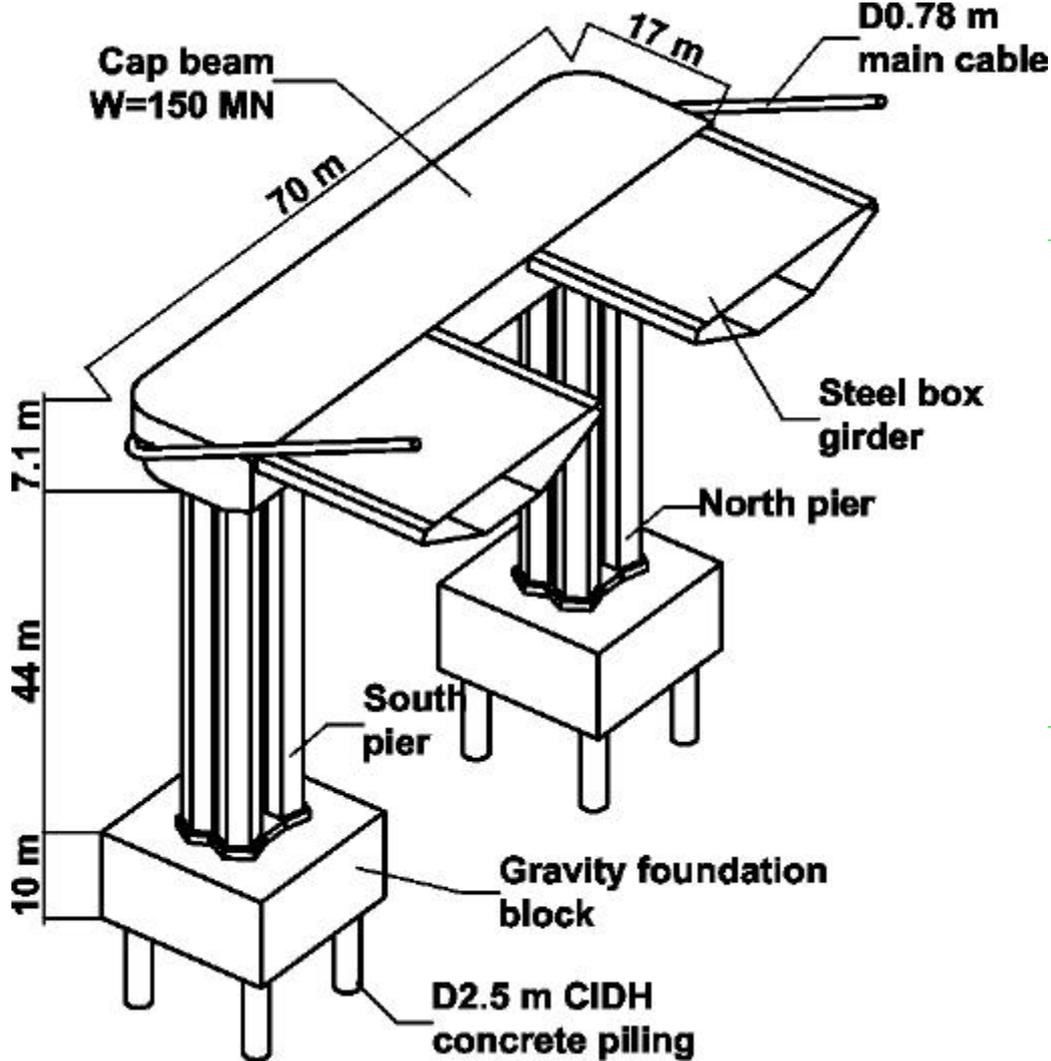
**Loma Prieta EQ
D = 100 km
M = 7.1**



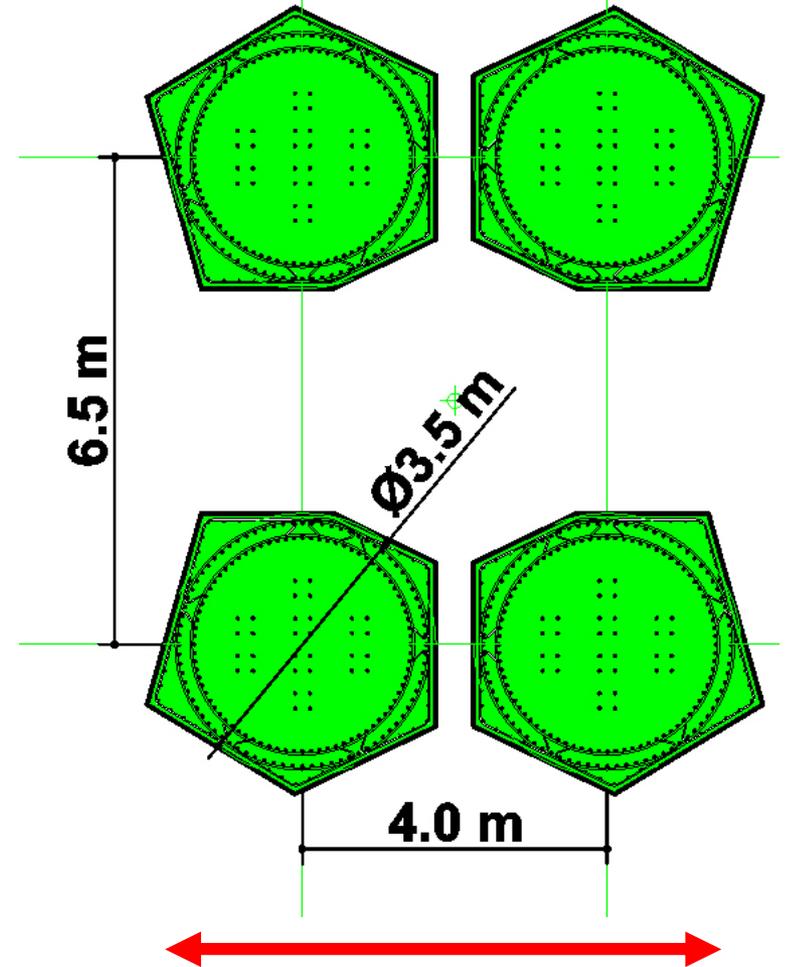
SFOBB East Span Segments



Pier W2

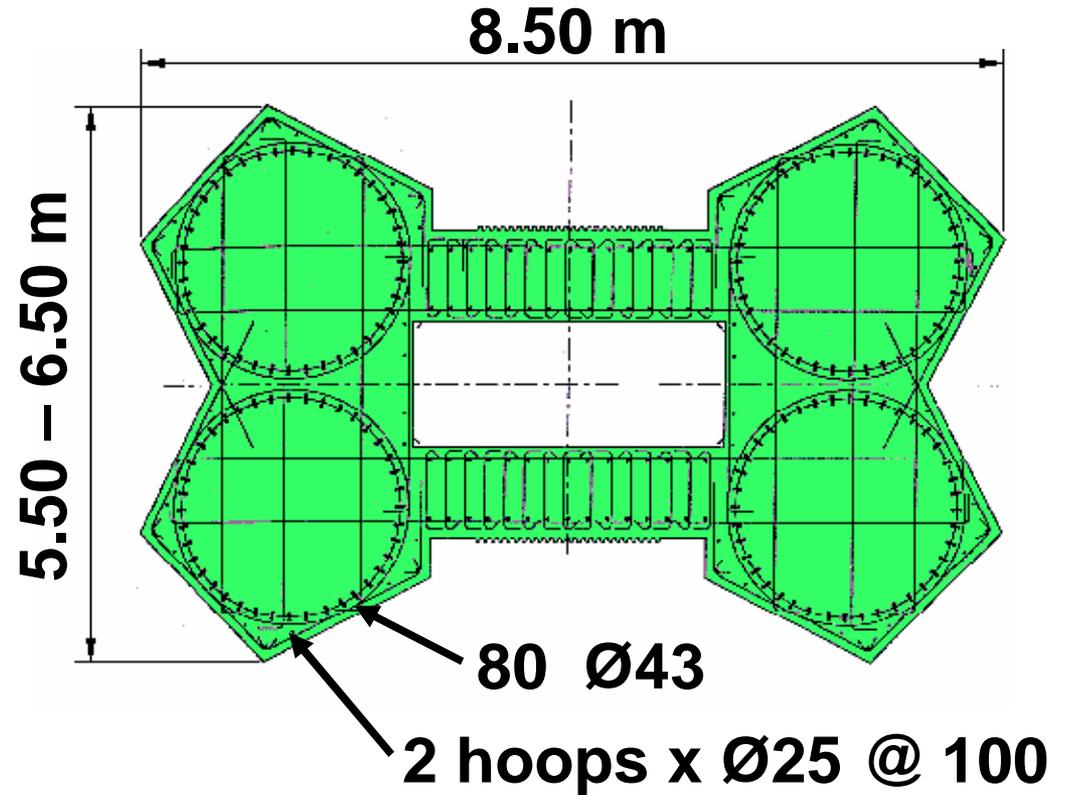
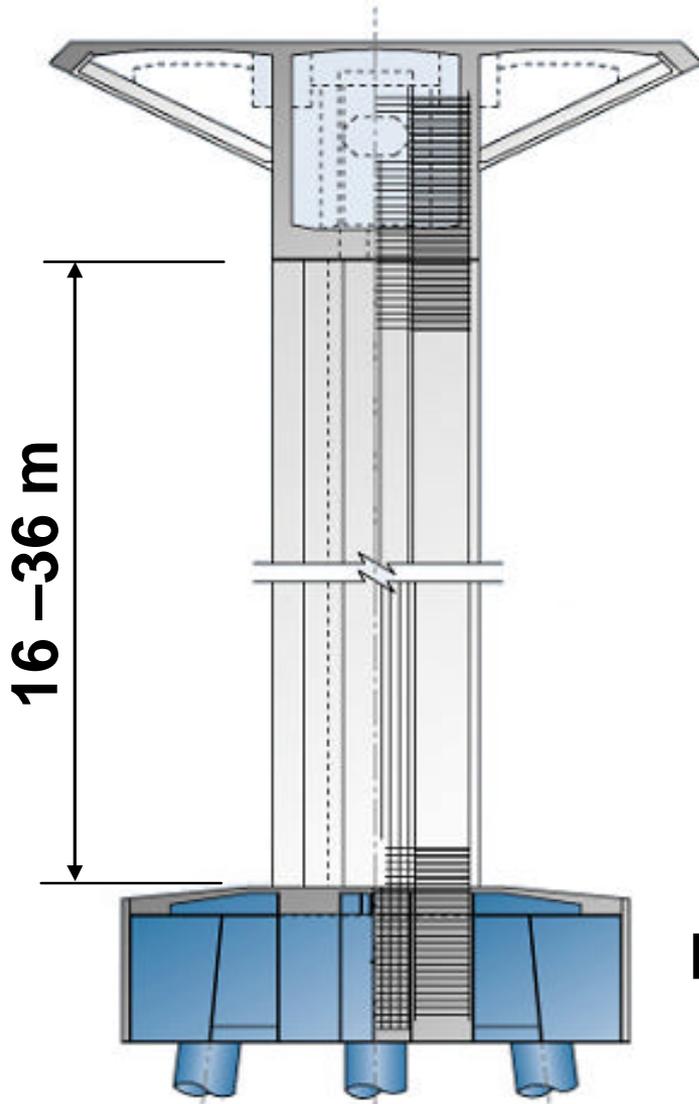


South Pier section



Longitudinal direction

Skyway Structures



Boundary Elements: $r_i=0.020$, $r_s=0.017$

Walls: $r_i=0.018$, $r_t=0.010$

Seismic Response Mechanism

Main span

Shear links

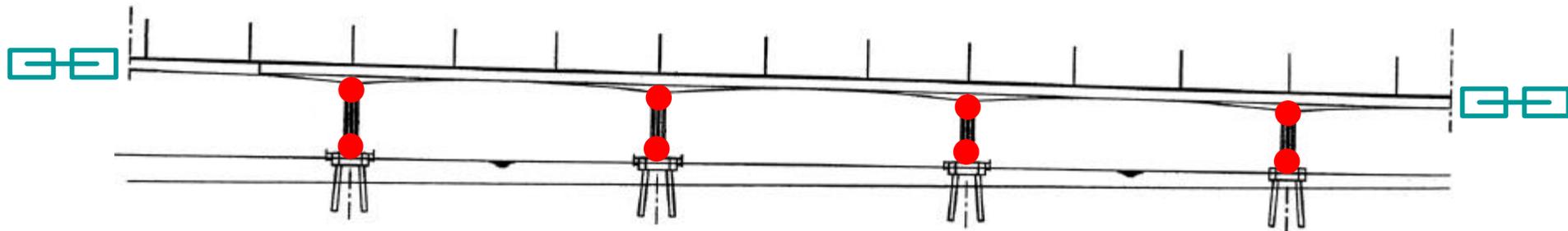
- Expected inelastic mechanism
- Possible inelastic mechanism
- Flexural hinge
- ▭ Axial-flexural hinge
- ▭ Axial hinge

