

DEPARTMENT OF TRANSPORTATION

DIVISION OF ENGINEERING SERVICES

Office of Structural Materials

Quality Assurance and Source Inspection



Bay Area Branch
690 Walnut Ave. St. 150
Vallejo, CA 94592-1133
(707) 649-5453
(707) 649-5493

Contract #: 04-0120F4Cty: SF/ALA Rte: 80 PM: 13.2/13.9File #: 69.25B**QUALITY ASSURANCE -- NON-CONFORMANCE REPORT****Location:** Changxing Island, Shanghai, P.R. China**Report No:** NCR-000738**Prime Contractor:** American Bridge/Fluor Enterprises, a JV**Date:** 20-May-2010**Submitting Contractor:** Zhenhua Port Machinery Company, Ltd (ZPMC), Changxing Island**NCR #:** ZPMC-0701**Type of problem:**

Welding	Concrete	Other	
Welding	Curing	Procedural	Bridge No: 34-0006
Joint fit-up	Coating	Other	Component: OBG Suspender Bracket SB66E
Procedural	Procedural	Description:	

Reference Description: Heat straightening of Suspender Bracket Top Plate utilizing excessive heat**Description of Non-Conformance:**

During the Quality Assurance (QA) random in-process observations of the fabrication of OBG Suspender Bracket (SB), this Caltrans QA Inspector and Structural Materials Representative documented the following:

-ZPMC personnel performed heat straightening of suspender bracket (SB66E) top plate X53B. The material was heated to a red color.

-AWS D1.5 2002 defines the color of material heated to 650 °C as a "dull red color".

-ZPMC Heat Straightening Report HSR1 (B)-8477 indicated that the maximum temperature shall not exceed 650 °C.

-A temperature indicating crayon, digital temperature measurement gauge, or other similar means of monitoring the temperature was not utilized by ZPMC QC and the actual maximum attained temperature was not measured.

-HSR1 (B)-8477 dated 5/13/2010, approved by ZPMC QA Manager Lu Jian Hua, did not provide information of the original deformation requiring correction by heat straightening.

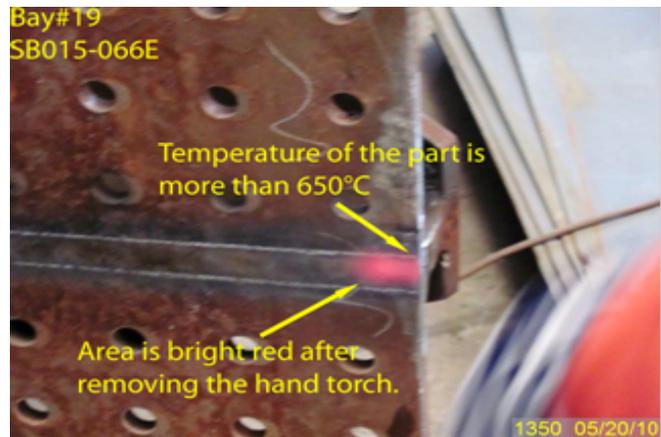
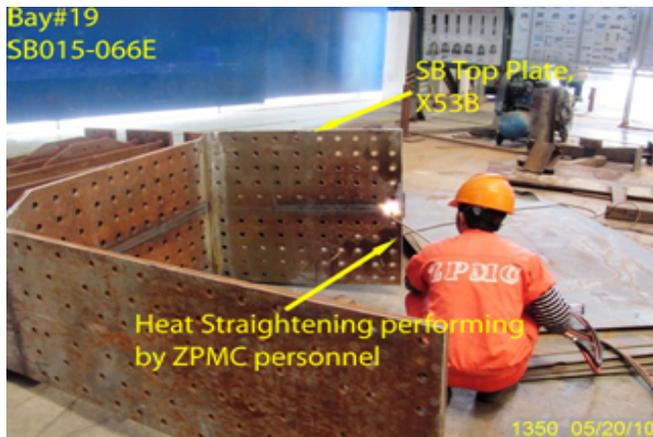
-ZPMC QC CWI personnel Xu Tao was aware of the on-going heat straightening work performed and allowed worker to perform without any temperature measuring device.

-The Suspender bracket is identified as SB015-066E.

-The base material thickness is 20mm.

QUALITY ASSURANCE -- NON-CONFORMANCE REPORT

(Continued Page 2 of 2)



Applicable reference:

AWS 1.5 2002 section 3.7.3 "Members distorted by welding shall be straightened by mechanical means or by carefully supervised application of a limited amount of localized heat as approved by the Engineer. The temperature of the heated areas as measured by approved methods shall not exceed 600°C [1100 °F] for quenched and tempered steel nor 650°C [1200 °F] (a dull, red color) for other steels. The part to be heated for straightening shall be substantially free of stress and from external forces, except those stresses resulting from the mechanical straightening method used in conjunction with the application of heat."

