## TABLE 5

SUMMARY OF ANALYTICAL RESULTS: METALS
SEISMIC RETROFIT OF THE WEST APPROACH
SAN FRANCISCO - OAKLAND BAY BRIDGE
**RETAINING WALL**

| BORING | DEPTH | SB | AS | BA | BE | CD | CR | CO | CU | PB | HG | MO | NI | SE | AG | TL | V | ZN |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| B-1 | S | <5.0 | <5.0 | 220 | <0.5 | 0.6 | 27 | 12 | 36 | 160 (4.9) | 0.21 | <2.5 | 26 | <2.5 | <0.5 | <5.0 | 22 | 180 |
| | 2 | <5.0 | <5.0 | 150 | <0.5 | 2.8 | 15 | 7.2 | 13 | 51 (1.7) | 0.11 | <2.5 | 17 | <2.5 | <0.5 | <5.0 | 15 | 360 |
| B-2 | S | <5.0 | <5.0 | 220 | <0.5 | 1 | 22 | 9.7 | 45 | 290 (11) {0.15} | 0.23 | <2.5 | 25 | <2.5 | <0.5 | <5.0 | 22 | 240 |
| B-3 | S | <5.0 | 5.1 | 200 | <0.5 | 1.4 | 40 | 16 | 57 | 120 (6.8) {ND}* | 0.21 | <2.5 | 37 | <2.5 | <0.5 | <5.0 | 25 | 340 |
| | 3 | <5.0 | <5.0 | 140 | <0.5 | 0.8 | 15 | 5.5 | 86 | 99 (3.8) | 0.1 | <2.5 | 26 | <2.5 | <0.5 | <5.0 | 15 | 150 |
| B-4 | S | <5.0 | <5.0 | 160 | <0.5 | 0.9 | 36 | 10 | 36 | 170 (10) {ND}* | 0.22 | <2.5 | 31 | <2.5 | <0.5 | <5.0 | 26 | 170 |
| | 1 | <5.0 | <5.0 | 180 | <0.5 | <0.5 | 23 | 12 | 24 | 65 (2.4) | 0.13 | <2.5 | 30 | <2.5 | <0.5 | <5.0 | 22 | 70 |
| B-5 | S | <5.0 | <5.0 | 180 | <0.5 | 0.7 | 35 | 13 | 38 | 110 (6.3) {ND}* | 0.2 | <2.5 | 35 | <2.5 | <0.5 | 5.4 | 29 | 120 |
| B-6 | S | <5.0 | <5.0 | 200 | <0.5 | 0.9 | 29 | 16 | 48 | 520 (24) {0.06} | 0.17 | <2.5 | 36 | <2.5 | <0.5 | 5.1 | 31 | 190 |
| B-7 | S | <5.0 | 5.1 | 230 | <0.5 | 0.8 | 24 | 15 | 39 | 100 (4.8) | 0.15 | <2.5 | 42 | <2.5 | <0.5 | 6.5 | 26 | 180 |
| B-8 | S | <5.0 | <5.0 | 100 | <0.5 | 1.1 | 26 | 5.6 | 44 | 1,800 (150) {1.2} | 0.18 | <2.5 | 24 | <2.5 | <0.5 | <5.0 | 21 | 350 |
| B-9 | S | <50 | <50 | 150 | <5.0 | <5.0 | 35 | 18 | 45* | 13* | 1.3 | <25 | 42 | <25 | <5.0 | <50 | 49 | 410 |
| | 3 | <5.0 | 5.2 | 110 | <0.5 | 0.7 | 26 | 5.2 | 130 | 200 (NS) | 3.5 (0.014) | <2.5 | 20 | <2.5 | <0.5 | <5.0 | 20 | 270 |
| B-10 | S | <5.0 | <5.0 | 84 | <0.5 | 0.7 | 21 | 5.9 | 110 | 140 (15) {1.5}* | 2.1 | <2.5 | 23 | <2.5 | <0.5 | <5.0 | 19 | 300 |
| | 3 | <5.0 | 7 | 53 | <0.5 | <0.5 | 14 | 2.1 | 29 | 440 (21) {0.53}* | 0.77 | <2.5 | 10 | <2.5 | <0.5 | <5.0 | 9.2 | 1200 |
| | 6 | <5.0 | <5.0 | 59 | <0.5 | <0.5 | 24 | 5.3 | 32 | 380 (14) {2.6} | 2.9 | <2.5 | 15 | <2.5 | <0.5 | <5.0 | 17 | 77 |
| B-11 | S | <5.0 | <5.0 | 52 | <0.5 | 0.5 | 30 | 5.7 | 38 | 350 (25) {0.55}* | 0.27 | <2.5 | 23 | <2.5 | <0.5 | <5.0 | 24 | 100 |
| | 2.5 | <5.0 | 9.1 | 100 | <0.5 | 0.7 | 32 | 7.8 | 62 | 380 (23) {0.87}* | 1.3 | <2.5 | 28 | <2.5 | <0.5 | <5.0 | 24 | 170 |
| B-13 | 1 | ND | 11 | 70 | ND | ND | 38 | 8.2 | 37 | 260 (12) {0.69} | 0.64 | ND | 36 | ND | 22 | ND | 35 | 94 |
| | 3 | ND | 11 | 48 | ND | ND | 23 | 2.7 | 20 | 10 | ND | ND | 23 | ND | ND | ND | 30 | 31 |
| | 6 | ND | 11 | 130 | ND | ND | 19 | 5.8 | 16 | 11 | ND | ND | 23 | ND | ND | ND | 21 | 42 |
| B14 | 1 | ND | 38 | 290 | ND | ND | 22 | 11 | 360 | 37* | 0.83 | 11 | 38 | ND | ND | ND | 40 | 700 |
| | 3 | ND | 39 | 12 | ND | ND | 24 | 24 | 100 | 11 | 2.9 (ND) | ND | 24 | ND | ND | ND | 45 | 15 |
| | 6 | ND | 5.1 | 9.9 | ND | ND | 39 | 4.4 | 3.7 | ND | 1.6 | ND | 19 | ND | ND | ND | 36 | 19 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 1 | ND | 250 | ND | 18 | 8.6 | 0.42 | 3.0 | 51 |
| 3 | ND | 78 | ND | 44 | 6.0 | ND | 5.7 | 75 |
| 5 | ND | 16 | ND | 41 | 4.8 | ND | ND | 21 |
| | 500 | 10,000 | 75 | 500 | 3,000 | 20 | | |
| | 15 | 100 | 0.75 | 5 | 80 | 0.2 | | |