Pier W2

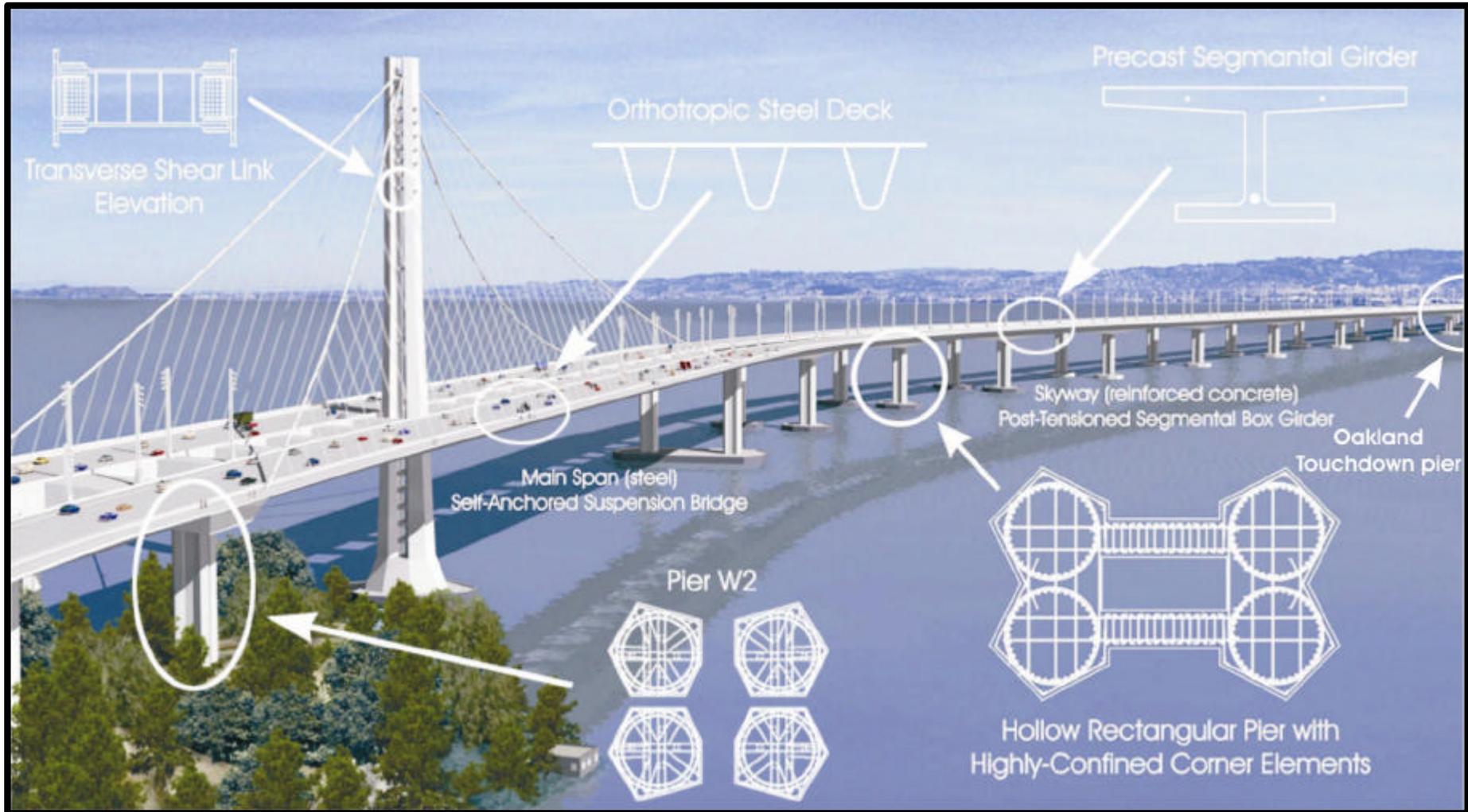
Tower

Pier E2

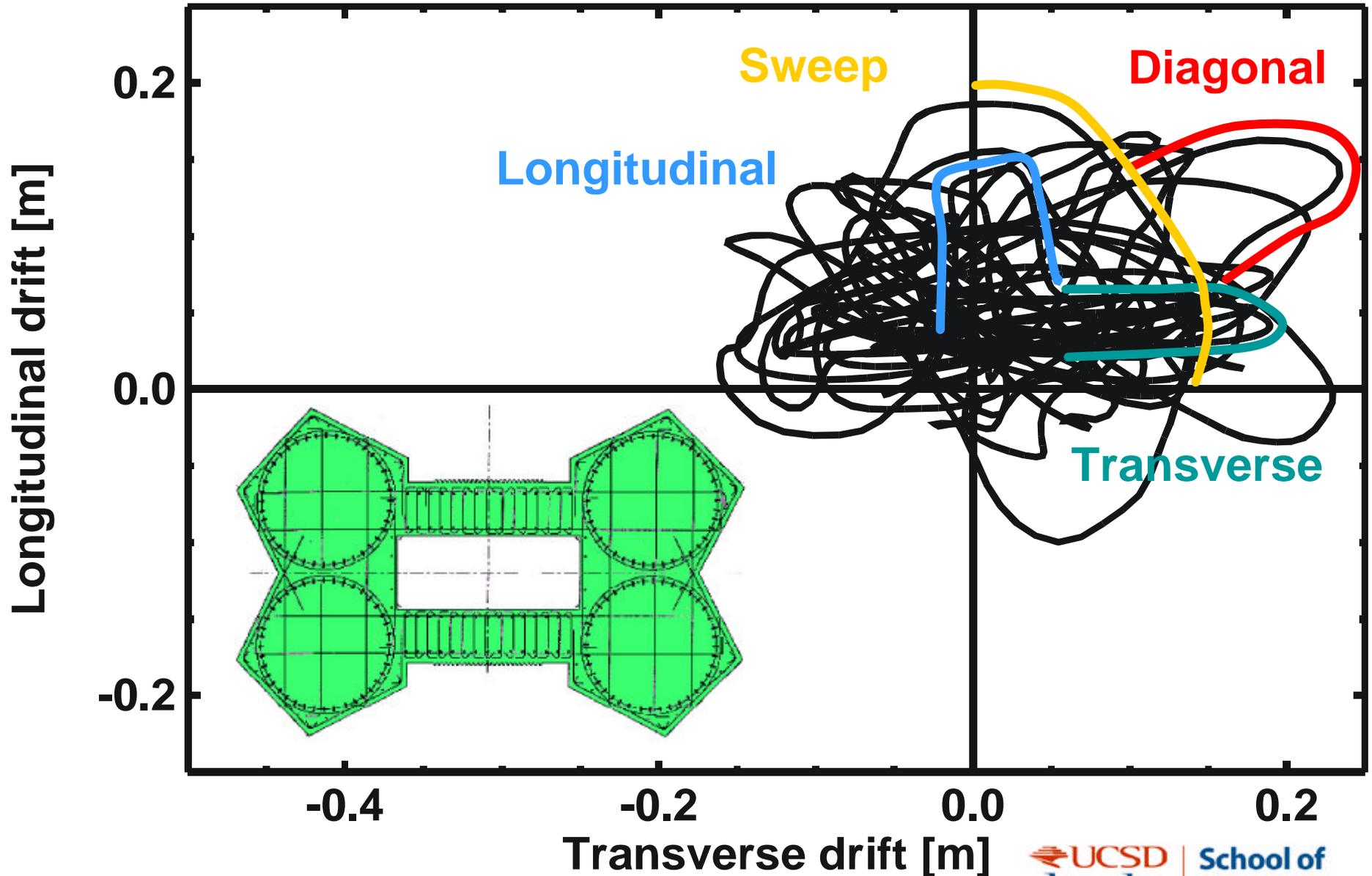
Skyway



Proof Test Program



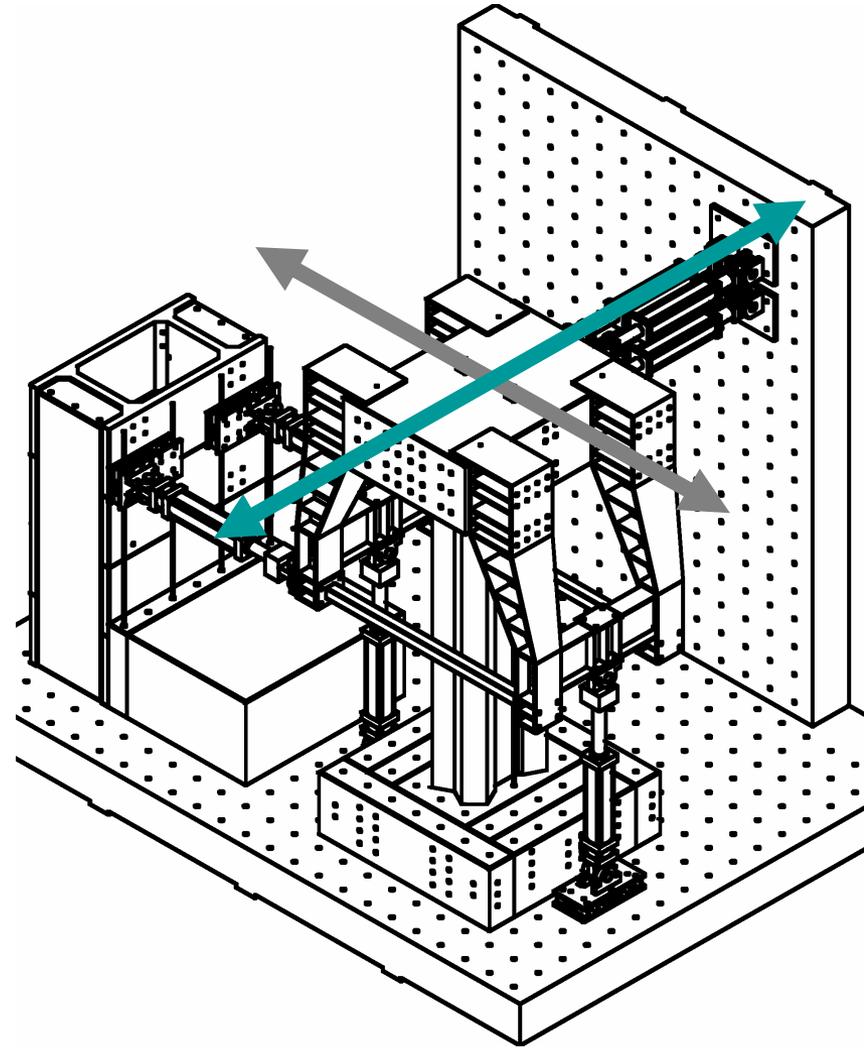
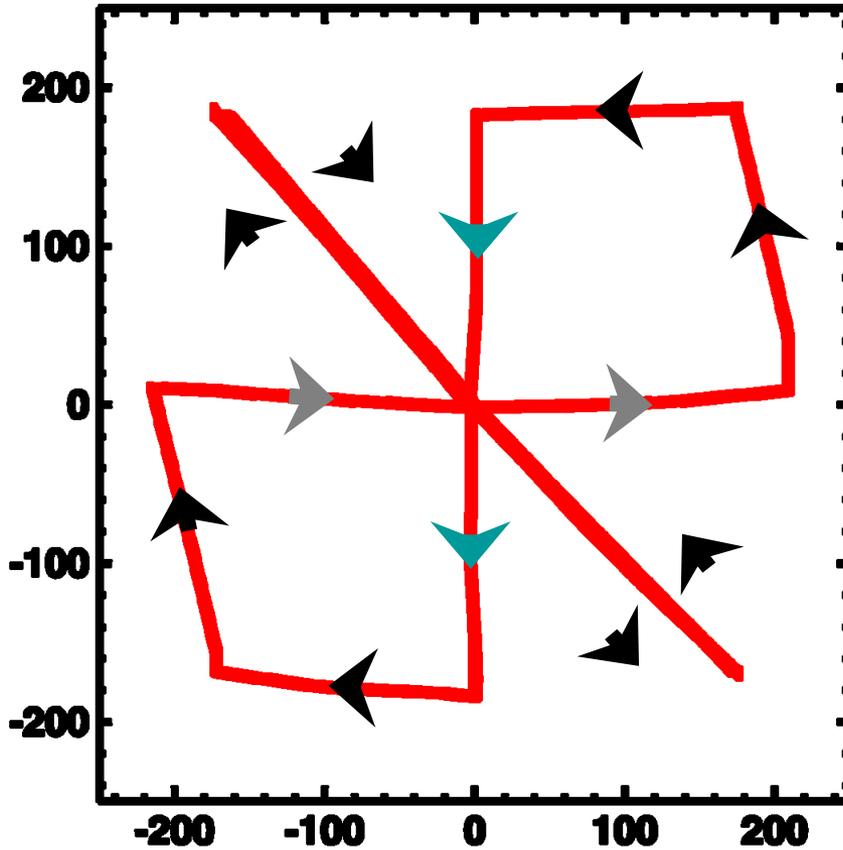
Seismic Drift of Skyway Pier E9



Skyway Pier Test Set UP

Loading History

Transverse Displacement (mm)



Longitudinal Displacement (mm)