Who discovered the problem: Hiranch Patel and Eric Tsang

Name of individual from Contractor notified: Steve Lawton

Time and method of notification: 15:00 Hrs, 05/20/10, Verbal

Name of Caltrans Engineer notified: Sean Eagen, Stanley Ku

Time and method of notification: 14:00 Hrs, 05/20/10, Verbal

QC Inspector's Name: Xu Tao

Was QC Inspector aware of the problem: Yes No

Contractor's proposal to correct the problem:

N/A

Comments:

This report is for the purpose of determining conformance with the contract documents and is not for the purpose of making repair or fit for purpose recommendations. Should you require recommendations concerning repairs or remedial efforts please contact Mazen Wahbeh, (818) 292-0659, who represents the Office of Structural Materials for your project.

Inspected By: Tsang, Eric SMR

Reviewed By: Wahbeh, Mazen SMR



DEPARTMENT OF TRANSPORTATION - District 4 Toll Bridge
666 Feng Bin Road Room 708, Changxing Island
Shanghai 201913 PR China
Tel: 021-56856666 ext 207061 Fax:

NON-CONFORMANCE REPORT TRANSMITTAL

To: AMERICAN BRIDGE/FLUOR, A JV
375 BURMA ROAD
OAKLAND CA 95607

Date: 21-May-2010

Contract No: 04-0120F4
04-SF-80-13.2 / 13.9

Dear: Mr. Charles Kanapicki

Job Name: SAS Superstructure

Attention: Mr. Thomas Nilsson Project/Fabrication Manager

Document No: 05.03.06-000696

Subject: NCR No. ZPMC-0701

Reference Description: Heat straightening of Suspender Bracket Top Plate utilizing excessive heat

The attached Non-Conformance Report describes an occurrence where the contractor did not comply with a requirement of the contract document as indicated below:

- Material or Workmanship not in conformance with contract documents.
- Quality Control (QC) not performed in conformance with contract documents.
- Recurring QC issue that constitutes a systematic problem in quality control.
- Non-Conformance Resolved.

Material Location: OBG **Lift:**

Remarks:

During the Quality Assurance (QA) random in-process observations of the fabrication of OBG Suspender Bracket (SB), this Caltrans QA Inspector and Structural Materials Representative documented the following:

- ZPMC personnel performed heat straightening of suspender bracket (SB66E) top plate X53B. The material was heated to a red color.
- AWS D1.5 2002 defines the color of material heated to 650 °C as a "dull red color".
- ZPMC Heat Straightening Report HSR1 (B)-8477 indicated that the maximum temperature shall not exceed 650 °C.

-A temperature indicating crayon, digital temperature measurement gauge, or other similar means of monitoring the temperature was not utilized by ZPMC QC and the actual maximum attained temperature was not measured.

-HSR1 (B)-8477 dated 5/13/2010, approved by ZPMC QA Manager Lu Jian Hua, did not provide information of the original deformation requiring correction by heat straightening.

-ZPMC QC CWI personnel Xu Tao was aware of the on-going heat straightening work performed and allowed worker to perform without any temperature measuring device.

- The Suspender bracket is identified as SB015-066E.
- The base material thickness is 20mm.

Action Required and/or Action Taken:

Propose a resolution for the identified non-conformance with revised procedures to prevent future occurrences. A response for the resolution of this issue is expected within 7 days.

NCT

(Continued Page 2 of 2)

Transmitted by: Sean Eagen Transportation Engineer

Attachments: ZPMC-0701

cc: Rick Morrow, Gary Pursell, Peter Siegenthaler, Stanley Ku, Brian Boal, Jason Tom, Contract Files, Ching Chao, Bill Casey

File: 05.03.06

NCR PROPOSED RESOLUTION

To: CALTRANS - SAS Superstructure
333 Burma Road
Oakland CA 94607

Attention: Pursell, Gary
Resident Engineer

Ref: 05.03.06-000696

Subject: NCR No. ZPMC-0701

Dated: 11-Jun-2010

Contract No.: 04-0120F4
04-SF-80-13.2 / 13.9

Job Name: SAS Superstructure

Document No.: ABF-NPR-000698 Rev: 00

Contractor's Proposed Resolution:

Reference Resolution: As the inspector did not have a temperature stick to determine that the member was heated above 650 degree Celsius it should not be assumed that the heat exceeded 650 degrees Celsius.

The basis of this NCR was made based on the inspector's subjective assessment of the color red. As he did not have a temperature stick to determine that the member was heated above 650 degree Celsius it should not be assumed that the heat exceeded 650 degrees Celsius. Based on this, the NCR is not based on objective evidence and therefore lacks merit, this NCR should be closed.