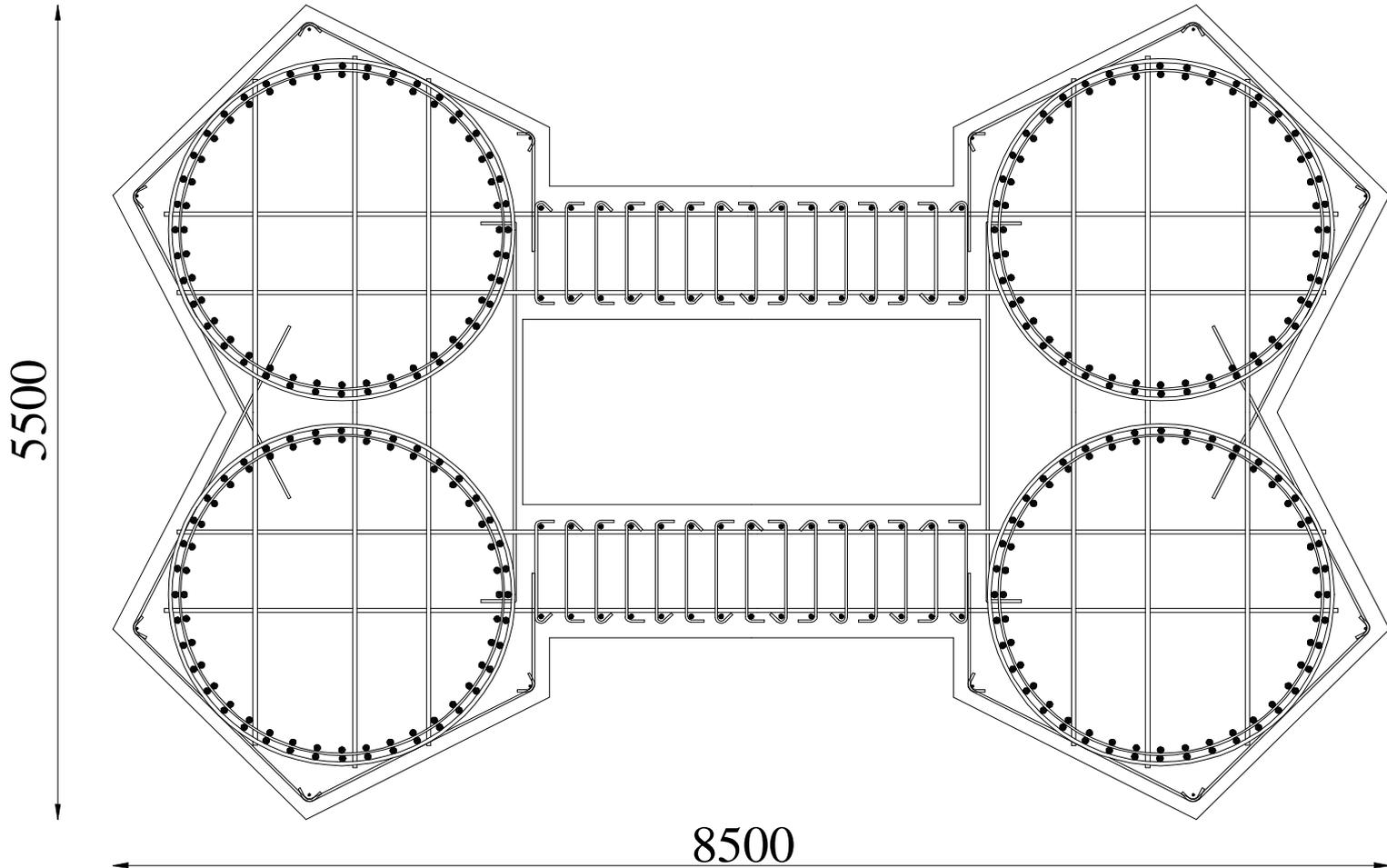
SFOBB Longitudinal Pier Test Setup

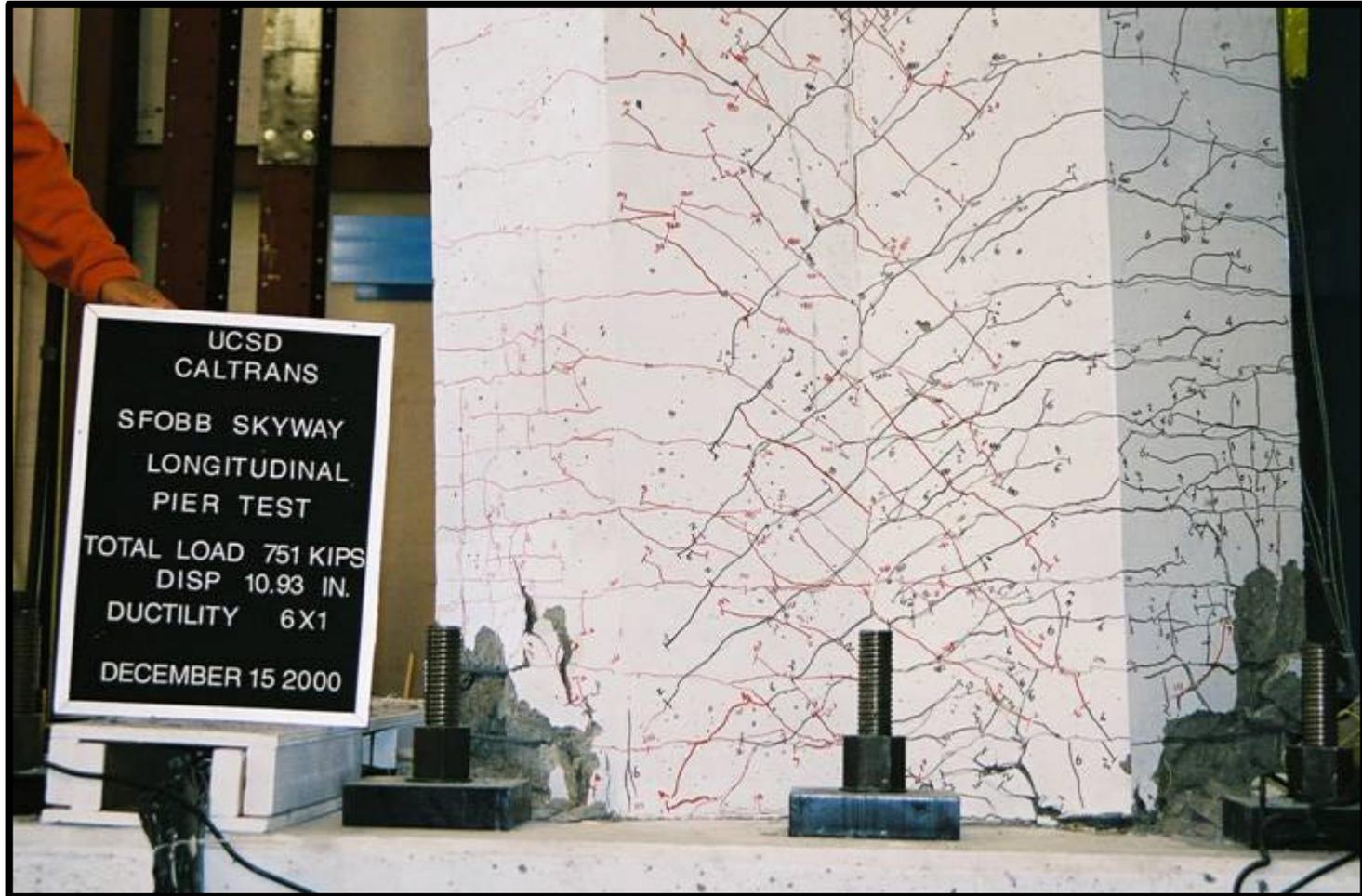


Skyway Pier Test: Front view of the test setup



Prototype section for Longitudinal Pier Test





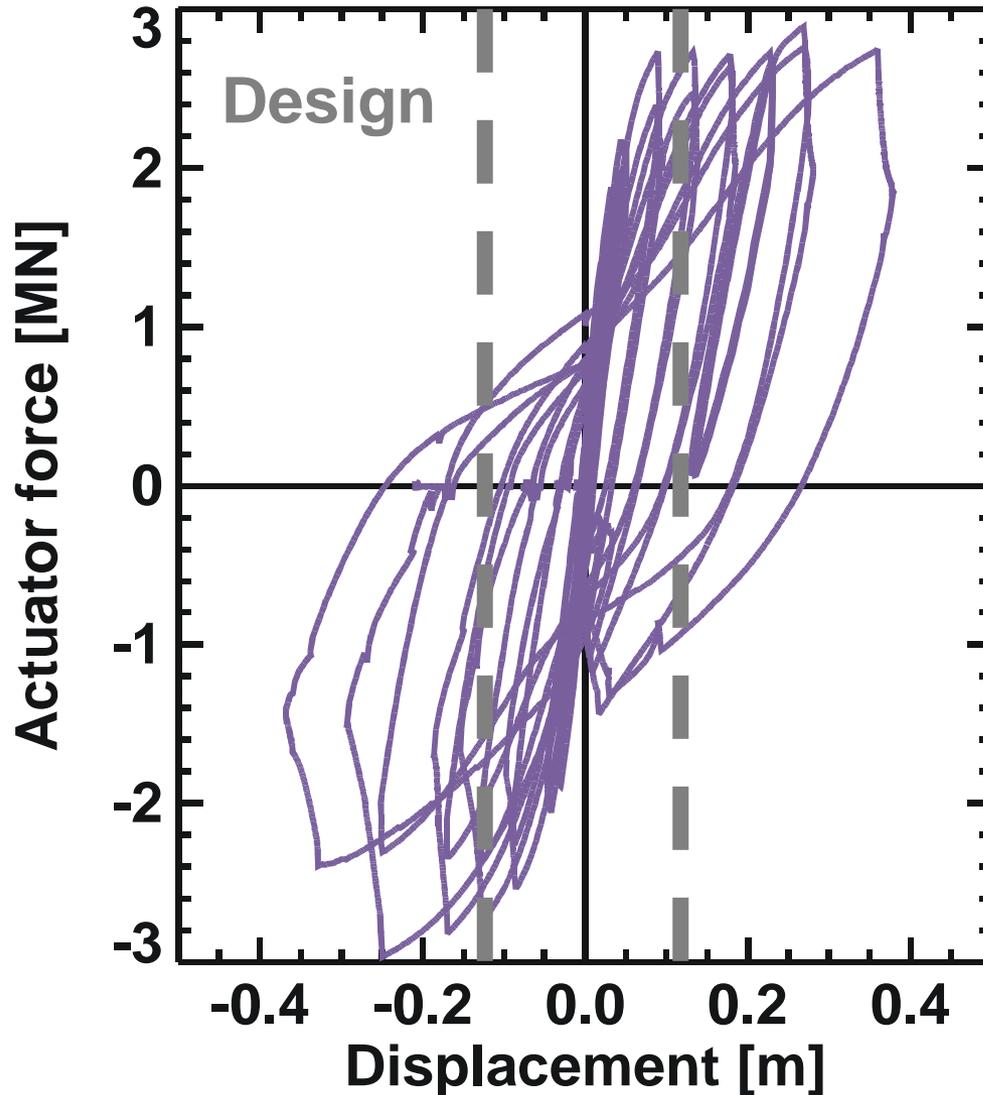
$$\mu_{\Delta} = 6 \times 1$$



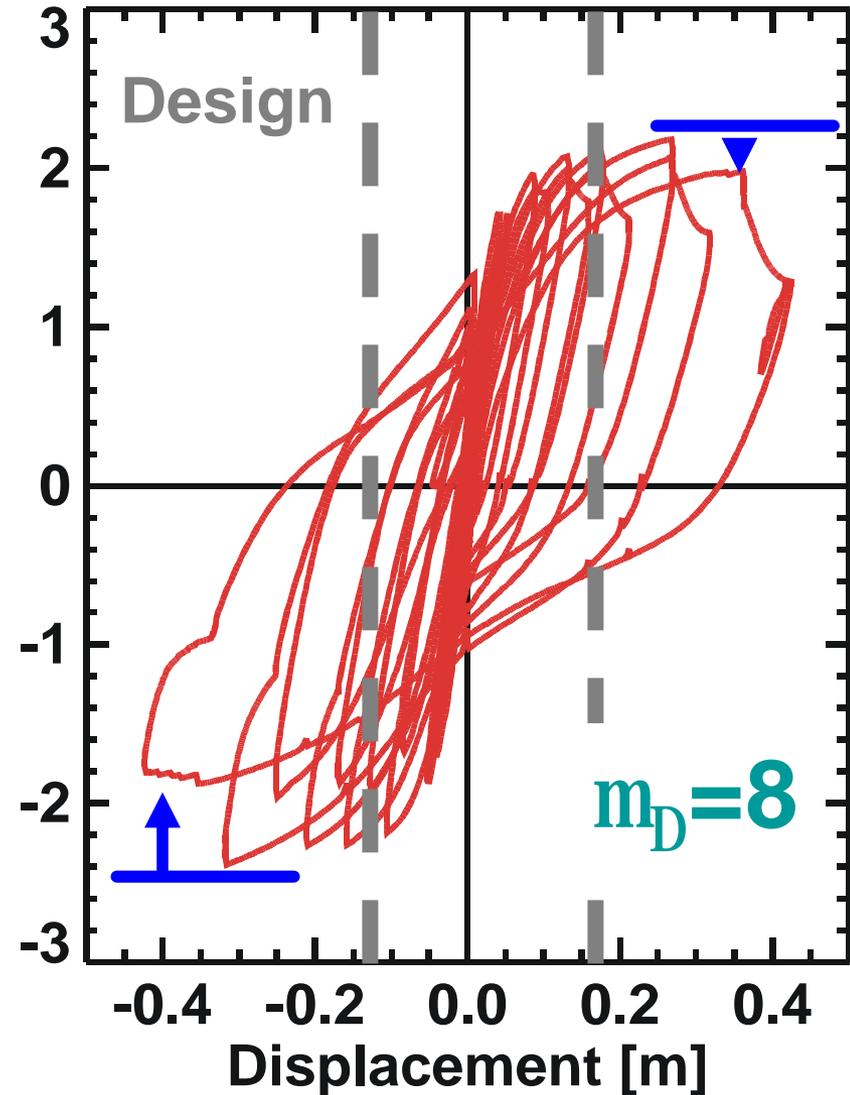
$$\mu_{\Delta} = 2 \times 1$$

Skyway Pier Test: Hysteretic behavior

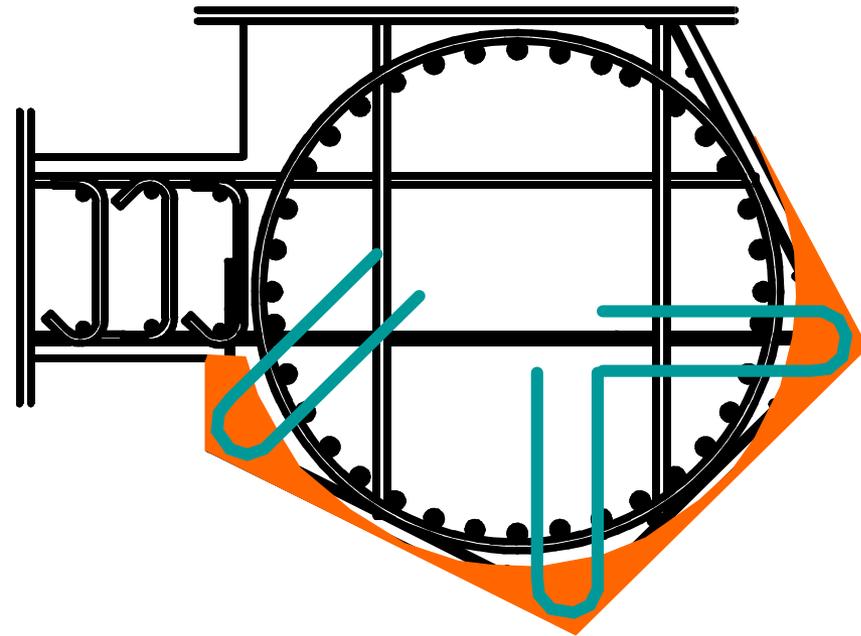
Transverse direction



Longitudinal direction



FEE Performance



$$m_D = 2$$

Spalling of the architectural concrete



Column Damage

**Longitudinal Pier
Test**

No isolation gaps



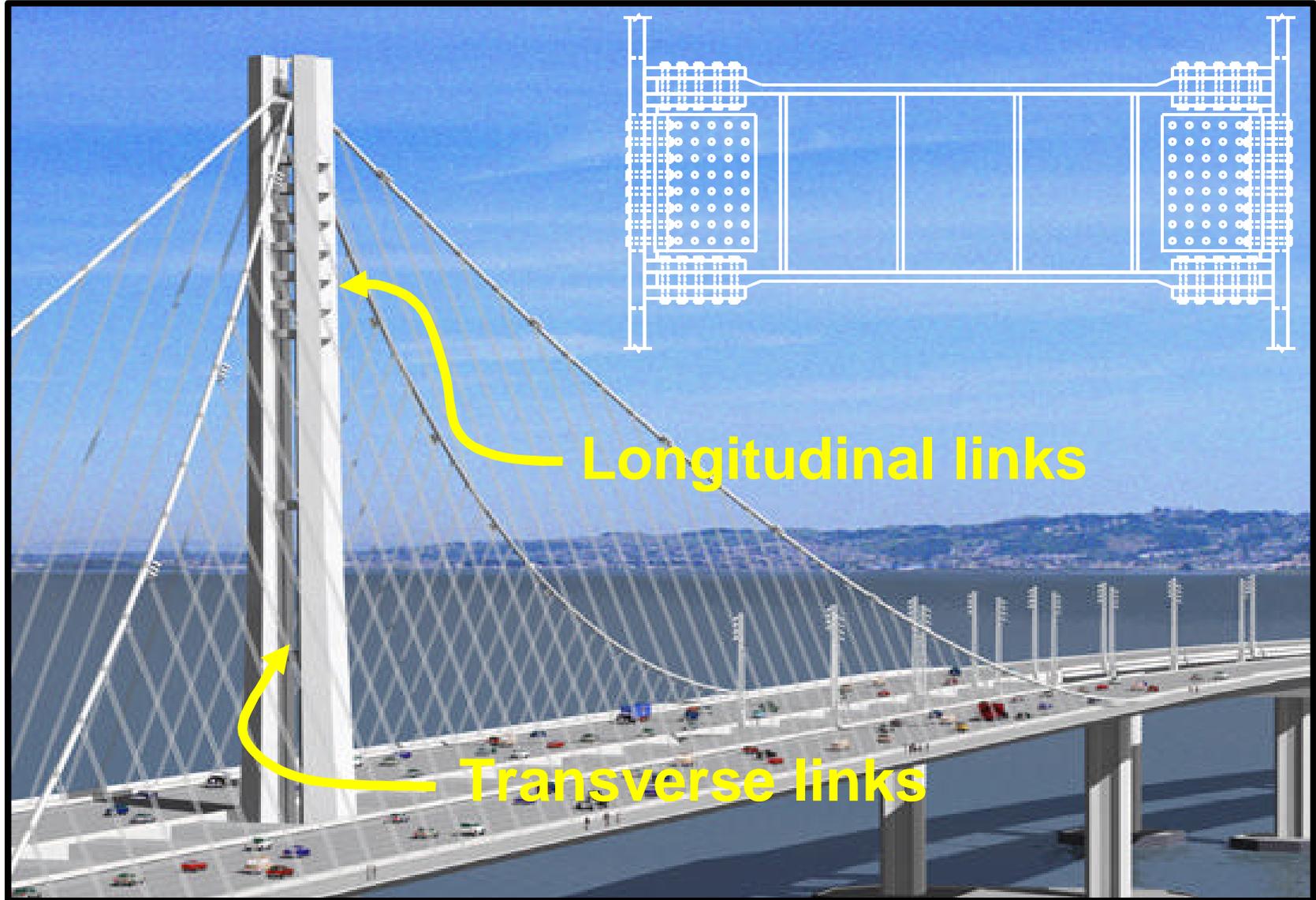
**Diagonal Pier
Test**

With isolation gaps

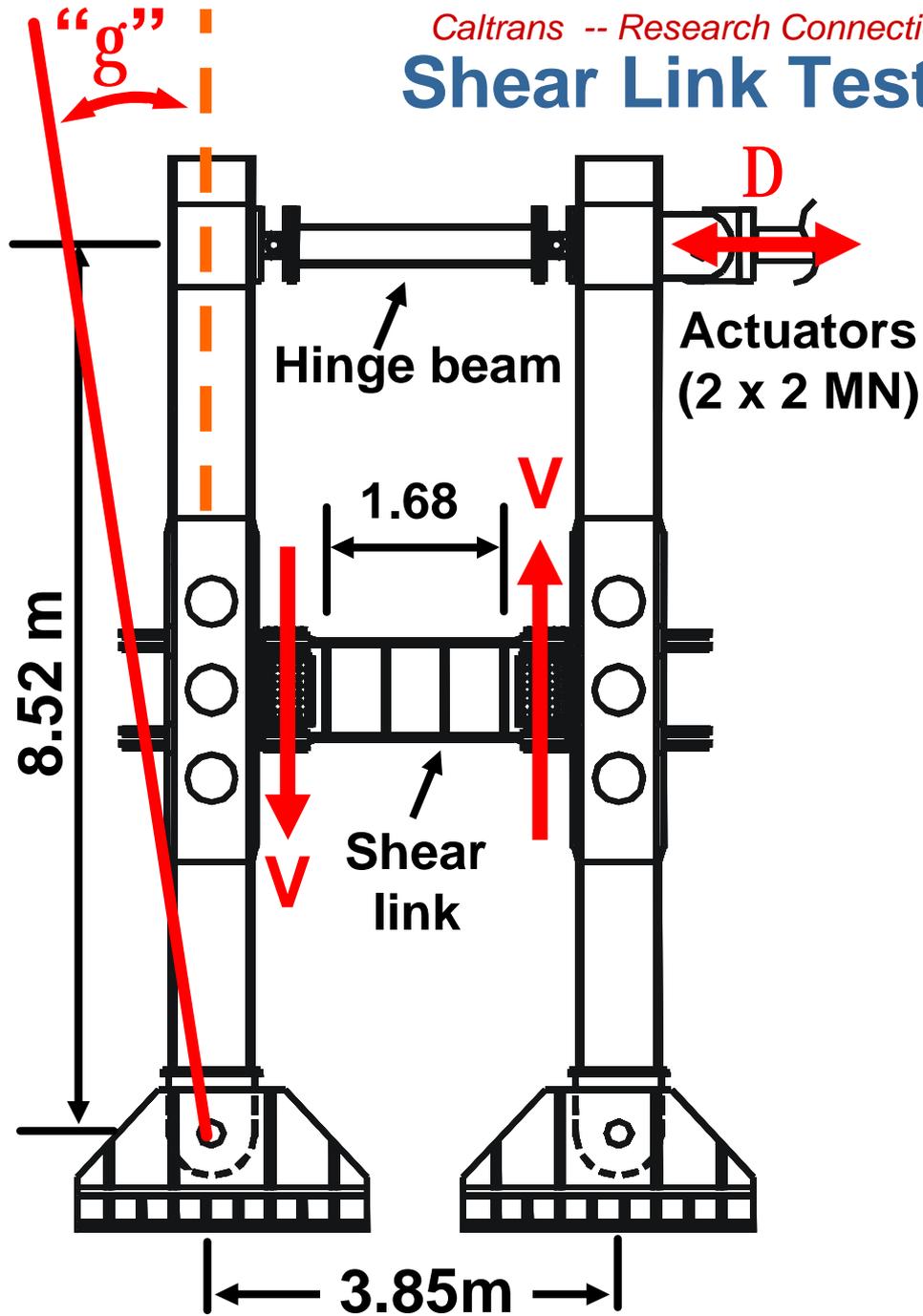




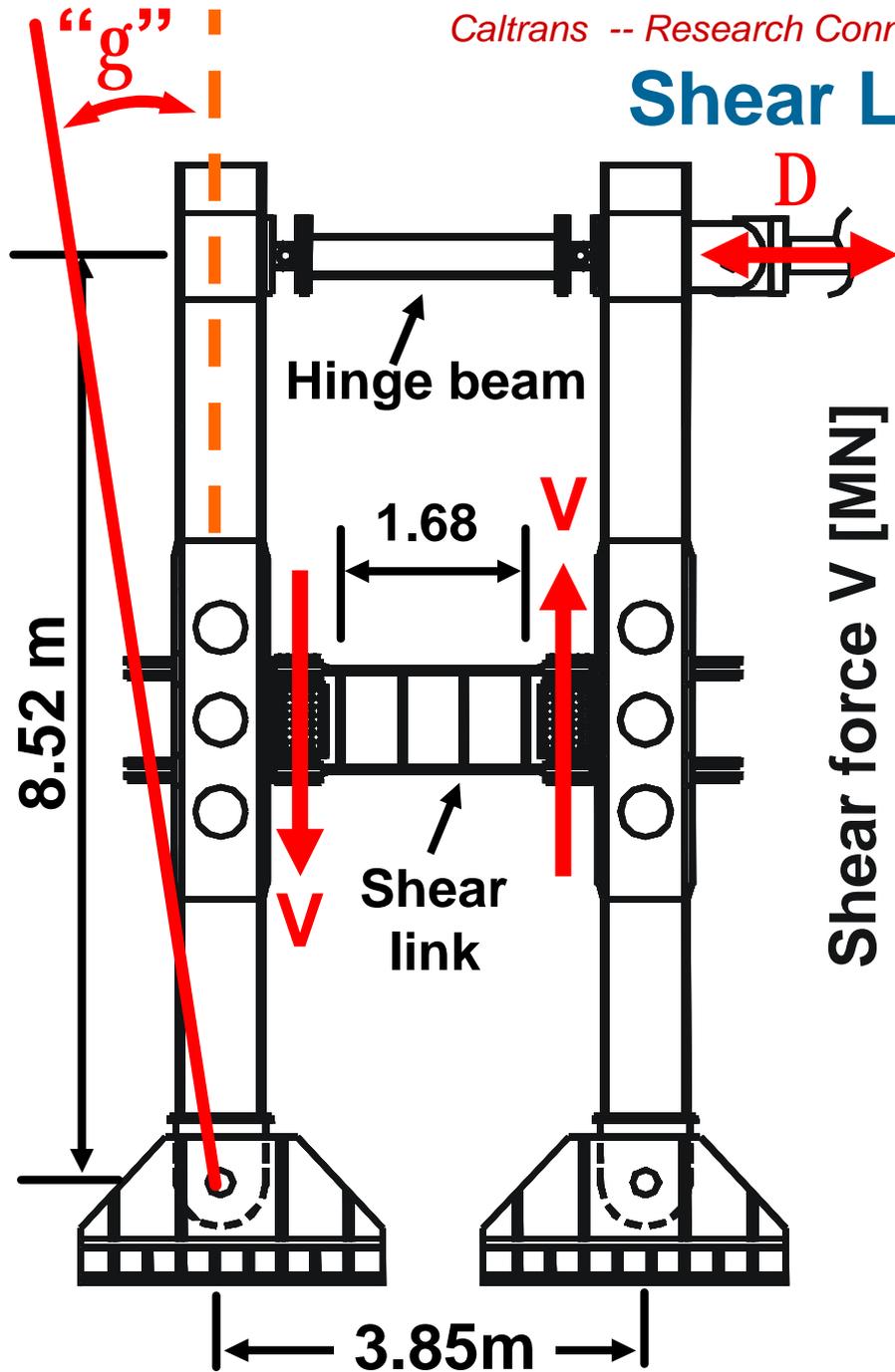
Shear Link Tests



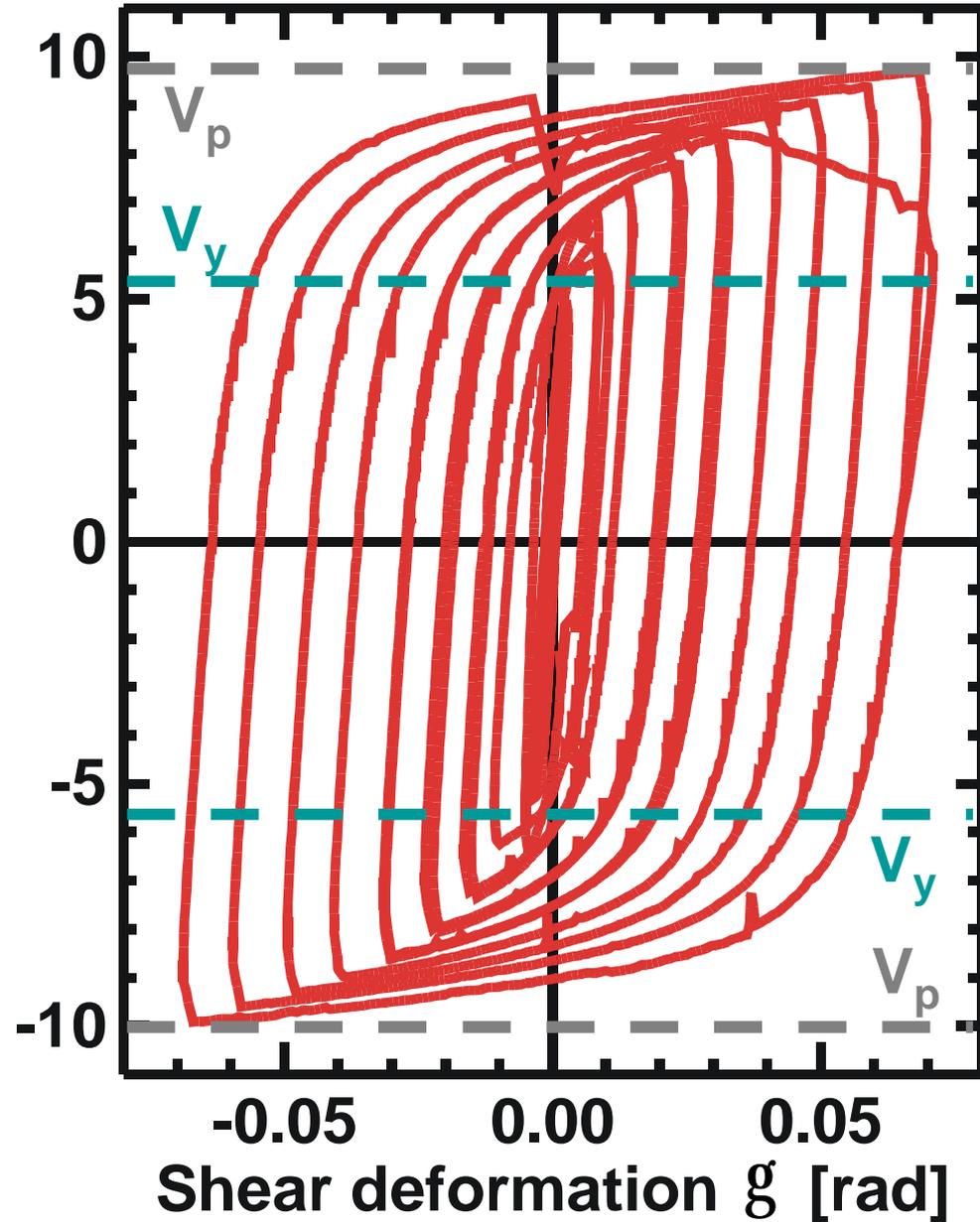
Shear Link Tests: Test setup



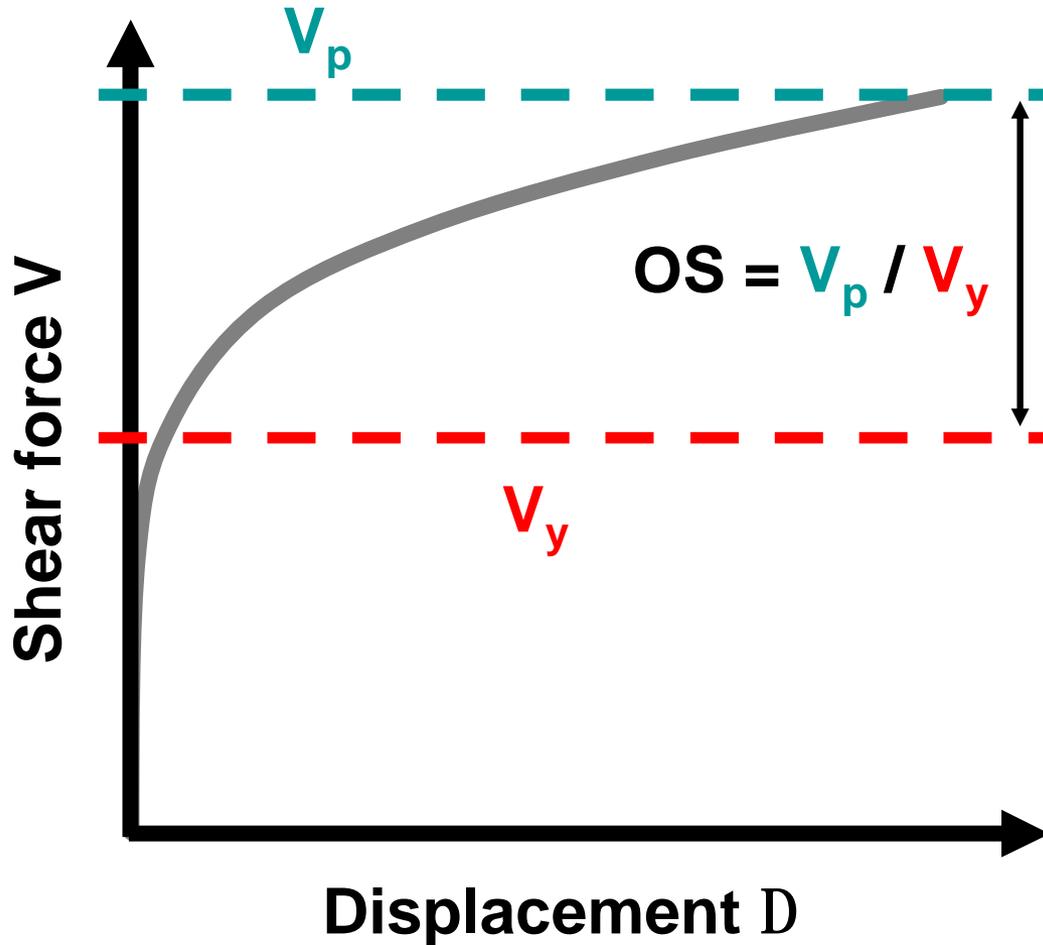
Shear Link Tests



Shear force V [MN]



Shear Link Overstrength

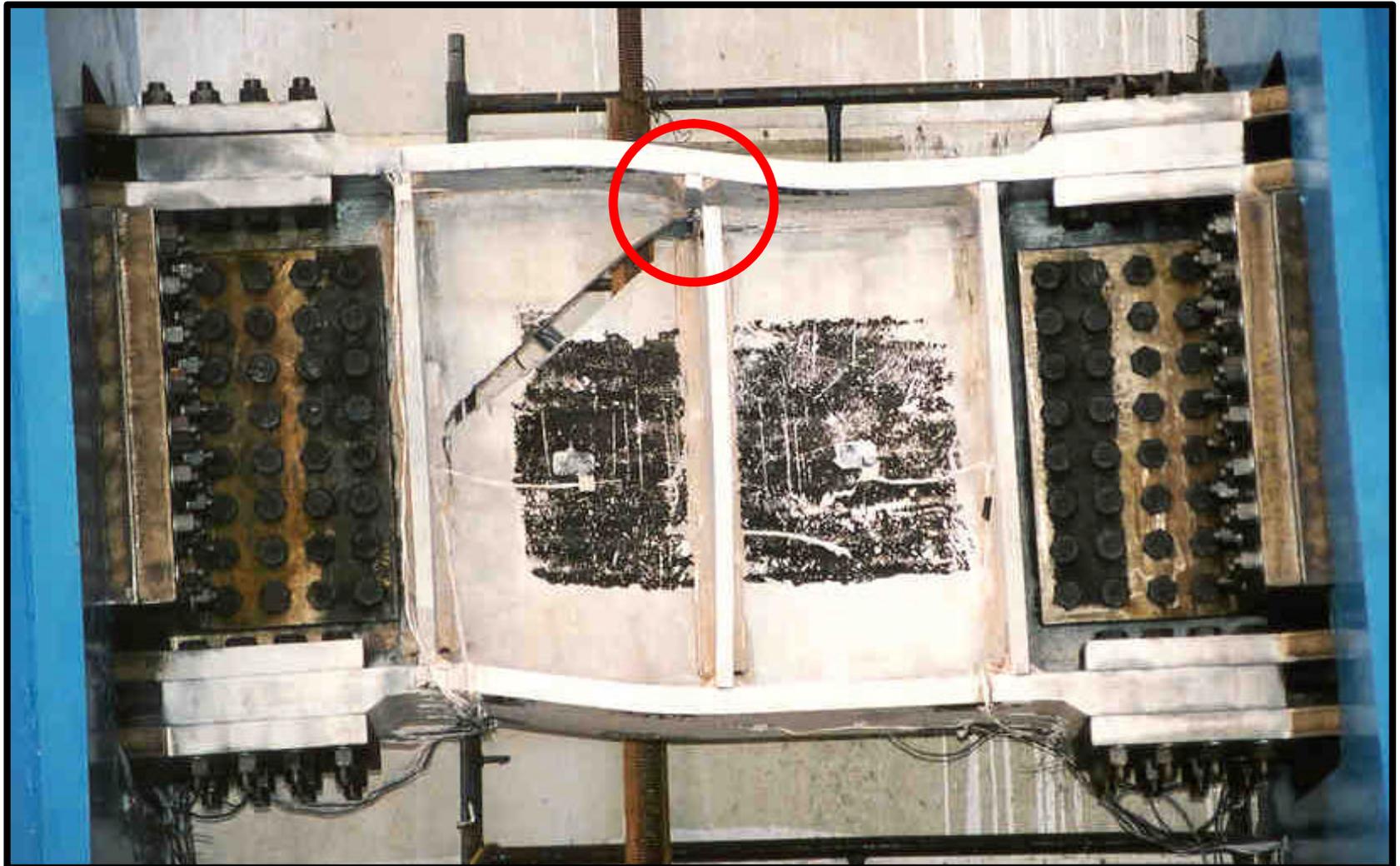


Overstrength

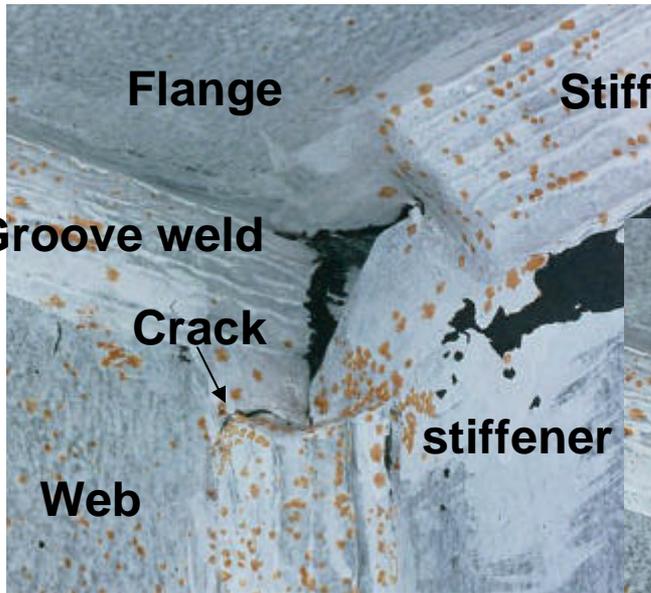
Transverse Link	1.83
Longitudinal Link	1.94
AISC Code	1.25