Submitted by: Ishibashi, Joshua

Attachment(s): ABF-NPR-000698R00

Caltrans' comments:

Status: REJ

Date: 14-Jun-2010

The heating noted in this NCR does not comply with the referenced sections of the AWS code. Please address issues related to both 1) the suitability of the material after being heated beyond limits allowed by the AWS code, and 2) QC not having the proper equipment to monitor temperatures during heat straightening operations.

Submitted by: Eagen, Sean

Attachment(s):

Date: 14-Jun-2010

NCR PROPOSED RESOLUTION

To: CALTRANS - SAS Superstructure
333 Burma Road
Oakland CA 94607

Attention: Pursell, Gary
Resident Engineer

Ref: 05.03.06-000696

Subject: NCR No. ZPMC-0701

Dated: 07-Jul-2010

Contract No.: 04-0120F4
04-SF-80-13.2 / 13.9

Job Name: SAS Superstructure

Document No.: ABF-NPR-000698 Rev: 01

Contractor's Proposed Resolution:

Reference Resolution: ZPMC has performed the hardness testing and used Table 3 in ASTM370 to determine the approximate tensile values

ZPMC has performed the hardness testing and used Table 3 in ASTM370 to determine the approximate tensile values and compared them to minimum required values found in ASTM 709 for Grade 50[345] and found they meet the minimum required values. ZPMC QA has also written and internal NCR to notify the Technical Department to provide more detail when writing the HSR and the QC Department to ensure they have the correct temperature monitoring equipment on hand during heat straightening. Based on these actions ZPMC requests that this NCR be closed.

Submitted by: Ishibashi, Joshua

Attachment(s): ABF-NPR-000698R01;

Caltrans' comments:

Status: AAP

Date: 07-Jul-2010

The corrective actions and preventive measures taken by the Contractor are acceptable. This NCR is considered closed.

Submitted by: Woo, Laraine

Attachment(s):

Date: 07-Jul-2010



No. B-811

LETTER OF RESPONSE

TO: American Bridge/Flour

DATE: 2010-07-02

REGARDING: NCR-000738(ZPMC-0701)

ZPMC has performed the hardness testing and used Table 3 in ASTM 370 to determine the approximate tensile values and compared them to minimum required values found in ASTM 709 for Grade 50[345] and found they meet the minimum required values. The testing was performed by CT's witness. ZPMC QA has written an internal NCR and advised to Technical Department to provide more detailing when issuing HSRs. All QC will be equipped with temperature monitoring equipment to prevent this issue from occurring again. Based on these, ZPMC is requesting that this NCR be closed.

ATTACHMENT:

N CR-000738(ZPMC-0701)

HARDNESS TESTING ANALYSIS

TENSILE AND HARDNESS REQUIREMENTS IN ASTM 709

APPROXIMATE HARDNESS CONVERSION NUMBERS IN ASTM 370

A handwritten signature in black ink, appearing to be 'J. W.' or similar, written in a cursive style.

7/2/10



DEPARTMENT OF TRANSPORTATION - District 4 Toll Bridge
666 Feng Bin Road Room 708, Changxing Island
Shanghai 201913 PR China
Tel: 021-56856666 ext 207061 Fax:

NON-CONFORMANCE REPORT TRANSMITTAL

To: AMERICAN BRIDGE/FLUOR, A JV
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Date: 21-May-2010

Contract No: 04-0120F4
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Dear: Mr. Charles Kanapicki
Attention: Mr. Thomas Nilsson Project/Fabrication Manager
Subject: NCR No. ZPMC-0701

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Reference Description: Heat straightening of Suspender Bracket Top Plate utilizing excessive heat

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02.02:15.04
NCT 05.03.06-000696.NCT

Received
NCT-000696 21 May 10 Page 1 of 2

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Contract #: 04-0120F4
 Cty: SF/ALA Rte: 80 PM: 13.2/13.9
 File #: 69.25B

QUALITY ASSURANCE -- NON-CONFORMANCE REPORT

Location: Changxing Island, Shanghai, P.R. China

Report No: NCR-000738

Prime Contractor: American Bridge/Fluor Enterprises, a JV

Date: 20-May-2010

Submitting Contractor: Zhenhua Port Machinery Company, Ltd (ZPMC), Changxing Island

NCR #: ZPMC-0701

Type of problem:

Welding Concrete Other

Welding Curing Procedural Bridge No: 34-0006

Joint fit-up Coating Other Component: OBG Suspender Bracket SB66E

Procedural Procedural Description:

Reference Description: Heat straightening of Suspender Bracket Top Plate utilizing excessive heat

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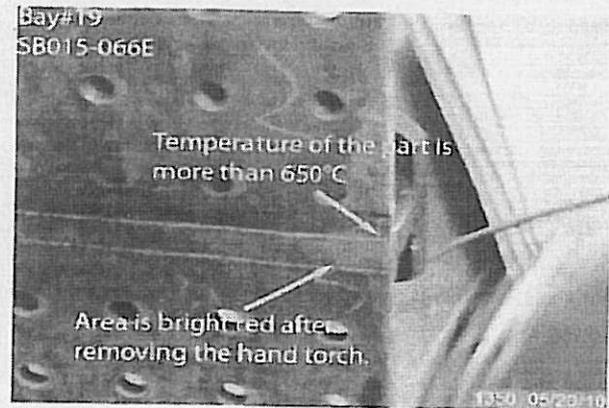
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QUALITY ASSURANCE -- NON-CONFORMANCE REPORT

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Comments:

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Inspected By: Tsang, Eric

SMR

Reviewed By: Wahbeh, Mazen

SMR

Area	Test ID					SB66E Top Plate Hardness Testing Analysis					Meets Requirement?
	A*	B*	C*	D*	E*	Average Value**	Corresponding Brinell Hardness Value***	Approximate Tensile Strength (ksi)***	Minimum Tensile Strength (ksi)****		
1	168	167	167	178	174	170	169	83	65	YES	
2	189	152	172	182	168	174	172	84	65	YES	
3	173	146	184	161	162	165	165	82	65	YES	
4	177	161	152	178	177	172	172	84	65	YES	
5	169	173	140	175	157	166	165	82	65	YES	

*All values are Brinell Hardness

**High and low values excluded when determining average value

*** Per Table 3 ASTM A370-07b

**** For Grade 50[345], per Table 1, ASTM A709/A709M-05



A 709/A 709M - 05

TABLE 1 Tensile and Hardness Requirements^A

NOTE 1— Where “...” appears in this table, there is no requirement.

Grade	Plate Thickness, in. [mm]	Structural Shape Flange or Leg Thickness, in. [mm]	Yield Point or Yield Strength, ^B ksi [MPa]	Tensile Strength, ksi [MPa]	Minimum Elongation, %				Reduction of Area ^{C,D} min, %	Brinell Hardness Number
					Plates and Bars ^{C,E}		Shapes ^F			
					8 in. or 200 mm	2 in. or 50 mm	8 in. or 200 mm	2 in. or 50 mm		
36 [250]	to 4 [100], incl	to 3 in. [75 mm], incl over 3 in. [75 mm]	36 [250] min 36 [250] min	58-80 [400-550] 58 [400] min	20 ...	23 ...	20 20	21 ^F 19
50 [345] 50S [345S]	to 4 [100], incl ^G	all	50 [345] min 50-65 345-450 ^H 50 [345] min	65 [450] min 65 [450] ^H min	18 ...	21 ...	18 18	21 ^F 21
50W [345W] and HPS 50W [HPS 345W] HPS 70W [HPS 485 W] 100 [690], 100W [690W], and HPS 100W [HPS 690W] 100 [690] and 100W [690 W]	to 4 [100], incl to 4 [100], incl to 2½ [65], incl over 2½ to 4 [65 to 100]	all ^G ^G ^G	70 [485] min ^B 100 [690] min ^B 90 [620] min ^B	85-110 [585-760] 110-130 [760-895] 100-130 [690-895]	19 ^J 18 ^J 16 ^J κ κ 235-293 ^L ...

^A See specimen orientation and preparation subsection in the Tension Tests section of Specification A 6/A 6 M.

^B Measured at 0.2 % offset or 0.5 % extension under load as described in Section 13 of Test Methods A 370.

^C Elongation and reduction of area not required to be determined for floor plates.

^D For plates wider than 24 in. [600 mm], the reduction of area requirement, where applicable, is reduced by five percentage points.

^E For plates wider than 24 in. [600 mm], the elongation requirement is reduced by two percentage points. See elongation requirement adjustments in the Tension Tests section of Specification A 6/A 6 M.

^F Elongation in 2 in. or 50 mm: 19 % for shapes with flange thickness over 3 in. [75 mm].

^G Not applicable.

^H The yield to tensile ratio shall be 0.85 or less.

^I For wide flange shapes with flange thickness over 3 in. [75 mm], elongation in 2 in. or 50 mm. of 18 % minimum applies.

^J If measured on the Fig. 3 (Test Methods A 370) 1½-in. [40-mm] wide specimen, the elongation is determined in a 2-in. or 50-mm. gage length that includes the fracture and shows the greatest elongation.

^K 40 % minimum applies if measured on the Fig 3 (Test Methods A 370) 1½-in. [40-mm] wide specimen; 50 % minimum applies if measured on the Fig. 4 (Test Methods A 370) ½-in. [12.5-mm] round specimen.

^L Applies only to Grades 100 [690] and 100W [690W] plates that are ¾ in. [10 mm] or less in thickness and are not tension tested (See 8.1).