Code significantly underestimates the overstrength

Shear Link Tests: Failure



Shear Link Test: Failure development



Stiffener / web
fillet weld

$g = 0.04$ rad

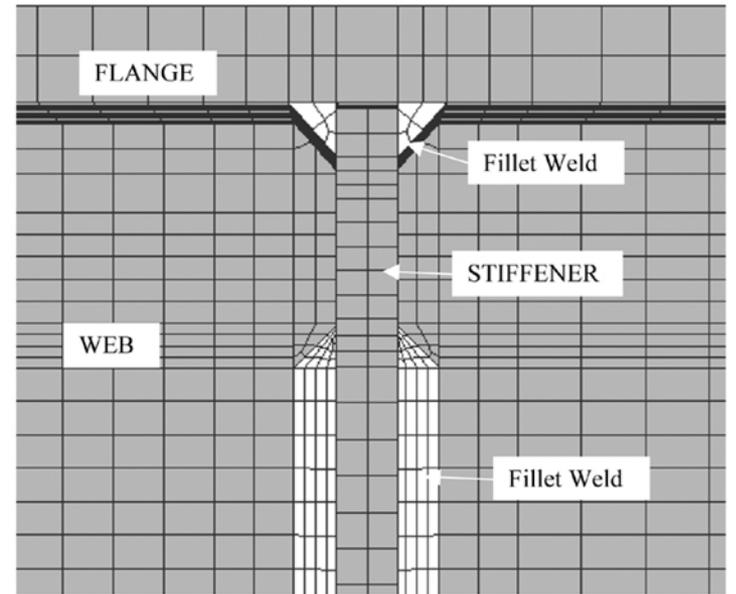
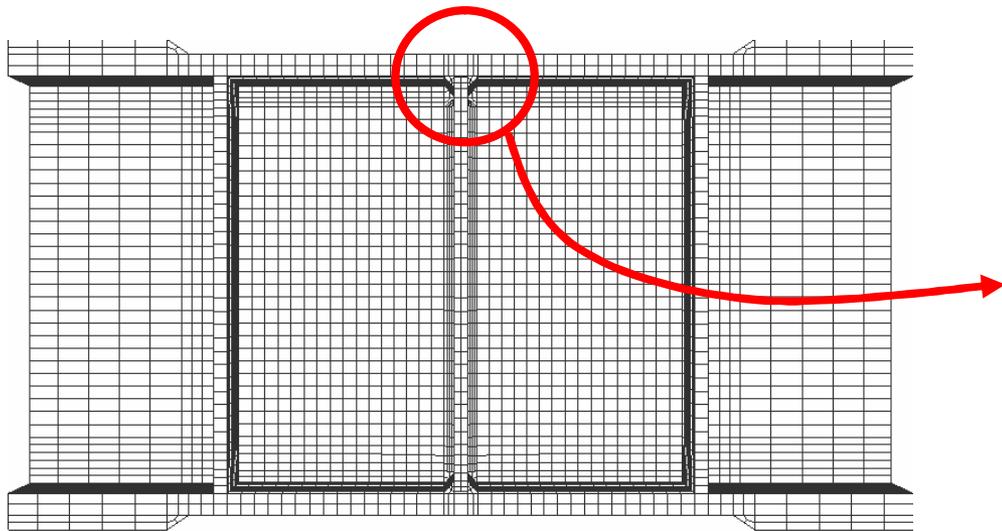


$g = 0.05$ rad

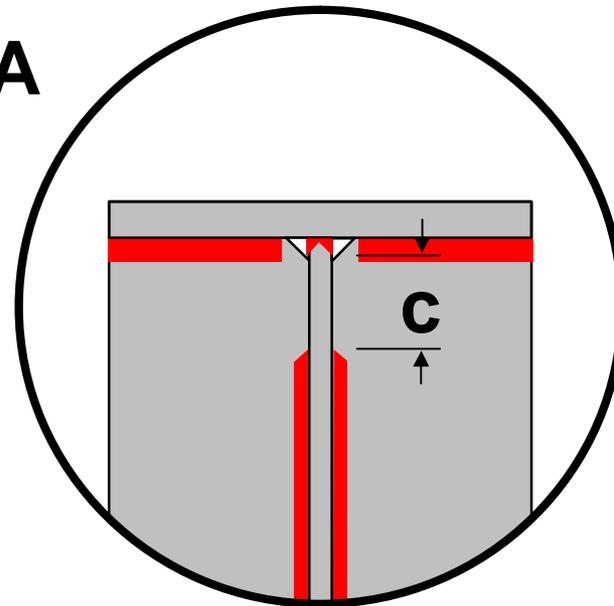
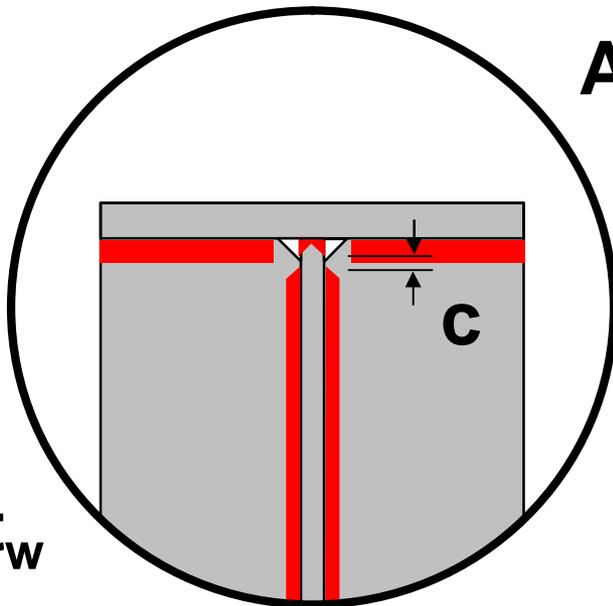
On the way to
 $g = 0.069$ rad



Finite Element Model



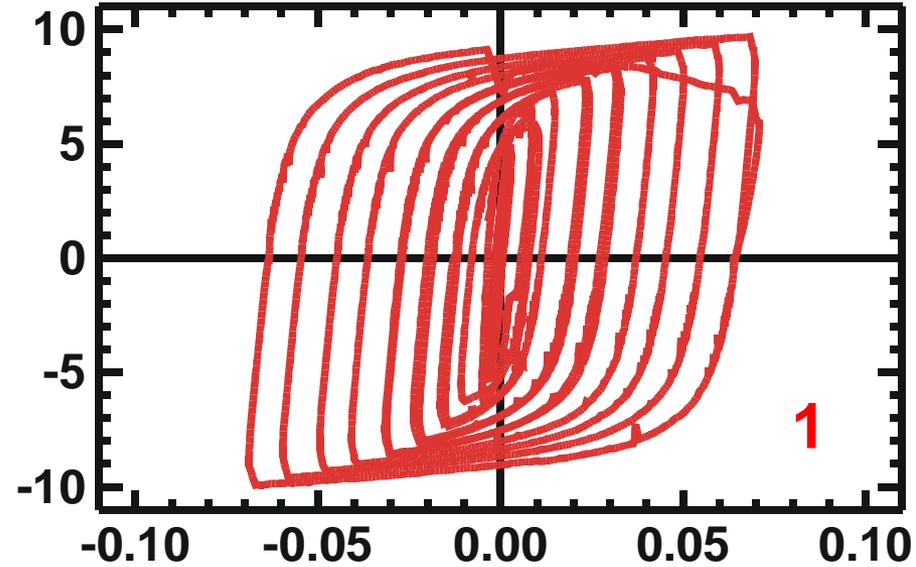
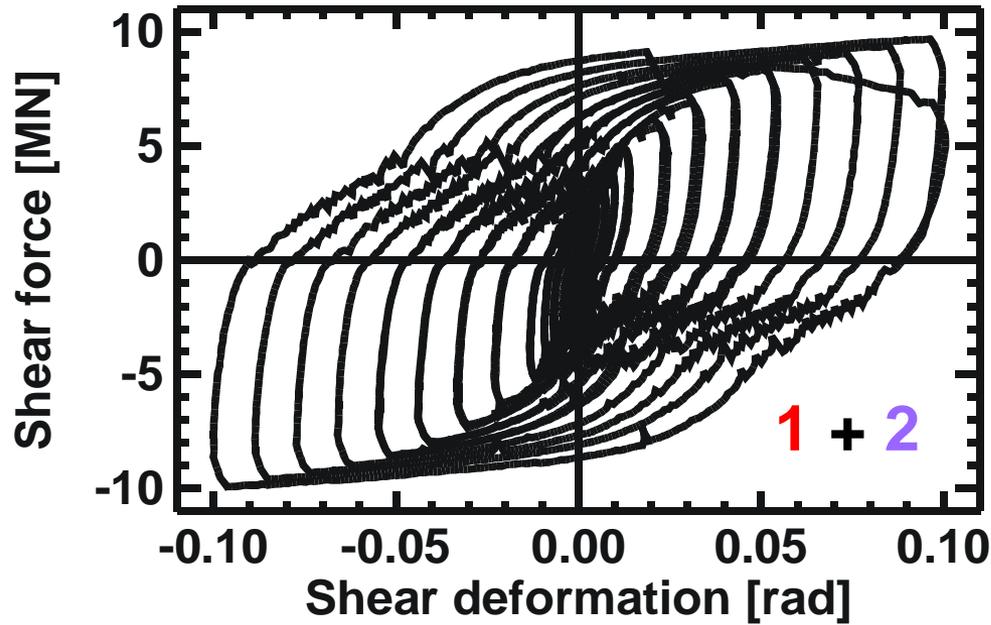
A-A



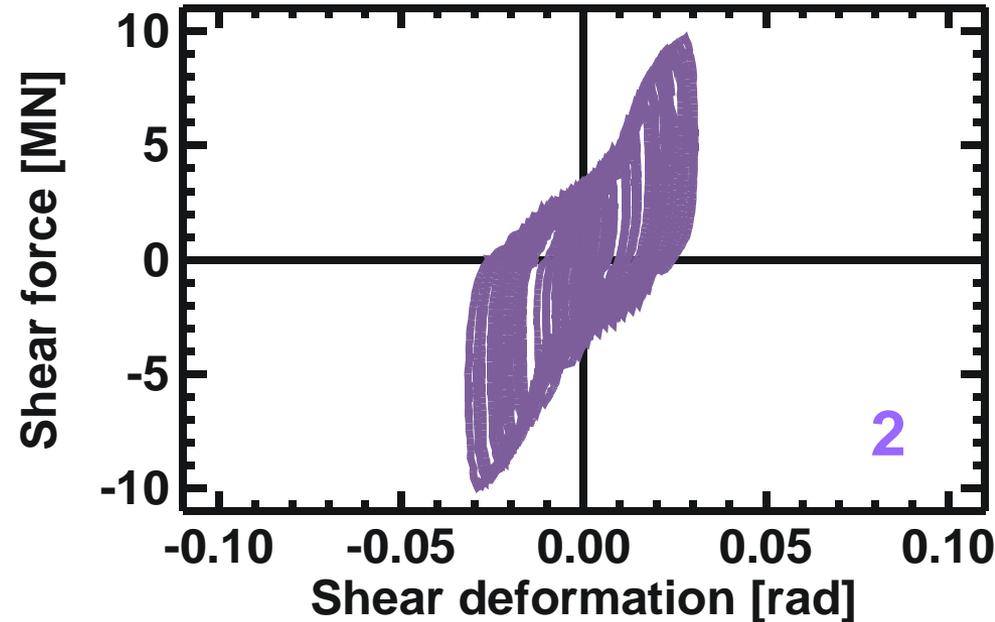
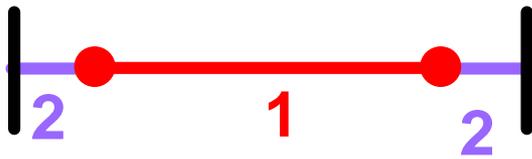
$$c = 1/2 t_w$$

$$c = 5 t_w$$

Global Bridge Analysis



Shear link model



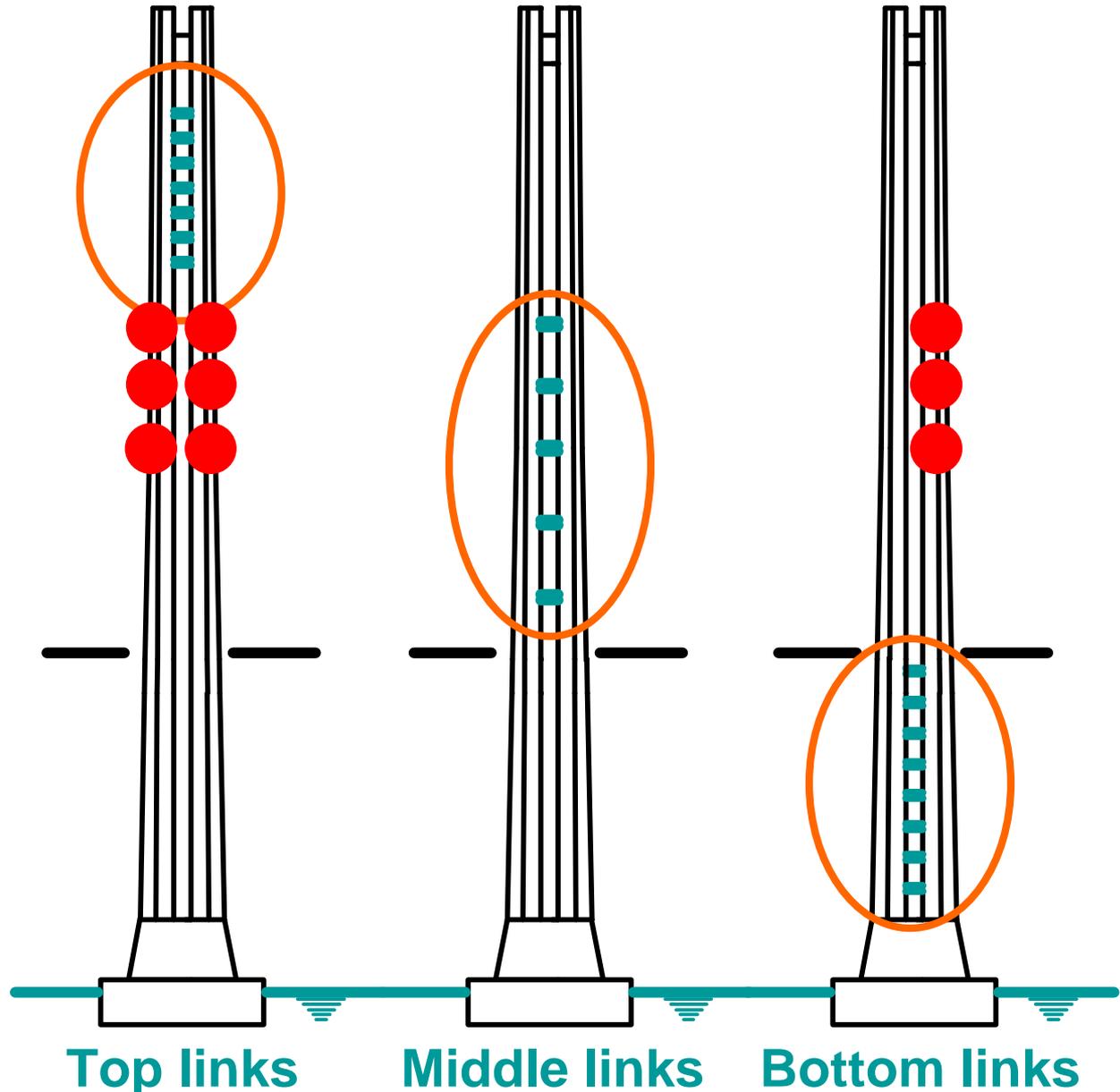
Time History Analyses: Parameter Study

- **Influence of tower link stiffness**
 - vary size of the tower links
- **Influence of tower link location**
 - vary link location along tower height
- **Influence of tower link inelastic behavior**
 - vary link hysteretic characteristics