TABLE 2 Grade 36 [250] Chemical Requirements (Heat Analysis)

NOTE 1— Where “...” appears in this table there is no requirement. The heat analysis for manganese shall be determined and reported as described in the Heat Analysis section of Specification A 6/A 6 M.

Product Thickness, in. (mm)	Shapes ^A All	Plates ^B				Bars ^B		
		To ¾ [20], incl	Over ¾ to 1½ [20 to 40], incl	Over 1½ to 2½ [40 to 65], incl	Over 2½ to 4 [65 to 100], incl	To ¾ [20], incl	Over ¾ to 1½ [20 to 40], incl	Over 1½ to 4 [100], incl
Carbon, max, %	0.26	0.25	0.25	0.26	0.27	0.26	0.27	0.28
Manganese, %	0.80-1.20	0.80-1.20	0.85-1.20	...	0.60-0.90	0.60-0.90
Phosphorus, max, %	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04
Sulfur, max, %	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05
Silicon, %	0.40 max	0.40 max	0.40 max	0.15-0.40	0.15-0.40	0.40 max	0.40 max	0.40 max
Copper, min, % when copper steel is specified	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20

^A Manganese content of 0.85 to 1.35 % and silicon content of 0.15 to 0.40 % is required for shapes with flange thickness over 3 in. [75 mm].

^B For each reduction of 0.01 % below the specified carbon maximum, an increase of 0.06 % manganese above the specified maximum will be permitted up to a maximum of 1.35 %.

A 992/A 992M Specification for Structural Steel Shapes
G 101 Guide for Estimating the Atmospheric Corrosion Resistance of Low-Alloy Steels

3. Terminology

3.1 Definitions of Terms Specific to This Standard:

 A 370 - 05

TABLE 3 Approximate Hardness Conversion Numbers for Non-austenitic Steels^A (Rockwell B to Other Hardness Numbers)

Rockwell B Scale, 100-kgf Load 1/16-in. (1.588-mm) Ball	Vickers Hardness Number	Brinell Hardness, 3000-kgf Load, 10-mm Ball	Knoop Hardness, 500-gf Load and Over	Rockwell A Scale, 60-kgf Load, Diamond Penetrator	Rockwell F Scale, 60-kgf Load, 1/16-in. (1.588-mm) Ball	Rockwell Superficial Hardness			Approximate Tensile Strength ksi (MPa)
						15T Scale, 15-kgf Load, 1/16-in. (1.588-mm) Ball	30T Scale, 30-kgf Load, 1/16-in. (1.588-mm) Ball	45T Scale, 45-kgf Load, 1/16-in. (1.588-mm) Ball	
100	240	240	251	61.5	...	93.1	83.1	72.9	116 (800)
99	234	234	246	60.9	...	92.8	82.5	71.9	114 (785)
98	228	228	241	60.2	...	92.5	81.8	70.9	109 (750)
97	222	222	236	59.5	...	92.1	81.1	69.9	104 (715)
96	216	216	231	58.9	...	91.8	80.4	68.9	102 (705)
95	210	210	226	58.3	...	91.5	79.8	67.9	100 (690)
94	205	205	221	57.6	...	91.2	79.1	66.9	98 (675)
93	200	200	216	57.0	...	90.8	78.4	65.9	94 (650)
92	195	195	211	56.4	...	90.5	77.8	64.8	92 (635)
91	190	190	206	55.8	...	90.2	77.1	63.8	90 (620)
90	185	185	201	55.2	...	89.9	76.4	62.8	89 (615)
89	180	180	196	54.6	...	89.5	75.8	61.8	88 (605)
88	176	176	192	54.0	...	89.2	75.1	60.8	86 (590)
87	172	172	188	53.4	...	88.9	74.4	59.8	84 (580)
86	169	169	184	52.8	...	88.6	73.8	58.8	83 (570)
85	165	165	180	52.3	...	88.2	73.1	57.8	82 (565)
84	162	162	176	51.7	...	87.9	72.4	56.8	81 (560)
83	159	159	173	51.1	...	87.6	71.8	55.8	80 (550)
82	156	156	170	50.6	...	87.3	71.1	54.8	77 (530)
81	153	153	167	50.0	...	86.9	70.4	53.8	73 (505)
80	150	150	164	49.5	...	86.6	69.7	52.8	72 (495)
79	147	147	161	48.9	...	86.3	69.1	51.8	70 (485)
78	144	144	158	48.4	...	86.0	68.4	50.8	69 (475)
77	141	141	155	47.9	...	85.6	67.7	49.8	68 (470)
76	139	139	152	47.3	...	85.3	67.1	48.8	67 (460)
75	137	137	150	46.8	99.6	85.0	66.4	47.8	66 (455)
74	135	135	147	46.3	99.1	84.7	65.7	46.8	65 (450)
73	132	132	145	45.8	98.5	84.3	65.1	45.8	64 (440)
72	130	130	143	45.3	98.0	84.0	64.4	44.8	63 (435)
71	127	127	141	44.8	97.4	83.7	63.7	43.8	62 (425)
70	125	125	139	44.3	96.8	83.4	63.1	42.8	61 (420)
69	123	123	137	43.8	96.2	83.0	62.4	41.8	60 (415)
68	121	121	135	43.3	95.6	82.7	61.7	40.8	59 (405)
67	119	119	133	42.8	95.1	82.4	61.0	39.8	58 (400)
66	117	117	131	42.3	94.5	82.1	60.4	38.7	57 (395)
65	116	116	129	41.8	93.9	81.8	59.7	37.7	56 (385)
64	114	114	127	41.4	93.4	81.4	59.0	36.7	...
63	112	112	125	40.9	92.8	81.1	58.4	35.7	...
62	110	110	124	40.4	92.2	80.8	57.7	34.7	...
61	108	108	122	40.0	91.7	80.5	57.0	33.7	...
60	107	107	120	39.5	91.1	80.1	56.4	32.7	...
59	106	106	118	39.0	90.5	79.8	55.7	31.7	...
58	104	104	117	38.6	90.0	79.5	55.0	30.7	...
57	103	103	115	38.1	89.4	79.2	54.4	29.7	...
56	101	101	114	37.7	88.8	78.8	53.7	28.7	...
55	100	100	112	37.2	88.2	78.5	53.0	27.7	...
54	111	36.8	87.7	78.2	52.4	26.7	...
53	110	36.3	87.1	77.9	51.7	25.7	...
52	109	35.9	86.5	77.5	51.0	24.7	...
51	108	35.5	86.0	77.2	50.3	23.7	...
50	107	35.0	85.4	76.9	49.7	22.7	...
49	106	34.6	84.8	76.6	49.0	21.7	...
48	105	34.1	84.3	76.2	48.3	20.7	...
47	104	33.7	83.7	75.9	47.7	19.7	...
46	103	33.3	83.1	75.6	47.0	18.7	...
45	102	32.9	82.6	75.3	46.3	17.7	...
44	101	32.4	82.0	74.9	45.7	16.7	...
43	100	32.0	81.4	74.6	45.0	15.7	...
42	99	31.6	80.8	74.3	44.3	14.7	...
41	98	31.2	80.3	74.0	43.7	13.6	...
40	97	30.7	79.7	73.6	43.0	12.6	...
39	96	30.3	79.1	73.3	42.3	11.6	...
38	95	29.9	78.6	73.0	41.6	10.6	...
37	94	29.5	78.0	72.7	41.0	9.6	...
36	93	29.1	77.4	72.3	40.3	8.6	...
35	92	28.7	76.9	72.0	39.6	7.6	...
34	91	28.2	76.3	71.7	39.0	6.6	...
33	90	27.8	75.7	71.4	38.3	5.6	...

TABLE 3 *Continued*

Rockwell B Scale, 100-kgf Load 1/16-in. (1.588-mm) Ball	Vickers Hardness Number	Brinell Hardness, 3000-kgf Load, 10-mm Ball	Knoop Hardness, 500-gf Load and Over	Rockwell A Scale, 60-kgf Load, Diamond Penetrator	Rockwell F Scale, 60-kgf Load, 1/16-in. (1.588-mm) Ball	Rockwell Superficial Hardness			Approximate Tensile Strength ksi (MPa)
						15T Scale, 15-kgf Load, 1/16-in. (1.588-mm) Ball	30T Scale, 30-kgf Load, 1/16-in. (1.588-mm) Ball	45T Scale, 45-kgf Load, 1/16-in. (1.588-mm) Ball	
32	89	27.4	75.2	71.0	37.6	4.6	...
31	88	27.0	74.6	70.7	37.0	3.6	...
30	87	26.6	74.0	70.4	36.3	2.6	...

^A This table gives the approximate interrelationships of hardness values and approximate tensile strength of steels. It is possible that steels of various compositions and processing histories will deviate in hardness-tensile strength relationship from the data presented in this table. The data in this table should not be used for austenitic stainless steels, but have been shown to be applicable for ferritic and martensitic stainless steels. The data in this table should not be used to establish a relationship between hardness values and tensile strength of hard drawn wire. Where more precise conversions are required, they should be developed specially for each steel composition, heat treatment, and part.