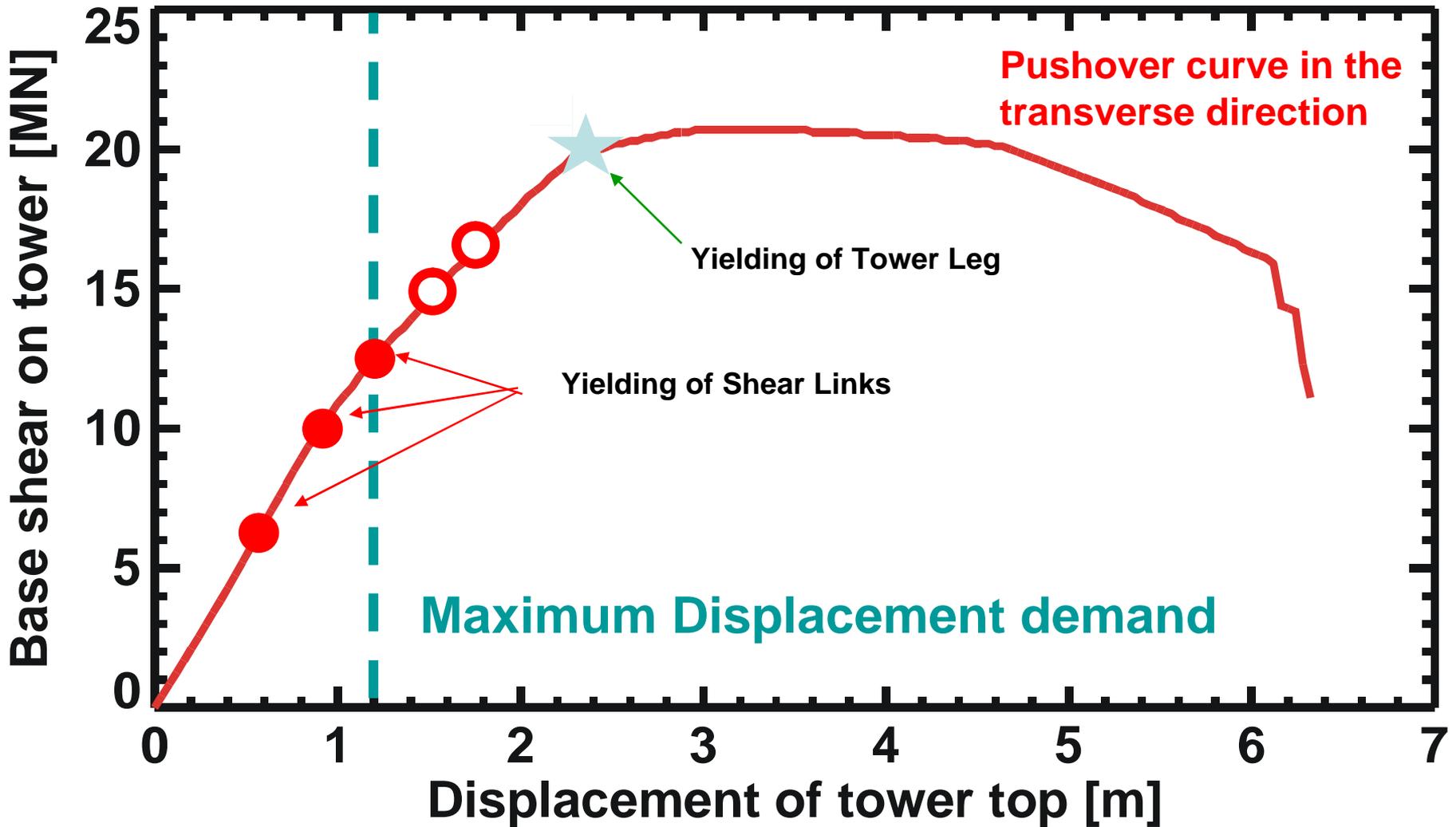
Influence of Tower Link Location

● Yielding of the tower shaft during SEE

Tune strength, stiffness and location of the links to achieve the optimum design



Tower Displacement Capacity/Demand



SFOBB East Bay Replacement



State of US Infrastructure



2003 Report Card for America's Infrastructure

Roads	D+
Bridges	C
Transit	C-

Aviation	D
Schools	D-
Drinking Water	D

<p>America's Infrastructure G.P.A. = D+</p> <p>Total Investment Needs = \$ 1.6 Trillion</p> <p><i>(estimated 5-year need)</i></p>	<p>A = Exceptional B = Good C = Fair D = Poor F = Inadequate</p>	<p>Each category was evaluated on the basis of condition and performance, capacity vs. need, and funding vs. need.</p>
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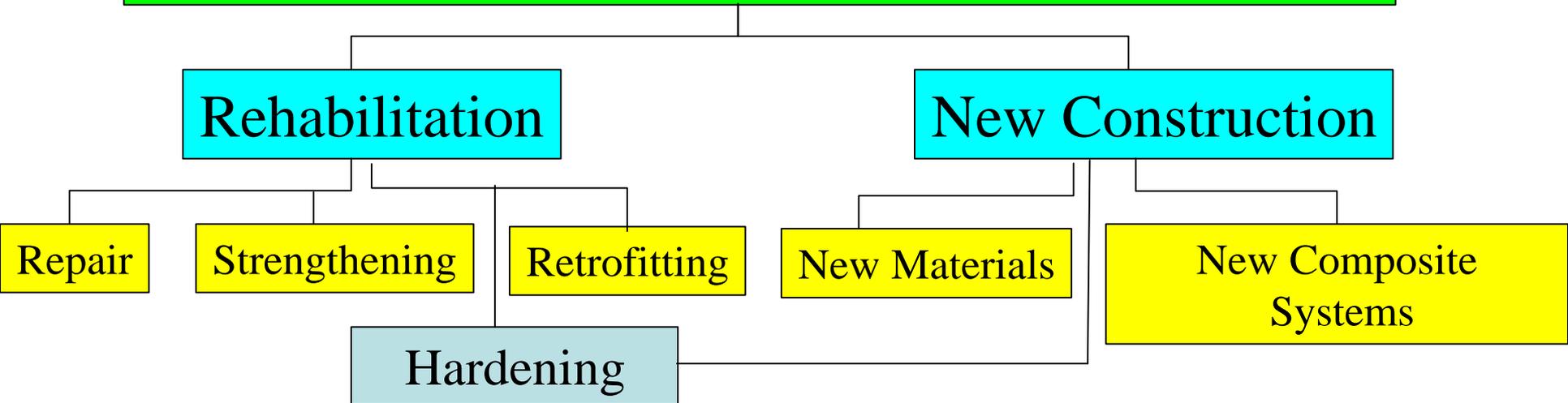
Condition of Constructed Facilities



Structural Health Monitoring
Damage Prognosis
Life Cycle Prediction
Renewal Engineering

New Materials
New Application/Construction Processes
New Design Concepts
New Infrastructure Management

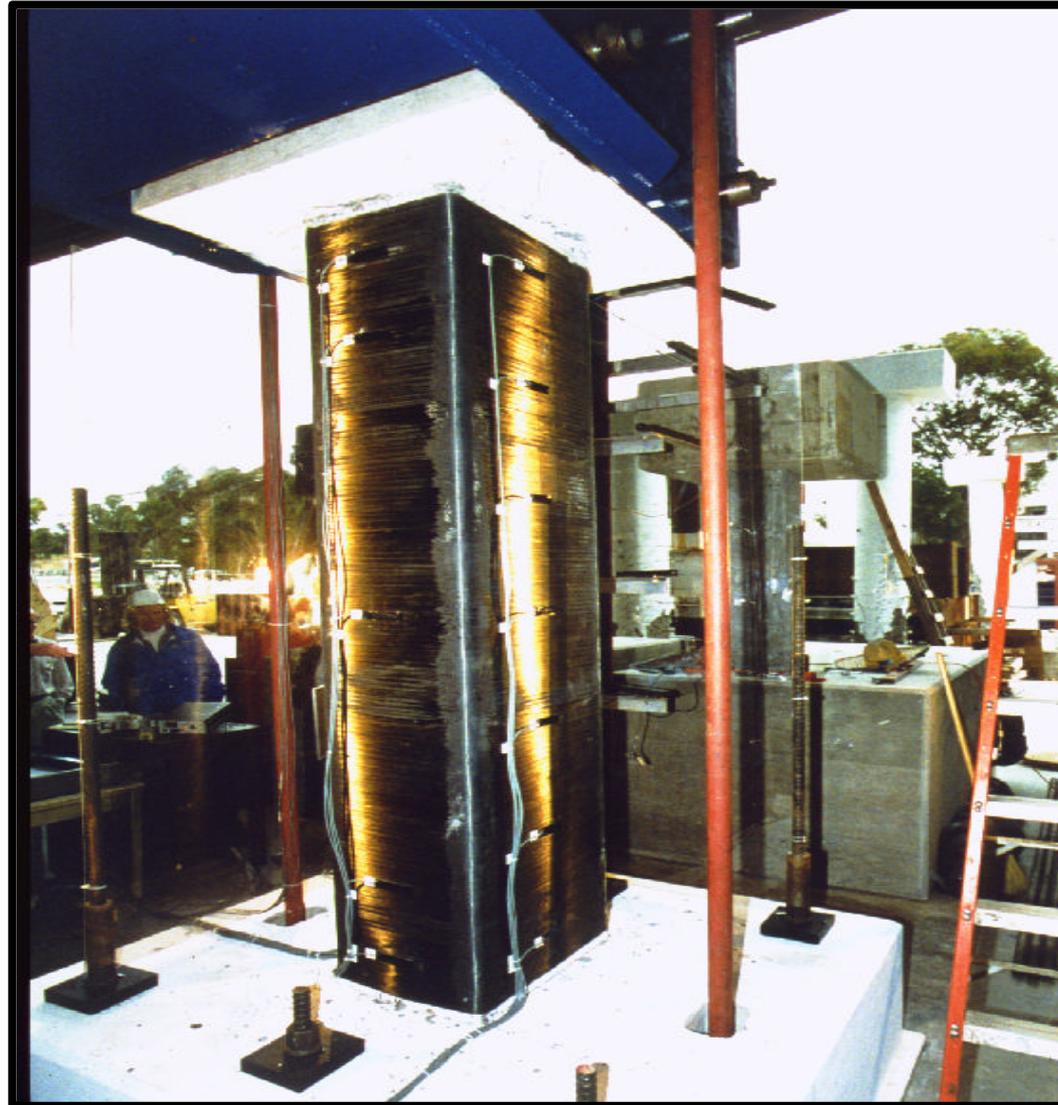
RENEWAL OF STRUCTURAL INVENTORY



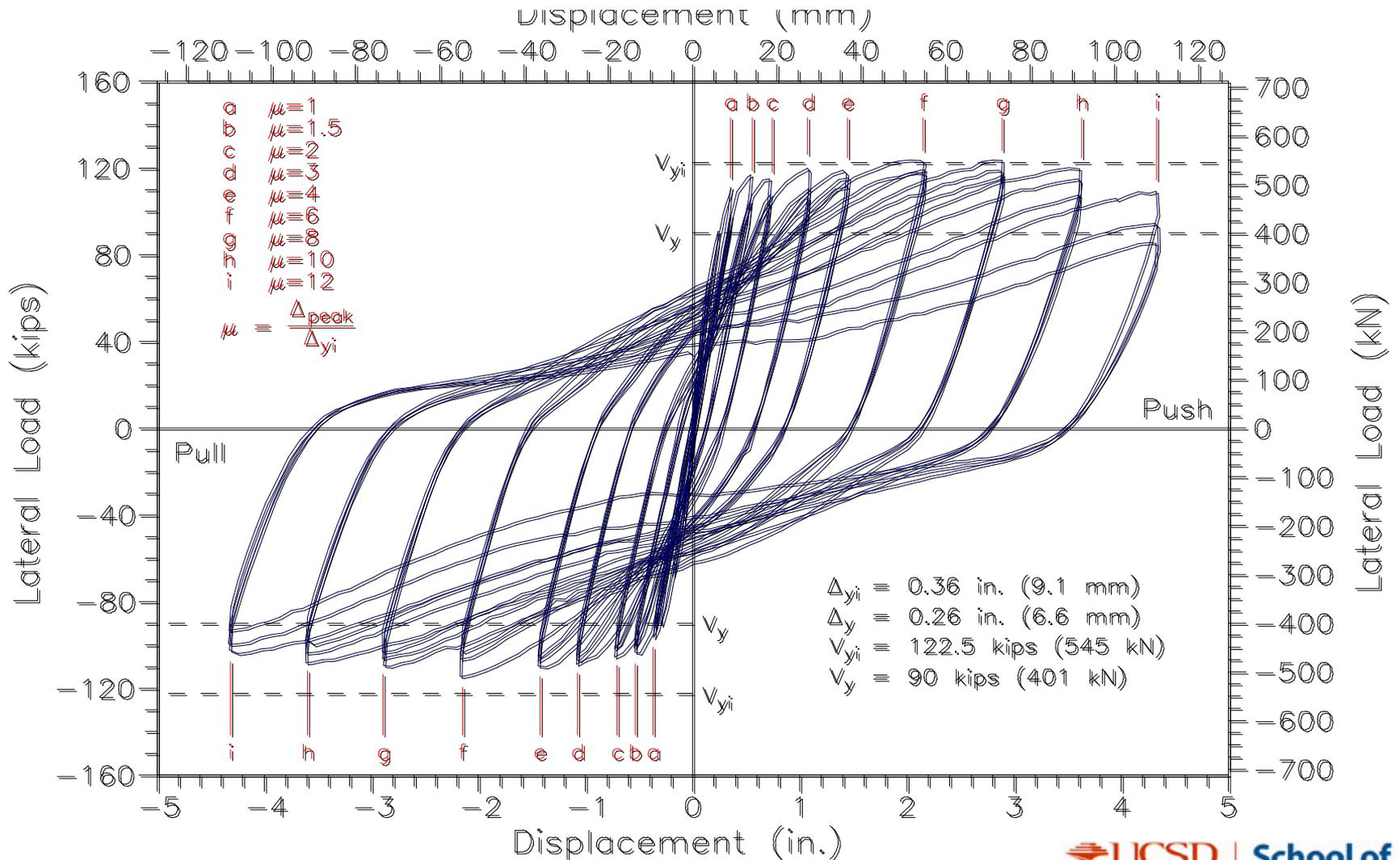
Distributed Sensors/Networks
Wireless Instrumentation/Data
Instantaneous Access/Processing
Data Archiving, etc.