TABLE 4 Approximate Hardness Conversion Numbers for Austenitic Steels (Rockwell C to other Hardness Numbers)

Rockwell C Scale, 150-kgf Load, Diamond Penetrator	Rockwell A Scale, 60-kgf Load, Diamond Penetrator	Rockwell Superficial Hardness		
		15N Scale, 15-kgf Load, Diamond Penetrator	30N Scale, 30-kgf Load, Diamond Penetrator	45N Scale, 45-kgf Load, Diamond Penetrator
48	74.4	84.1	66.2	52.1
47	73.9	83.6	65.3	50.9
46	73.4	83.1	64.5	49.8
45	72.9	82.6	63.6	48.7
44	72.4	82.1	62.7	47.5
43	71.9	81.6	61.8	46.4
42	71.4	81.0	61.0	45.2
41	70.9	80.5	60.1	44.1
40	70.4	80.0	59.2	43.0
39	69.9	79.5	58.4	41.8
38	69.3	79.0	57.5	40.7
37	68.8	78.5	56.6	39.6
36	68.3	78.0	55.7	38.4
35	67.8	77.5	54.9	37.3
34	67.3	77.0	54.0	36.1
33	66.8	76.5	53.1	35.0
32	66.3	75.9	52.3	33.9
31	65.8	75.4	51.4	32.7
30	65.3	74.9	50.5	31.6
29	64.8	74.4	49.6	30.4
28	64.3	73.9	48.8	29.3
27	63.8	73.4	47.9	28.2
26	63.3	72.9	47.0	27.0
25	62.8	72.4	46.2	25.9
24	62.3	71.9	45.3	24.8
23	61.8	71.3	44.4	23.6
22	61.3	70.8	43.5	22.5
21	60.8	70.3	42.7	21.3
20	60.3	69.8	41.8	20.2

requirement, the conversions listed in Table 2, Table 3, Table 4, and Table 5 shall be used.

15.2.2 When recording converted hardness numbers, the measured hardness and test scale shall be indicated in parentheses, for example: 353 HB (38 HRC). This means that a hardness value of 38 was obtained using the Rockwell C scale and converted to a Brinell hardness of 353.

16. Brinell Test

16.1 Description:

16.1.1 A specified load is applied to a flat surface of the specimen to be tested, through a hard ball of specified diameter. The average diameter of the indentation is used as a basis for calculation of the Brinell hardness number. The quotient of the applied load divided by the area of the surface of the

indentation, which is assumed to be spherical, is termed the Brinell hardness number (HB) in accordance with the following equation:

$$HB = P / [(\pi D/2)(D - \sqrt{D^2 - d^2})] \quad (4)$$

where:

- HB = Brinell hardness number,
- P = applied load, kgf,
- D = diameter of the steel ball, mm, and
- d = average diameter of the indentation, mm.

NOTE 11—The Brinell hardness number is more conveniently secured from standard tables such as Table 6, which show numbers corresponding to the various indentation diameters, usually in increments of 0.05 mm.

NOTE 12—In Test Method E 10 the values are stated in SI units, whereas in this section kg/m units are used.

TABLE 5 Approximate Hardness Conversion Numbers for Austenitic Steels (Rockwell B to other Hardness Numbers)

Rockwell B Scale, 100-kgf Load, $\frac{1}{16}$ -in. (1.588-mm) Ball	Brinell Indentation Diameter, mm	Brinell Hardness, 3000-kgf Load, 10-mm Ball	Rockwell A Scale, 60-kgf Load, Diamond Penetrator	Rockwell Superficial Hardness		
				15T Scale, 15-kgf Load, $\frac{1}{16}$ -in. (1.588-mm) Ball	30T Scale, 30-kgf Load, $\frac{1}{16}$ -in. (1.588-mm) Ball	45T Scale, 45-kgf Load, $\frac{1}{16}$ -in. (1.588-mm) Ball
100	3.79	256	61.5	91.5	80.4	70.2
99	3.85	248	60.9	91.2	79.7	69.2
98	3.91	240	60.3	90.8	79.0	68.2
97	3.96	233	59.7	90.4	78.3	67.2
96	4.02	226	59.1	90.1	77.7	66.1
95	4.08	219	58.5	89.7	77.0	65.1
94	4.14	213	58.0	89.3	76.3	64.1
93	4.20	207	57.4	88.9	75.6	63.1
92	4.24	202	56.8	88.6	74.9	62.1
91	4.30	197	56.2	88.2	74.2	61.1
90	4.35	192	55.6	87.8	73.5	60.1
89	4.40	187	55.0	87.5	72.8	59.0
88	4.45	183	54.5	87.1	72.1	58.0
87	4.51	178	53.9	86.7	71.4	57.0
86	4.55	174	53.3	86.4	70.7	56.0
85	4.60	170	52.7	86.0	70.0	55.0
84	4.65	167	52.1	85.6	69.3	54.0
83	4.70	163	51.5	85.2	68.6	52.9
82	4.74	160	50.9	84.9	67.9	51.9
81	4.79	156	50.4	84.5	67.2	50.9
80	4.84	153	49.8	84.1	66.5	49.9

16.1.2 The standard Brinell test using a 10-mm ball employs a 3000-kgf load for hard materials and a 1500 or 500-kgf load for thin sections or soft materials (see Annex A2 on Steel Tubular Products). Other loads and different size indentors may be used when specified. In recording hardness values, the diameter of the ball and the load must be stated except when a 10-mm ball and 3000-kgf load are used.