Example of Composite Retrofit of Column

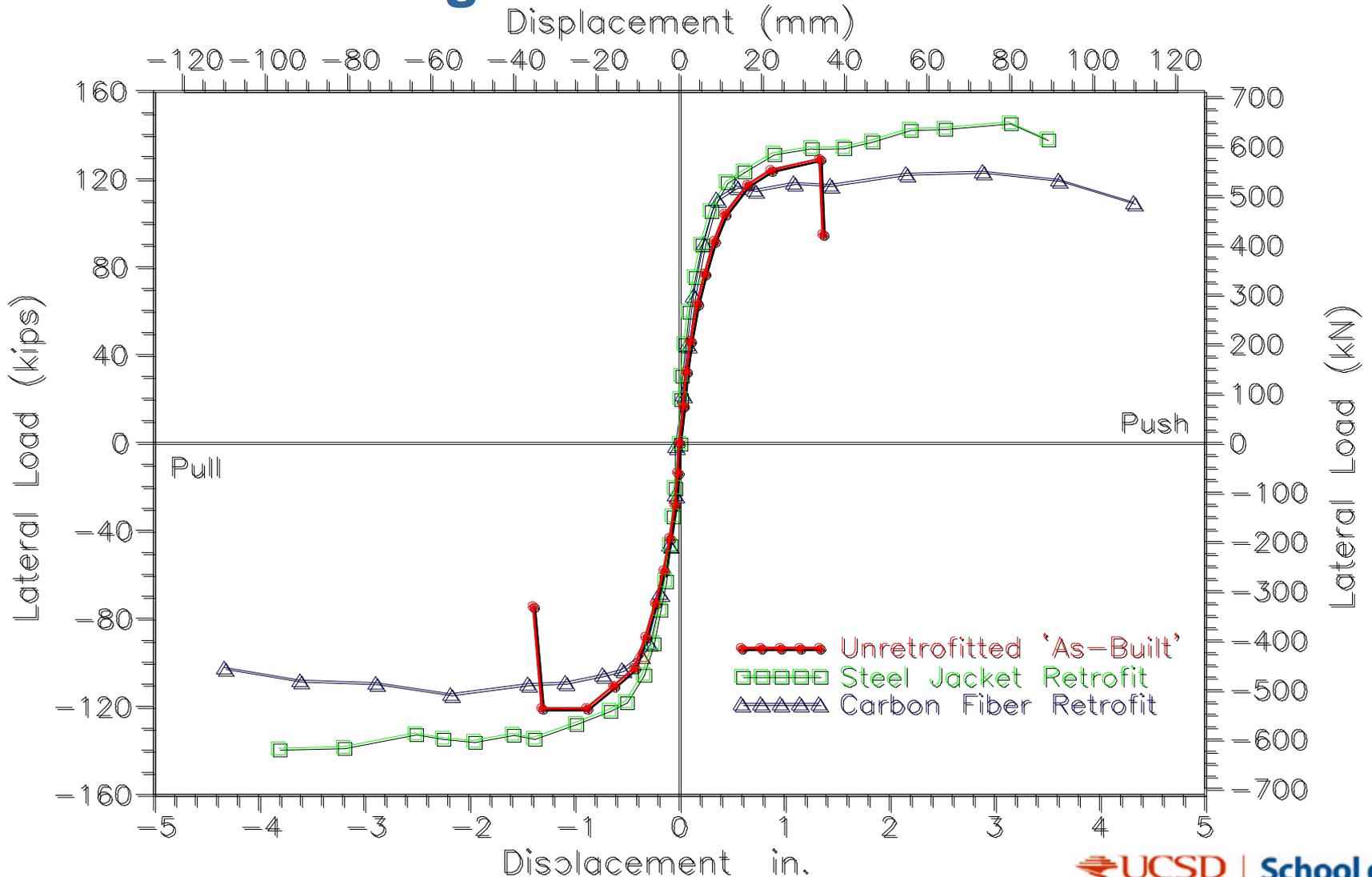
Rectangular
Column
CFRP Retrofit



Load-Displacement Curve for Fiber Retrofitted Column - Rectangular Shear Column 2.5%



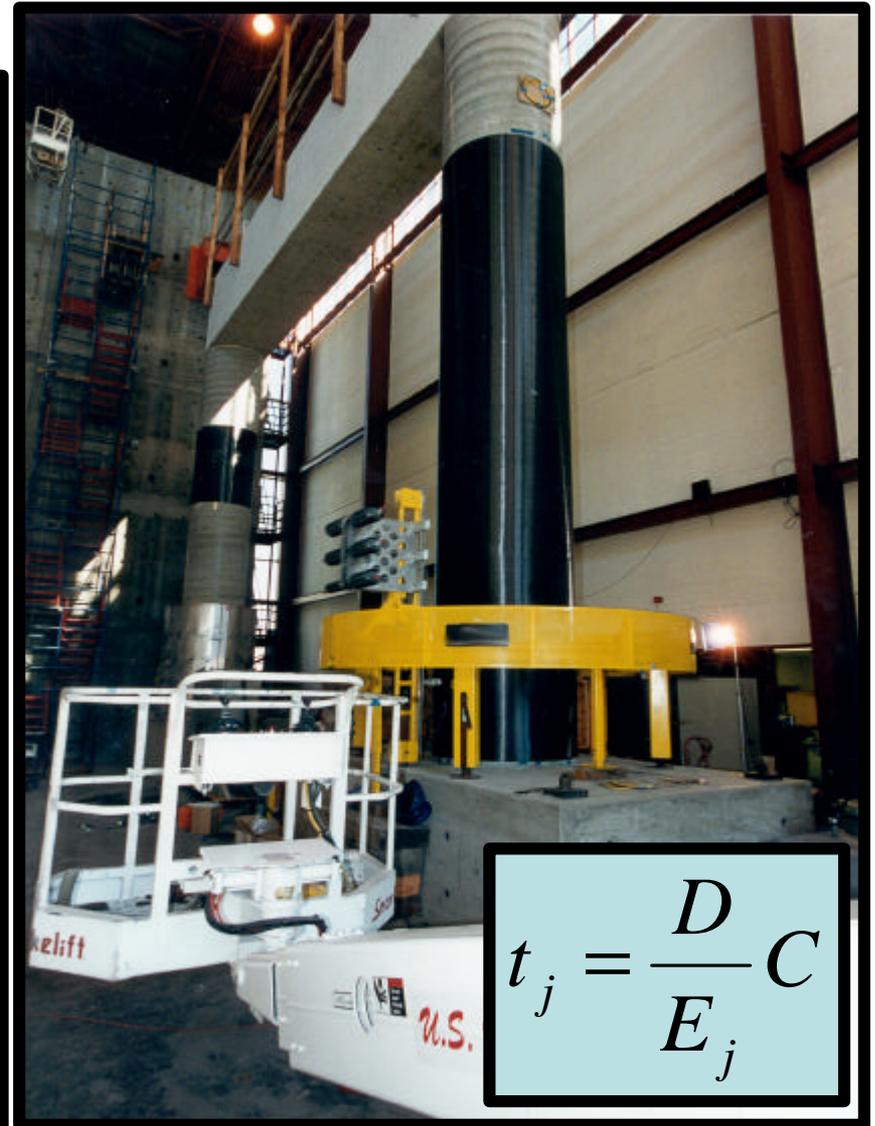
Comparison of Load-Displacement Envelopes Rectangular Shear Column 2.5%



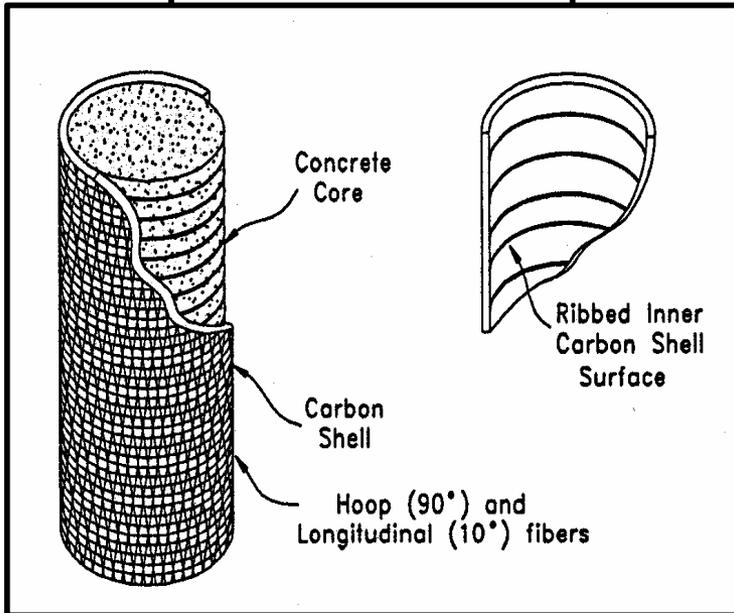
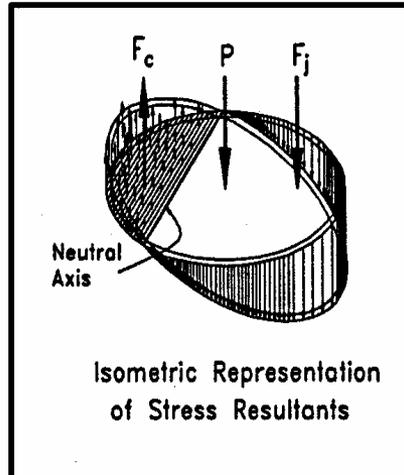
Installation of FRP Jacket, I-10 Santa Monica Viaduct



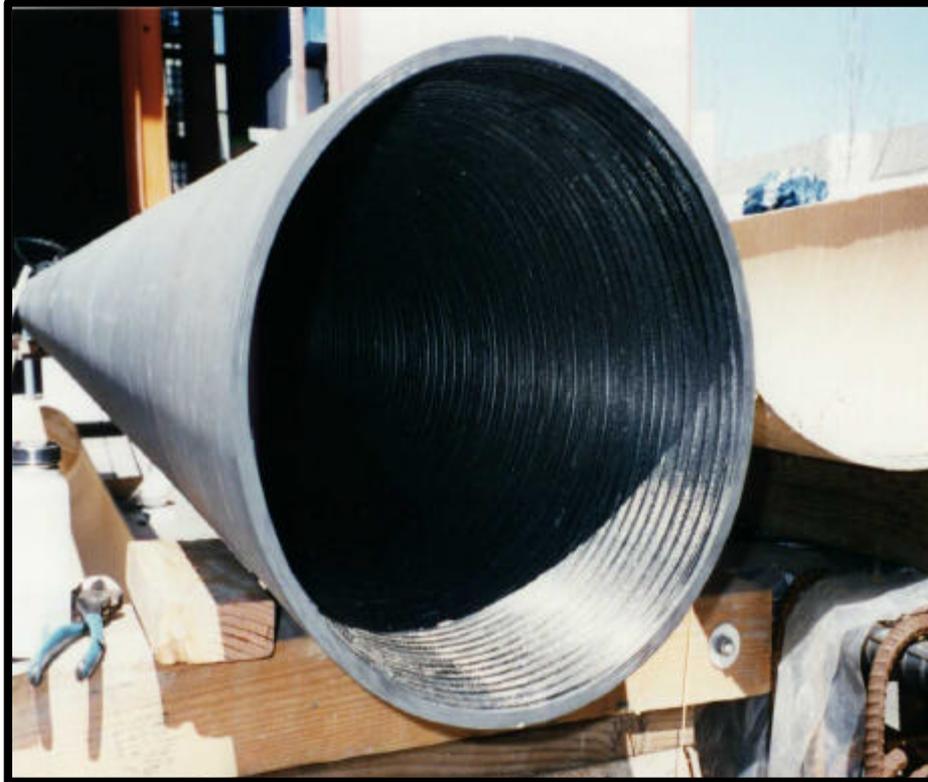
Full Scale Proof Test



Concrete Filled Carbon Shell System



Concrete Filled Carbon Shell System









Toro Peak



UCSD Advanced Composites Bridge
Imperial County (near Palm Springs)



100 accelerometers, strain gages, and video link

Bridge → Toro Peak → Mt Soledad → Anywhere worldwide

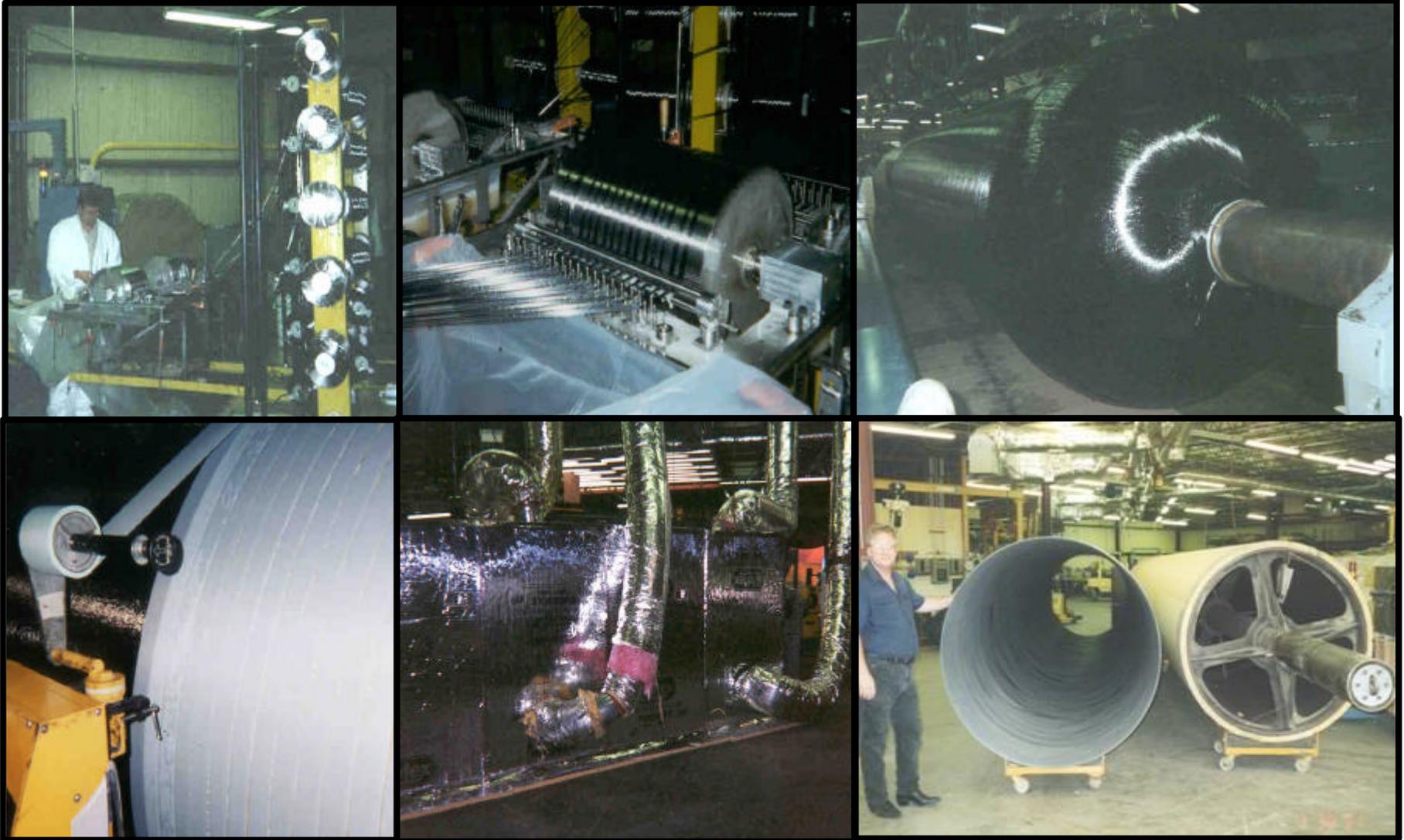
Continuous Wireless Monitoring <http://hpwren.ucsd.edu/>

Caltrans -- Research Connection -- Thursday, June 17, 2004

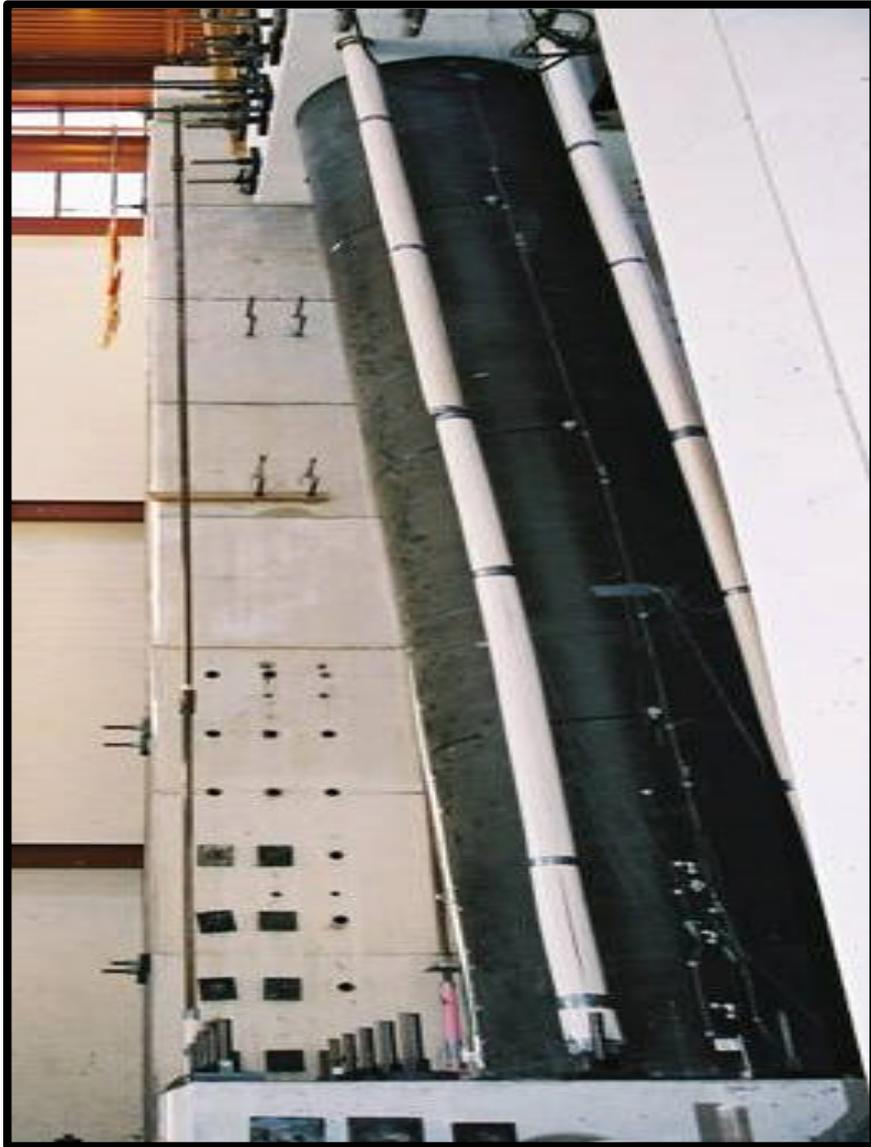
Pylon Shell (1.5m Diameter, 9mm thick)



Pylon Manufacturing



Extreme drift at displacement ductility 7



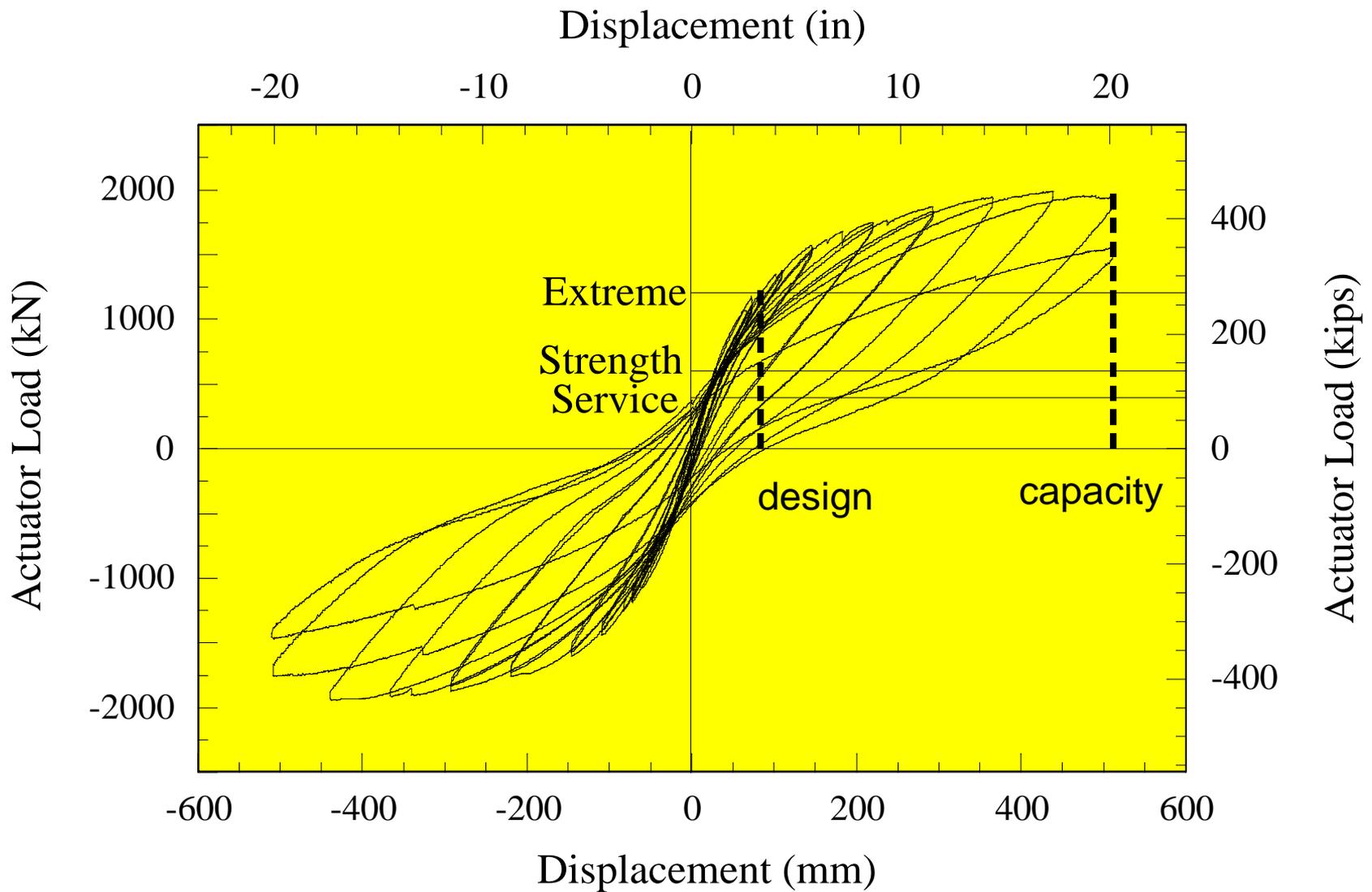
Ruptured bars at end of test (15 out of 30 bars ruptured w/minimal strength degradation)



a) Push side of footing



b) Pull side of footing

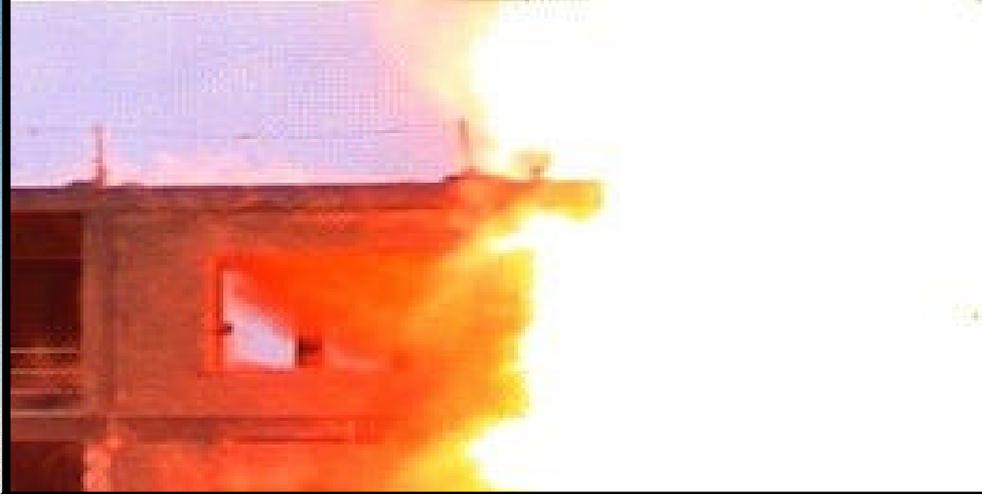




Applications of CSS

- ***Modular Construction***
- ***Light-weight***
- ***Stay-in-place Forms***
- ***Reinforcement***
- ***Seismic – Confinement***
- ***Blast Resistance***

Blast Mitigation of Critical Structures



Caltrans -- Research Connection -- Thursday, June 17, 2004

What the threat may look like!



Blast Retrofit of Buildings





Blast Damage to Unretrofitted and Retrofitted Reinforced Concrete Column (CTS-1 Structure)





DB-20 High Speed Photography

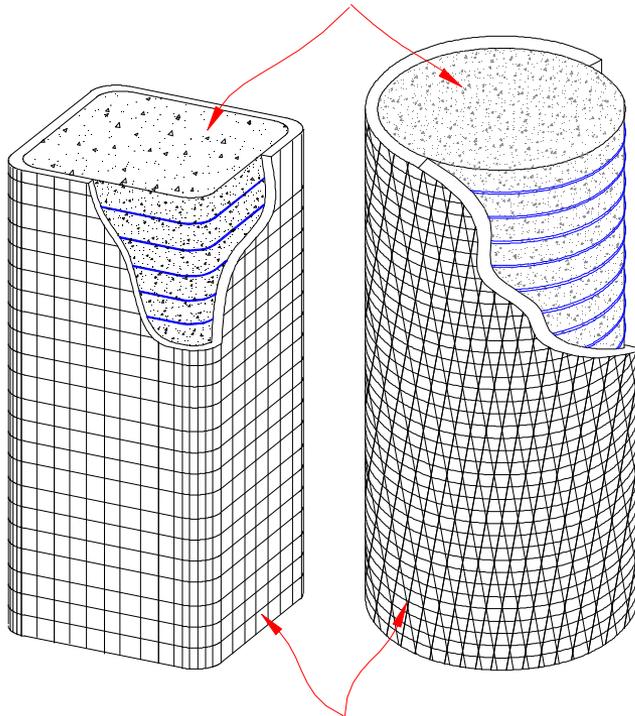




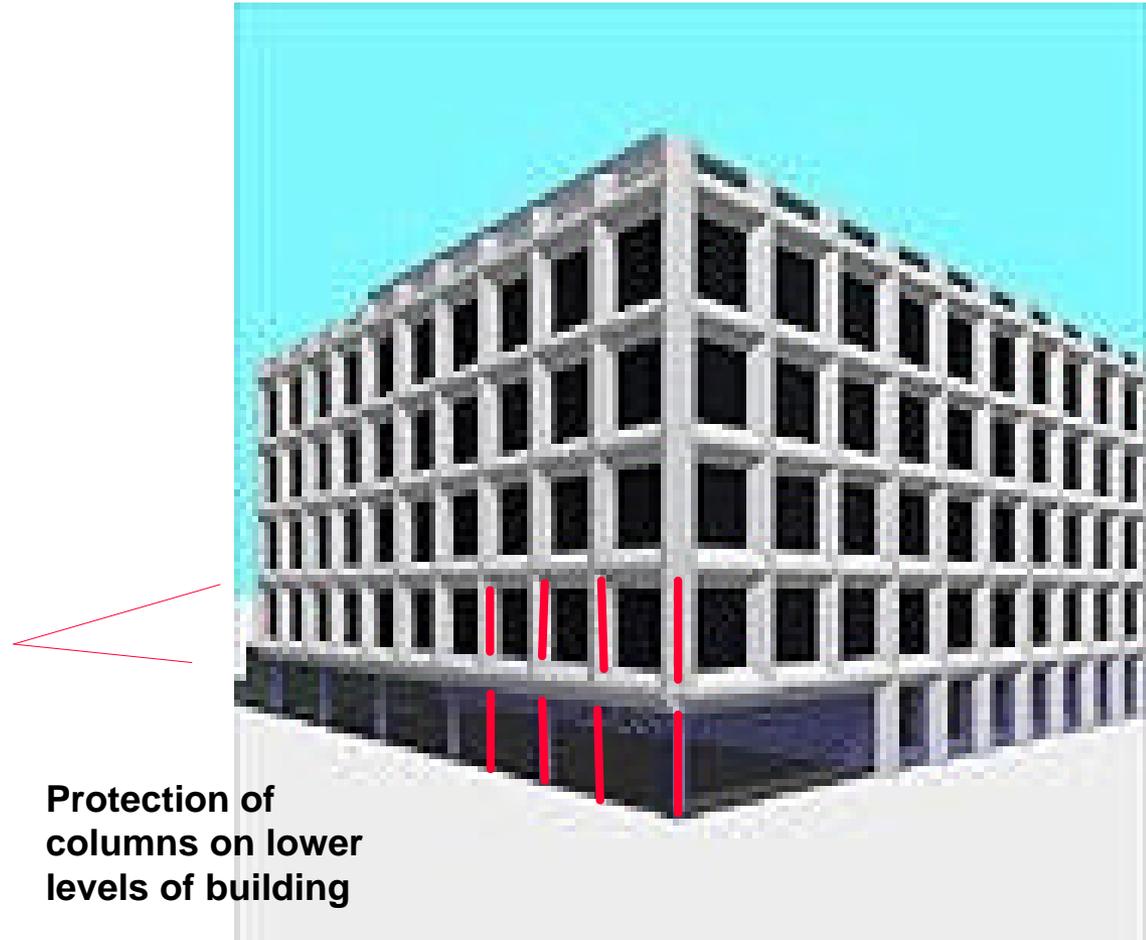


Column Protection For New Critical Facilities

Concrete core



Carbon composite shell with transverse and longitudinal fibers



Protection of columns on lower levels of building



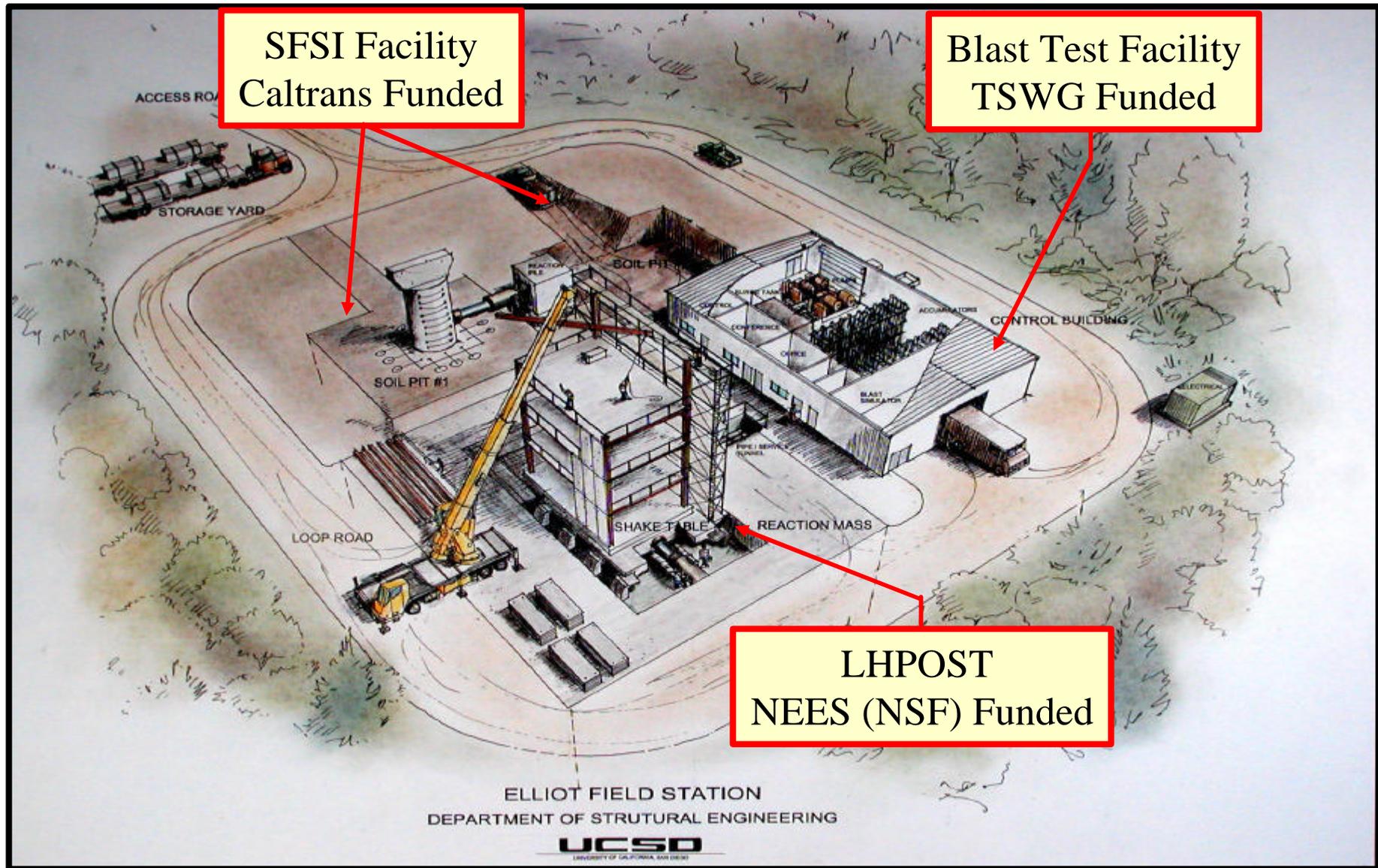
**Four 27-strand DSI
tendons looped
through footing for a
total applied axial
load of approximately
2000 tons**

Camp Elliott Development Project

SFSI Facility
Caltrans Funded

Blast Test Facility
TSWG Funded

LHPOST
NEES (NSF) Funded



ELLIOT FIELD STATION
DEPARTMENT OF STRUTURAL ENGINEERING
UCSD
UNIVERSITY OF CALIFORNIA, SAN DIEGO

CONCLUSIONS

Research on Seismic Bridge Response leads to

1. Better Simulation Tools for Seismic Response Assessment
2. Retrofit Technology Development to Correct Local Detailing Deficiencies
3. Proof of Concept Testing to Validate Retrofit Measures and New Design Concepts