16.1.3 A range of hardness can properly be specified only for quenched and tempered or normalized and tempered material. For annealed material a maximum figure only should be specified. For normalized material a minimum or a maximum hardness may be specified by agreement. In general, no hardness requirements should be applied to untreated material.

16.1.4 Brinell hardness may be required when tensile properties are not specified.

16.2 *Apparatus*—Equipment shall meet the following requirements:

16.2.1 *Testing Machine*—A Brinell hardness testing machine is acceptable for use over a loading range within which its load measuring device is accurate to $\pm 1\%$.

16.2.2 *Measuring Microscope*—The divisions of the micrometer scale of the microscope or other measuring devices used for the measurement of the diameter of the indentations shall be such as to permit the direct measurement of the diameter to 0.1 mm and the estimation of the diameter to 0.05 mm.

NOTE 13—This requirement applies to the construction of the microscope only and is not a requirement for measurement of the indentation, see 16.4.3.

16.2.3 *Standard Ball*—The standard ball for Brinell hardness testing is 10 mm (0.3937 in.) in diameter with a deviation from this value of not more than 0.005 mm (0.0004 in.) in any diameter. A ball suitable for use must not show a permanent change in diameter greater than 0.01 mm (0.0004 in.) when pressed with a force of 3000 kgf against the test specimen.

16.3 *Test Specimen*—Brinell hardness tests are made on prepared areas and sufficient metal must be removed from the surface to eliminate decarburized metal and other surface irregularities. The thickness of the piece tested must be such that no bulge or other marking showing the effect of the load appears on the side of the piece opposite the indentation.

16.4 *Procedure*:

16.4.1 It is essential that the applicable product specifications state clearly the position at which Brinell hardness indentations are to be made and the number of such indentations required. The distance of the center of the indentation from the edge of the specimen or edge of another indentation must be at least two and one-half times the diameter of the indentation.

16.4.2 Apply the load for a minimum of 15 s.

16.4.3 Measure two diameters of the indentation at right angles to the nearest 0.1 mm, estimate to the nearest 0.05 mm, and average to the nearest 0.05 mm. If the two diameters differ by more than 0.1 mm, discard the readings and make a new indentation.

DEPARTMENT OF TRANSPORTATION

DIVISION OF ENGINEERING SERVICES

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Contract #: 04-0120F4Cty: SF/ALA Rte: 80 PM: 13.2/13.9File #: xx.25A**QUALITY ASSURANCE -- NON-CONFORMANCE RESOLUTION****Location:** Changxing Island, Shanghai, P.R. China**Report No:** NCS-000705**Prime Contractor:** American Bridge/Fluor Enterprises, a JV**Date:** 07-Jul-2010**Submitting Contractor:** Zhenhua Port Machinery Company, Ltd (ZPMC), Changxing Island **NCR #:** ZPMC-0701**Type of problem:**

Welding	Concrete	Other	
Welding	Curing	Procedural	Bridge No: 34-0006
Joint fit-up	Coating	Other	Component:
Procedural	Procedural	Descriptor:	

Date the Non-Conformance Report was written: 20-May-2010**Description of Non-Conformance:**

During the Quality Assurance (QA) random in-process observations of the fabrication of OBG Suspender Bracket (SB), this Caltrans QA Inspector and Structural Materials Representative documented the following:

-ZPMC personnel performed heat straightening of suspender bracket (SB66E) top plate X53B. The material was heated to a red color.

-AWS D1.5 2002 defines the color of material heated to 650 °C as a "dull red color".

-ZPMC Heat Straightening Report HSR1 (B)-8477 indicated that the maximum temperature shall not exceed 650 °C.

-A temperature indicating crayon, digital temperature measurement gauge, or other similar means of monitoring the temperature was not utilized by ZPMC QC and the actual maximum attained temperature was not measured.

-HSR1 (B)-8477 dated 5/13/2010, approved by ZPMC QA Manager Lu Jian Hua, did not provide information of the original deformation requiring correction by heat straightening.

-ZPMC QC CWI personnel Xu Tao was aware of the on-going heat straightening work performed and allowed worker to perform without any temperature measuring device.

-The Suspender bracket is identified as SB015-066E.

-The base material thickness is 20mm.

Contractor's proposal to correct the problem:

Perform hardness testing over area in question.

Corrective action taken:

